HANDBOOK

FOR

SURVEYORS.

BY

MANSFIELD MERRIMAN,

Member of American Society of Civil Engineers,

AND

JOHN P. BROOKS,

President of the Clarkson College of Technology.

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PREFACE TO FIRST EDITION.

This work is designed for the use of classes in technical schools, and also as a field book for surveyors. It is intended to embrace in concise form the ground that a student should cover in surveying before taking up the subject of railroad location. Hence it includes the fundamental theoretical principles, land and town surveying, leveling and simple triangulation, and topography. The attempt has been made to discuss each of these topics clearly and concisely, and in accordance with the best modern methods.

The need of the volume arose merely from the fact that no text-book on elementary surveying in pocket-book form can now be found in the market. While in the field a student should have a book of tables ever at hand, and if these are combined with the text a double advantage is often found, particularly in adjusting instruments and in ruling forms for notes.

In arranging the order of presentation the rule has been as far as possible to proceed from the simple to the complex in a natural order. For instance, the most difficult thing in surveying is the determination of a true meridian, and hence in this volume it comes last of all, although in most other books it is presented at an early stage.

As all persons likely to use the volume have access to surveying instruments, no illustrations of these are given. The effort has been made, however, to set forth methods of testing and comparing instruments more fully than is usually done in elementary books. As an instance of this, attention is called to the determination of the eccentricity of the graduated circle of a transit given in Article 27.

The old terms "latitude" and "departure," borrowed from navigation, are not here used, but instead "latitude difference" and "longitude difference" are employed, as is universally

done in geodetic surveying; the terms "latitude" and "longitude" are moreover used in the same sense as in geodesy and astronomy. That this method has advantages the experience of many years of teaching may bear witness.

The first field work done by a student is usually plotted to a large scale, and hence in Chapter IV the effort is made to clearly distinguish between large-scale and small-scale topography Both the transit and the plane-table method of stadia work are presented, but preference is given to the former. Hydrographic and mine surveying are briefly outlined, the latter being with especial reference to the practice in the anthracite regions of Pennsylvania.

The tables of natural functions are given to five decimal places, while logarithms and logarithmic functions are given to six decimals. The old-fashioned traverse table is omitted, as it is of little value when sines and cosines are at hand. The tables for stadia reductions are those computed by Professor Arthur Winslow for two minute intervals of vertical angles. For assistance in compiling Tables III, V, and VI, acknowledgments are due to the United States Coast and Geodetic Survey.

NOTE TO FIFTH EDITION.

This edition is mainly characterized by new tables of positions of Polaris and by a new chart of lines of equal magnetic declination, the copy for which has been kindly furnished by the U. S. Coast and Geodetic Survey.

A few minor revisions have been made here and there. All known errors have been corrected.

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A HANDBOOK FOR SURVEYORS.

CHAPTER I.

FUNDAMENTAL PRINCIPLES.

ART. 1. GEOMETRY AND TRIGONOMETRY.

Geometry and Surveying were originally synonymous, as the etymology of the former word indicates. They originated in Egypt, where monuments and boundary lines were annually obliterated by the inundation of the Nile. Euclid, professor of mathematics at Alexandria about 250 B.C., wrote a treatise on geometry which has never been equaled in logical methods. Geometry furnishes the principles on which the operations of surveying are founded, whereby line and angle measurements, the computation of areas, and the construction of maps are effected. Arithmetic and Trigonometry are the tools by which the principles of Geometry are applied.

The following theorems of plane geometry are perhaps those of greatest importance, but many others are constantly used in the field practice of engineers:

If two straight lines intersect, the opposite angles are equal.

Straight lines parallel to the same straight line are parallel to each other.

The sum of the interior angles of a polygon is equal to twice as many right angles as the polygon has sides minus four right angles.

The sum of the exterior angles formed by producing the sides of a polygon is equal to four right angles.

The square upon the hypothenuse of a right-angled triangle is equal to the sum of the squares upon the other two sides.

Angles at the center of a circle are in the same ratio as their intercepted arcs.

An angle at the circumference of a circle is measured by one half the arc intercepted by its sides.

If the angles of two triangles are equal each to each, the homologous sides are proportional and the triangles are similar.

The areas of similar polygons are as the squares of their homologous sides.

The area of a triangle is measured by one half the product of its base and altitude. The area of a trapezoid is measured by one half the product of the sum of its parallel sides by its altitude.

The area of a sector of a circle is measured by one half the product of its arc and radius.

The circumference of a circle is equal to its diameter multiplied by 3.1415927. The area of a circle is equal to the square of its radius multiplied by 3.1415927.

Trigonometry, or the solution of triangles by means of sines and tangents of the angles, originated in the thirteenth century, previous computations having been made with chords. The following rules for the solution of oblique triangles are here given for reference, but it should be remembered that no surveyor can attain success unless he is thoroughly conversant with all of them without the necessity of referring to a book.

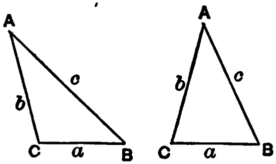


FIG. 1.

In any triangle let a, b, c, be the sides opposite the angles A, B, C. These sides are proportional to the sines of opposite angles. The value of each side may be expressed in three ways in terms of the other sides and angles; thus,

$$a = b\frac{\sin A}{\sin B} = c\frac{\sin A}{\sin C} = \sqrt{b^2 + c^2 - 2bc \cos A};$$

$$b = a\frac{\sin B}{\sin A} = c\frac{\sin B}{\sin C} = \sqrt{a^2 + c^2 - 2ac \cos B};$$

$$c = a\frac{\sin C}{\sin A} = b\frac{\sin C}{\sin B} = \sqrt{a^2 + b^2 - 2ab \cos C}.$$

Also each angle may be expressed as follows:

$$\sin A = \frac{a}{b}\sin B = \frac{a}{c}\sin C, \quad \cos A = \frac{b^2 + c^2 - a^2}{2bc};$$

$$\sin B = \frac{b}{a} \sin A = \frac{b}{c} \sin C, \quad \cos B = \frac{a^2 + c^2 - b^2}{2ac};$$

$$\sin C = \frac{c}{a} \sin A = \frac{c}{b} \sin B, \quad \cos C = \frac{a^2 + b^2 - c^2}{2ab}.$$

If A be made a right angle these reduce to the formulas for right triangles, which are too well known to be repeated here.

When two sides and their included angle are given, as a, b, C, then the formulas

$$\cot A = \frac{b}{a \sin C} - \cot C, \qquad \cot B = \frac{a}{b \sin C} - \cot C,$$

determine A and B, while as a check, $A + B + C = 180°$; the third side is then found from

$$c = a \sin C / \sin A.$$

When the three sides a, b, c are given, the cosines of the angles can be independently computed from the formulas above given. But some prefer to divide the triangle into two right-angled triangles by dropping a perpendicular from A upon the base a, thus dividing it into two segments, a_1 and a_2. The sum of these segments is a, their difference is

$$a_1 - a_2 = \frac{(b + c)(b - c)}{a}.$$

Let this difference be called d; then

$$a_1 = \tfrac{1}{2}(a + d) \quad \text{and} \quad a_2 = \tfrac{1}{2}(a - d).$$

Lastly the angles are found by

$$\cos B = a_2/c, \quad \cos C = a_1/b_1, \quad \text{and} \quad \sin A = a \sin B/b;$$

as a check $A + B + C = 180°$.

While the above expressions are sufficient for the solution of all plane triangles, there are other formulas more convenient for logarithmic computation for certain special cases. Tables of natural functions are generally used in ordinary surveying, particularly in the field, while logarithmic tables are perhaps better for rapid work in the office. The young surveyor should be prepared to solve triangles quickly and rapidly by either method.

In all kinds of computations a neat and orderly arrangement should be followed, and it is recommended that all problems given in these pages, as well as those arising in field practice, should be solved in ink in a special book and be preserved for reference. Check computations should in all cases be made; this can be done by finding the same quantity in different ways, by computing the three angles independently and taking their sum, or by using both natural functions and logarithmic tables.

Prob. 1. Given $a = 227.52$ feet, $b = 168.00$ feet, $C = 137° 25'$; to compute independently the angles A and B.

Art. 2. Lines, Angles, and Azimuths.

The measurement of a line consists in finding how many times it contains the unit of measure. For several centuries the Gunter's chain of 66 feet has been the English linear unit for land measurements; it is divided into 100 parts, called links, and lengths are expressed in chains aud links, the latter being written as decimals of a chain; thus 12 chains and 72 links is 12.72 chains. Although this chain is rapidly going out of use, the young surveyor should be acquainted with it, since a large part of the land records in the United States is based upon it.

In computing areas the chain has the advantage that square chains are easily reduced to acres by moving the decimal point one place to the left. This is because 66 feet $\times$ 66 feet $=$ 4356 square feet, which is one tenth of an acre. For example, a rectangular lot 6.48 chains long and 2.15 chains wide contains 13.932 square chains, or 1.3932 acres.

The unit of linear measure now generally used in the United States is the foot. In measuring lines a chain 100 feet long, divided into 100 links, is used, and distances are recorded in feet, decimals of a foot being estimated when possible. Tapes of various kinds, with the foot divided decimally, are also used, especially in cities where precise measurements are necessary.

Custom and civil laws have decided that the length of the

boundary line of a field is not the actual distance on the surface of the ground, but that it is the projection of that distance on a horizontal plane. In like manner, the area of a field is not the exposed superficial surface, but the projection of that surface on a horizontal plane. In all land surveying, therefore, horizontal distances are to be measured, and from these the areas are to be computed.

The angle between two boundary lines of a field is the horizontal angle between their horizontal projections. Angles are measured by means of a graduated plate which can be leveled so as to be brought into a horizontal plane. Although it is possible to make complete surveys by means of the chain alone, it is much cheaper to make a number of angle measurements to be used in connection with a few measured linear distances.

The unit of angular measure is the degree, or the ninetieth part of a right angle. The degree is divided into sixty minutes and the minute into sixty seconds. In rough land surveying the angles are measured to the nearest quarter degree, in ordinary work to the nearest minute, and in triangulation they are expressed in seconds.

An arc of a circle containing 57.3 degrees, or more accurately 57.29578 degrees, is equal in length to the radius. At a distance of 1000 feet an angle of one degree subtends an arc of 17.453 feet, while an angle of one minute subtends 0.291 feet. The sine of one degree is 0.017452, and the sine of one minute is 0.000291. Thus for angles less than one degree the subtended arcs may be taken as closely proportional to their sines.

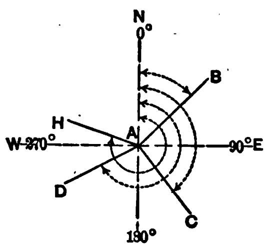


FIG. 2.

The angle which a line makes with a standard line of reference is called the azimuth of the line. The standard line is usuusually a north and south line, or meridian. In land surveying azimuths are measured from the north around through the east

south and west in the direction of motion of the hands of a clock. Thus the azimuth of the north point is 0°, of the east 90°, of the south 180°, and of the west 270°. In Fig. 2 the azimuth of the line AB is 60°, the azimuth of AC is 150°, the azimuth of AD is 250°, and the azimuth of AH is 290°. When the azimuths of two lines are known, the angle between them is found by taking the difference of the azimuths; thus $DAH = 290° - 250° = 40°$.

The back azimuth of a line is its azimuth measured at the other end with reference to a meridian drawn through that end. In plane surveying all the meridians are parallel, and hence the back azimuth of a line differs by 180° from the azimuth. For instance in Fig. 3 let the azimuth of AB be 45°, then the back azimuth is 225°. In any case the back azimuth of a line BA is the azimuth of AB, the initial letter indicating the end where the azimuth is measured. In geodetic surveying the meridians converge toward the pole, and hence the back azimuth of a line differs from its azimuth by an amount slightly greater or less than 180°; also the south is taken as the initial point, and the azimuths are measured around through the west, north, and east.

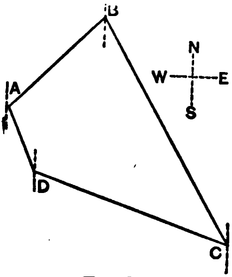


FIG. 3.

When the interior angles of a polygon have been measured and also the azimuth of one of its sides, the azimuths of the other sides are easily found. No special rules need be given for finding these, for no error can occur if a sketch be drawn in each particular case. For example, in Fig. 3, if the angle B is 75° and the azimuth of AB is 45°, then the azimuth of BC is 150°; if further the angle C is 40°, then the azimuth of CD is 290°, and so on.

Prob. 2. A polygon of six sides has the interior angles $A = 58° 24'$, $B = 121° 30'$, $C = 123° 30'$, $D = 188° 15'$, $E = 95° 14'$, $F = 133° 07'$. Compute the azimuth of each of the sides when the azimuth of AB is 0° 00′. Also when the azimuth of BC is 0° 00′.

ART. 3. LATITUDES AND LONGITUDES.

In geography the latitude of a point is its angular distance north or south from the equator, and the longitude of a point is its angular distance west or east from an assumed meridian. In plane surveying the meanings of the words are analogous, but the distances are measured in feet from any two convenient lines of reference which intersect at right angles; one of these lines is generally a north and south line or meridian. Thus in Fig. 4 let SN be a meridian and WE be a line perpendicular to it. Let A and B be the ends of the line AB, and from each let perpendiculars be drawn to NS and WE. Then a_1A and b_1B are the latitudes, and aA and bB are the longitudes of the points A and B. Latitudes of points north of WE are regarded as positive, while those of points south of it are negative. Longitudes east of NS are positive, while those west of NS are negative. Thus the point C has a positive latitude and a negative longitude.

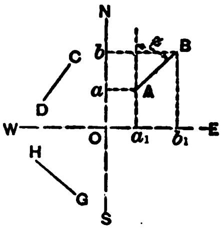


FIG. 4.

The difference of the latitudes of the ends of a line is called the latitude difference of that line; thus ab is the latitude difference of AB. The difference of the longitudes of the ends of a line is called the longitude difference of that line; thus a_1b_1 is the longitude difference of AB. In general let L_1 and L_2 be the latitudes of two points, and M_1 and M_2 their longitudes; then L_1-L_2 is the latitude difference and M_1-M_2 is the longitude difference.

When the length and azimuth of a line are known its latitude and longitude differences are found by multiplying the length by the cosine and sine of the azimuth. Thus, from Fig. 4,

$$\text{Latitude difference of } AB = ab = l\cos Z.$$
$$\text{Longitude difference of } AB = a_1b_1 = l\sin Z.$$

For example, let the length of a line be 457.69 feet and its azimuth be 279° 01′ 44″; then its latitude difference is + 71.83 feet and its longitude difference is — 452 02 feet.

When the latitude L_1 and longitude M_1 of a point are known, as also the length and azimuth of a line joining that point with another, the latitude L_2 and the longitude M_2 of the second point are

$$L_2 = L_1 + l \cos Z, \qquad M_2 = M_1 + l \sin Z.$$

The proof of these equations is readily seen from Fig. 4, taking A as the first point and B as the second.

The latitude and longitude of a line are often called coordinates, while the two standard reference lines SN and WE are called the coordinate axes, and their intersection O is known as the origin of coordinates. The latitudes and longitudes of points in the four quadrants formed by these axes have the same signs as sines and cosines in trigonometry. It is usual in land surveys to assume the coordinate axes in such positions that all the points of the survey will fall in the NE quadrant where their latitudes and longitudes are positive. Thus Fig. 5 shows a field $ABCD$ with the coordinates of each corner positive with respect to the two axes.

A line whose azimuth is known is often called a course, the word course implying a definite direction. Lines or courses running northward, or toward the top of the page, are called north courses, while those that run southward are south courses; thus in Fig. 5 the lines DA and AB are north courses, while BC and CD are south courses. Lines running eastward, or toward the right of the page, are called east courses, while those running westward are west courses; thus AB and BC are east courses, while CD and DA are west courses.

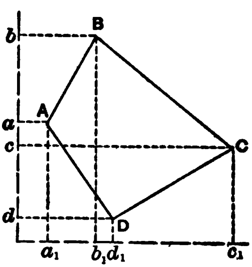


Fig. 5.

The latitude difference of a north course is positive and is called a northing, while that of a south course is negative and is called a southing; thus ab is positive, but bc is negative. The longitude difference of an east course is positive and is called an easting, while that of a west course is negative and is called a

westing; thus b_1c_1 is positive, but c_1d_1 is negative. If attention be paid to the signs of the cosines and sines of the azimuth in making the computations, the latitude and longitude differences will always come out with their proper signs. In many books on surveying the northings and southings are called latitudes instead of latitude differences, while the eastings and westings are called departures instead of longitude differences; but the plan here adopted is more in accordance with the methods of geodesy.

Prob. 3. Given the latitude of one end of a line, as $+ 2804.4$, its longitude as $+ 4661.3$, its length 797.2 feet, and its azimuth 115° 44′ 28″. Compute the latitude and longitude of the other end. (Draw a figure before beginning the solution.)

Art. 4. Areas of Triangles and Trapezoids.

The areas of fields are usually expressed in acres, square rods, and square feet, there being 160 square rods in an acre and 272¼ square feet in a square rod. In rough land surveys the area is expressed in acres, roods, and square rods, a rood being one fourth of an acre. In speaking of areas a square rod is usually called simply a rod.

The area of any triangle is equal to one-half the product of the two sides into the sine of their included angle. Thus, if a, b, c, be the sides opposite the angles A, B, C, respectively, the area can be expressed in three ways,

$$\text{Area} = \tfrac{1}{2}\, ab \sin C = \tfrac{1}{2}\, ac \sin B = \tfrac{1}{2}\, bc \sin A;$$

and if one of the angles, as A, is a right angle, the area is simply $\frac{1}{2}bc$. As an example, let $a = 22.00$ chains, $c = 13.20$ chains, and $B = 53°\ 08'$; from Table I sin B is found to be 0.80003, and then the area is 116.164 square chains, or 11 acres, 98 square rods, and 170 square feet.

When the three sides of a triangle have been measured its area may be found by the following rule: Add together the three sides and take half their sum, from the half-sum subtract each side separately, multiply together the half-sum and the three remainders, and take the square root of the product.

Or, let a, b, c, be the three sides, and s the half-sum $\frac{1}{2}(a+b+c)$; then

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}.$$

For example, let $a = 220$ feet, $b = 176$ feet, and $c = 132$ feet; then $s = 264$, $s-a = 44$, $s-b = 88$, $s-c = 132$, and the area is 11616 square feet, or $42\frac{2}{3}$ square rods.

If the latitudes and longitudes of the vertices of a triangle with respect to a meridian ON and a parallel OE are given, the area of the triangle is easily computed, it being the difference between the area of a rectangle and of three right-angled triangles. For example, let the latitudes of the points A, B, and C in Fig. 6 be 400, 250, and 100 feet respectively, and the corresponding longitudes be 500, 700, and 80 feet. Then the height of the rectangle is 300 feet and its width is 620 feet, which give 186,000 square feet for its area. The sum of the areas of the three right-angled triangles is 124,500 square feet. Hence the area of $A\ B\ C$ is 1 acre and 17,940 square feet.

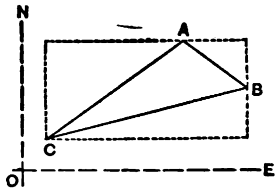


FIG. 6.

The area of a trapezoid is equal to half the sum of the parallel sides multiplied by its altitude. The trapezoids of most common occurrence in surveying have two right angles, as for instance $aABb$ in Fig. 5, whose area is $\frac{1}{2}(aA + bB)ab$. In order to determine the area of an irregular figure like that of $ABCD$ in Fig. 7, perpendiculars, or offsets, are sometimes erected upon the straight line AD and their lengths measured as well as their distances apart, the distances bc, cd, etc., being

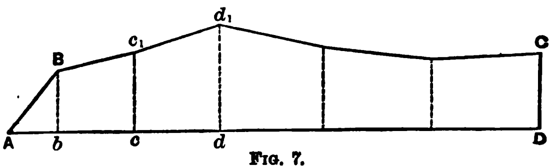


FIG. 7.

such that Bc_1, c_1d_1, etc., may be regarded as practically straight. Then the total area is the sum of the areas of the

triangle ABb, and of the trapezoids bBc_1c, cc_1d_1d, etc. This method is particularly applicable to cases where the lengths of the offsets are less than one or two chains and where great precision is not required.

The area of any polygon may be determined by dividing it into triangles. Fig. 8 shows two ways of thus dividing a six-sided field, and many others are possible. In practice it is more advantageous to measure a number of angles and a few sides, rather than all the sides of all the triangles. But a better method for computing the area of a polygon is by means of trapezoids, as explained in the next article.

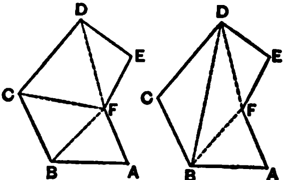


FIG. 8.

Prob. 4. Compute the area of the first diagram in Fig. 8 from the following data: $AB = 317.8$ feet, $BF = 284.3$ feet, $FA = 250.5$ feet, $FC = 512.7$ feet, $FD = 510.0$ feet, $DEF = 90° \, 00'$, $EFD = 69° \, 45'$, $DFC = 61° \, 12'$, $CFB = 49° \, 30'$.

ART. 5. AREAS OF POLYGONS.

To determine the area of a polygonal field it is customary to measure the length of each side and each of the interior angles. The azimuth of one side is also either determined or assumed; then by Art. 2 the azimuth of each of the other sides is readily found. Let $ABCDEA$ in Fig. 9 be a field in which the length and azimuth of each side is known. It is required to deduce a method for computing the area.

Let a meridian be drawn through the most westerly corner of the field, and from each of the other corners let perpendiculars Bb, Cc, Dd, and Ee be drawn to it; these are the longitudes of the corners (Art. 3). Then the area of the field is equal to the area $bBCDd$ minus the areas AbB and

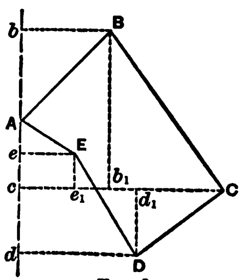


FIG. 9.

$AEDd$. The first area is formed by the two trapezoids $bBCc$ and $cCDd$, the second is the triangle AbB, while the third is formed by the triangle AEe and the trapezoid $eEDd$. Hence

$$\text{Area} = \tfrac{1}{2}(bB + cC)bc + \tfrac{1}{2}(cC + dD)cd$$
$$- \tfrac{1}{2}bB \,.\, Ab - \tfrac{1}{2}eE \,.\, eA - \tfrac{1}{2}(dD + eE)de,$$

and the double area of the field is

$$2 \text{ Area} = (bB + cC)bc + (cC + dD)cd - bB \,.\, Ab$$
$$- eE \,.\, eA - (dD + eE)de,$$

and it has been shown in Art. 3 how all the quantities in this expression can be computed.

The longitude of a point is its distance from the meridian (Art. 3); thus bB and cC are the longitudes of the points B and C. The longitude of a line or course may now be defined to be the longitude of its middle point, thus $\frac{1}{2}(bB + cC)$ is the longitude of the course BC. Hence $bB + cC$ is the double longitude of BC, or the double longitude of any course is the sum of the longitudes of its ends.

Inspection of the above expression for the double area of a field shows two facts: First, that the double area is the difference of two quantities, one being the sum of the areas of the trapezoids included between the south courses and the meridian, while the other is the sum of the areas of the trapezoids and triangles included between the north courses and the meridian. Second, that each of these areas is the product of the double longitude of a course by its latitude difference. Hence let S_1, S_2, etc., be the double longitudes of the south courses and s_1, s_2, etc., their southings, and let N_1, N_2, etc., be the double longitudes of the north courses, and n_1, n_2, etc., their northings; then

$$2 \text{ Area} = S_1s_1 + S_2s_2 + \text{etc.} - N_1n_1 - N_2n_2 - \text{etc.}$$

gives a general rule for computing the area of any polygonal field. The areas S_1s_1, S_2s_2, etc., are often called south areas, while the others are called north areas.

The northings and southings of each course having been computed by Art. 3, as also the eastings and westings, it only remains to find the double longitudes. For the first course

AB the double longitude is its easting bB. For the second course BC the double longitude is $bB + cC$, that is, $bB + bB + b_1C$. For the third course CD the double longitude is $cC + dD$, that is, $bB + cC + b_1C - Cd_1$. In general the following rule will be useful:

> The double longitude of any course is equal to the double longitude of the preceding course plus the longitude difference of that course plus the longitude difference of the course itself.

When the longitude difference is negative, or a westing, it is used with the minus sign and hence subtracted instead of added. If the meridian is drawn through the most westerly corner of the field, as in Fig. 9, all the double longitudes are positive. As a check on the work the double longitude of the last course will be found equal to its westing; thus the double longitude of EA is eE.

The following steps in the computation of the area of a polygonal field may now be enumerated:

1st. Measure the length of each side or course and each of the interior angles; these constitute the field notes. Also measure the azimuth of one of the courses, or if this is not measured assume any value for this azimuth.

2d. Compute the azimuth of each of the other courses (Art. 2).

3d. Compute the latitude difference and the longitude difference for each course (Art. 3).

4th. Compute the double longitude for each course.

5th. Multiply each double longitude by its latitude difference; call the positive products north areas, and the negative products south areas.

6th. Take the sum of the south areas and the sum of the north areas; one half of their difference will be the area of the field.

In Art. 6 a numerical example will be given illustrating the computations in full.

Prob. 5. A triangle ABC has sides with the following lengths and azimuths:

AB,	$l = 312.0$ feet,	$Z = 45$ degrees.
BC,	$l = 540.4$ feet,	$Z = 135$ degrees.
CA,	$l = 624.0$ feet,	$Z = 285$ degrees.

Compute the latitude differences, the longitude differences and the double longitudes for each course.

Art. 6. Computation of Areas.

The following are the lengths of the sides and the interior angles of a polygon as measured in surveying a field:

$$\begin{array}{llll}
AB = 816.5 \text{ feet}, & & A = & 58^\circ\ 14' \\
BC = 510.0 \text{ feet}, & & B = & 120\ \ 00 \\
CD = 204.0 \text{ feet}, & & C = & 125\ \ 00 \\
DE = 102.1 \text{ feet}, & & D = & 200\ \ 00 \\
EF = 612.0 \text{ feet}, & & E = & 83\ \ 34 \\
FA = 714.7 \text{ feet}, & & F = & 133\ \ 12
\end{array}$$

No azimuth was taken in the field, and hence for the purpose of computing the area the meridian is assumed to pass through AB, so that the azimuth of AB is 0° 00′.

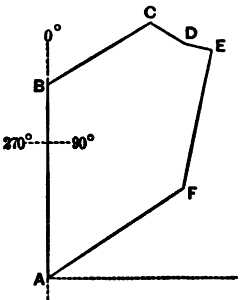


Fig. 10.

The first step is to find the azimuths of the other sides by the method of Art. 3. In general the azimuth of any course is equal to that of the preceding course, plus 180 degrees, minus the interior angle between the two courses. Thus the azimuth of BC is $0° + 180° - 120° = 60°$; the azimuth of CD is $60° + 180° - 125° = 115°$, and so on. As a check on the work the azimuth of AB computed from that of FA, should be found to be 0° 00′.

The latitude and longitude differences of the courses are next computed as follows, by Art. 3:

$$\begin{array}{lllr}
\text{Lat. Diff. } AB = 816.5 \cos & 0^\circ\ 00' & = & +\ 816.50 \\
\text{Lat. Diff. } BC = 510.0 \cos & 60^\circ\ 00' & = & +\ 255.00 \\
\text{Lat. Diff. } CD = 204.0 \cos & 115^\circ\ 00' & = & -\ \ 86.21 \\
\text{Long. Diff. } AB = 816.5 \sin & 0^\circ\ 00' & = & 0.00 \\
\text{Long. Diff. } BC = 510.0 \sin & 60^\circ\ 00' & = & +\ 441.67 \\
\text{Long. Diff. } EF = 612.0 \sin & 191^\circ\ 26' & = & -\ 121.32
\end{array}$$

In like manner all the latitude and longitude differences are computed and the results are tabulated, the positive latitude differences being northings and the negative ones southings,

while the positive longitude differences are eastings, and the negative ones westings.

Courses.	Lengths, feet.	Azimuths.	Lat. Differences.		Long. Differences.	
			Northings.	Southings.	Eastings.	Westings.
AB	816.5	0° 00′	816.50		0.00	0.00
BC	510.0	60 00	255.00		441.67	
CD	204.0	115 00		86.21	184.89	
DE	102.1	95 00		8.89	101.71	
EF	612.0	191 26		599.85		121.32
FA	714.7	238 14		376.26		607.65
		Totals......	1071.50	1071.22	728.27	728.97
		Errors.....	0.28		0.70	

Since the survey was made by a circuit from A back to A it is evident that the sum of the northings should equal the sum of the southings ; also the sum of the eastings should equal the sum of the westings. In practice this is rarely attained, but there is an error, called the error of closure, which should be adjusted before the double longitudes are computed. In this case the significance of the errors, 0.28 feet in latitude and 0.70 feet in longitude is that, if starting from A, the corners were to be accurately located from the above data, the end A' of the line FA' would fall 0.28 feet to the north of A and 0.70 feet west of it.

The error of closure is caused by errors in the measurement of the lines, or in observing the angles, or in both. However, if the sum of the interior angles of the polygon equals 180° into the number of sides minus 360°, the probability is that the error of closure is mostly due to the linear measures. As the error in measuring a line increases with its length, the error in latitude should be distributed among all the latitude differences in proportion to their lengths, one half of it being applied to the northings and one half to the southings. The error in longitude is treated in the same way. Thus in this case the errors per foot in latitude and longitude are

$$\frac{0.14}{1071} = 0.000135, \qquad \frac{0.35}{728} = 0.000481,$$

and the adjusted latitude and longitude differences are found as follows:

$$\begin{array}{lll}
\text{Northing} & AB = 816.50 - 0.000135 \times 816 = 816.39 \\
\text{Southing} & CD = 86.21 + 0.000135 \times 86 = 86.22 \\
\text{Easting} & BC = 441.67 + 0.000481 \times 442 = 441.88 \\
\text{Westing} & EF = 121.32 - 0.000481 \times 121 = 121.26
\end{array}$$

and their values are inserted in the table given below.

The double longitudes of the courses are next computed. For the course AB, the double longitude is its departure 0.00, for the second course BC it is 441.9, for CD it is 451.9 + 441.9 + 185.0 = 1068.8, and so on. As a check on the work the double longitude of the last course will be found equal to its westing. The fifth column of the table gives all the double longitudes.

Courses.	Adjusted Lat. Differences		Adjusted Long. Differences		Double Longitudes.	Double Areas.	
	N.	S.	E.	W.		North.	South.
AB	816.4		0.0	0.0	0.0	0	
BC	255.0		441.9		441.9	112 685	
CD		86.2	185.0		1068.8		92 131
DE		8.9	101.8		1355.6		12 065
EF		600.0		121.3	1336.1		801 660
FA		376.3		607.4	607.4		228 565
	1071.4	1071.4	728.7	728.7		112 685	1 134 421

The fifth step is to multiply the double longitude of each course by its adjusted latitude difference, and to place the products in the columns of double areas. Lastly each of these columns is added, and then the double area of the field is

$$1\,134\,421 - 112\,685 = 1\,021\,736 \text{ square feet,}$$

and accordingly the required area is 510 868 square feet, which is equal to 11 acres, 116 rods, and 127 square feet.

This result can be verified by making another computation in which the meridian is assumed to pass through some other side, as BC. Then the azimuth of BC will be 0°00′, that of CD will be 55° 00′ and so on. A new set of latitude and longitude projections is computed and these are adjusted in the manner explained. The double longitudes of the courses are then found and each is multiplied by its corresponding northing or southing. Lastly one half of the difference of these products will give the area in square feet, which should closely agree with the result found above.

Prob. 6. Compute the area of the above field taking the azimuth of BC as 0° 00′; also taking the azimuth of EF as 0° 00′; also taking the azimuth of AB as 90° 00′.

ART. 7. DIVISION OF LAND.

An infinite number of problems may arise in the division of a field. The simpler ones will be readily solved by the use of the principles of geometry. The more difficult ones can be solved after a complete survey of the field and the computation of its area has been made.

The first problem to be considered is that of dividing a field into two given parts by a line starting from a given point. As an example let the field whose area was computed in Art. 6 be taken, and let it be required to draw from the point D, a line DP so that the area $BCDP$ shall be 5 acres, or 217 800 square feet. The solution of the problem involves the determination of the distance AP or BP, and of the length and azimuth of the dividing line DP. (Fig. 11.)

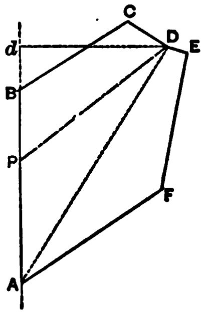


FIG. 11.

Let a line be drawn from D to the corner A, and suppose that the area $ABCDA$ can be found. Then the area of the triangle $APDA$ is known, as this is equal to $ABCDA$ minus 5 acres. The longitude dD of the point D is also known. Hence the length of AP is

$$AP = \frac{2 \text{ area of } APDA}{dD};$$

and then $PB = AB - AP$. The length and azimuth of DP are finally computed from the right triangle of dDP.

To perform the computations for finding the area $ABCDA$, the adjusted latitude and longitude differences of the courses from A to D are to be taken from Art. 6 and inserted in the new table given below. The latitude difference of the course DA is then found from the principle that the sum of the northings must equal the sum of the southings, and the longitude

Courses.	Latitude Differences.		Longitude Differences.		Double Longitudes.	Double Areas.	
	N.	S.	E.	W.		North.	South.
AB	816.4		0.0	0.0	0.0	0	
BC	255.0		441.9		441.9	112 685	
CD		86.2	185.0		1068.8		92 131
DA		(985.2)		(626.9)	626.9		617 622
	1071.4	1071.4	626.9	626.9		112 685	709 753

difference of *DA* is supplied in like manner. Completing then the computations, the area *ABCDA* is found to be 298 534 square feet. The area of the triangle *ADP* is this quantity minus 217 800 square feet, and the distance *AP* is

$$AP = \frac{2 \times 80\,734}{626.9} = 257.6 \text{ feet;}$$

whence *PB* is 558.8 feet, and hence the point *P* can be located from either *A* or *B*. The azimuth of *PD* is determined thus,

$$\tan dPD = \frac{dD}{Pd} = \frac{626.9}{558.8 + 255.0 - 86.2},$$

from which the angle *dPD* is found to be 40° 45′ nearly, which is the azimuth of *PD*. Lastly the length of *PD* is

$$PD = \frac{dD}{\sin Z} = 960.4 \text{ feet,}$$

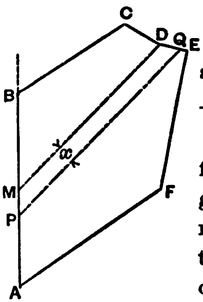


FIG. 12.

and thus the field is divided by the line *DP* so that the area *BCDP* is 5 acres.

A second problem is that of dividing a field into two parts by a line having a given direction. For example, let it be required to divide the field *ABCDEF* into two parts by a line *PQ* so that the azimuth of *PQ* shall be 45 degrees and the area *PBCDQ* shall be 5 acres (Fig. 12). First, the computation of the entire field is to be made as in Art. 6. Secondly, a line *DM* is drawn from the corner *D*, parallel to *QP*, and by the method above described the area *MBCDM* is found to be 186 224 square feet and the length of *DM* to be

886.6 feet. The area of the trapezoid $PMDQ$ is hence to be 31 576 square feet. Let x be the altitude of this trapezoid; its area is $\frac{1}{2}(MD + PQ)x$. But $PQ = MD + x \cot QPM + x \cot DQP$. Hence

$$\tfrac{1}{2}(2MD + x \cot QPM + x \cot DQP)x = 31\,576.$$

Since $QPM = 45°$ and $DQP = 50°$, this reduces to

$$x^2 + 964.2x = 34\,338,$$

from which x is found to be 34.4 feet. Then

$$MP = 34.4/\sin 45° = 48.6 \text{ feet},$$
$$DQ = 34.4/\sin 50° = 45\text{-}0 \text{ feet},$$
$$PQ = 886.6 + 34.4 - 1.8391 = 949.8 \text{ feet},$$

and lastly the distance AP is found to be 310.1 feet. Thus P and Q are located so that PQ has the azimuth 45°, and the area $PBODQP$ is 5 acres. This computation may now be checked by computing the area of $APQEFA$, which should be found to be 293 068 square feet.

Prob. 7. Divide the field $ABCDEFA$ into two equal parts by a line PQ drawn from the middle point of AB. Also divide it into two equal parts by a line PQ drawn perpendicular to the side AB.

Art. 8. Inaccessible Distances.

A common problem in surveying is to find the horizontal distance between two points when one or both of them are inaccessible. This can be solved in many ways by the application of the principles of geometry and trigonometry.

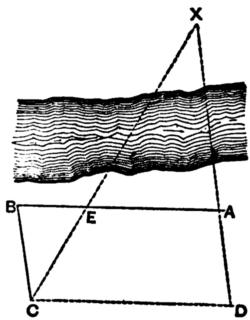


Fig. 13.

In Fig. 13 let A be an accessible point and X an inaccessible point on the other side of a river. It is required to find the distance AX by means of the chain alone. Place a point D at any convenient position in the prolongation of XA, lay off a distance AB, make BC equal to AD, and DC equal to AB, thus forming a parallelogram $ABCD$.

Mark a point E where XC cuts AB, measure AE, EB, and BC. Then from the similar triangles CBE and EXA,

$$AX = \frac{AE \times BC}{BE},$$

by which the required distance can be computed.

By the use of an instrument for measuring angles the field operations become much simpler, and indeed the method by the chain is often impracticable when AX is a long line. Let (in Fig. 13) a line AE be measured, and also the two angles A and E; then the angle X is $180° - A - E$, and

$$AX = AE\frac{\sin E}{\sin X},$$

which is the required distance. The base line AE should usually be nearly as long as the distance AX in order to secure the most accurate result, and it is also well that the angles A and E should be approximately equal.

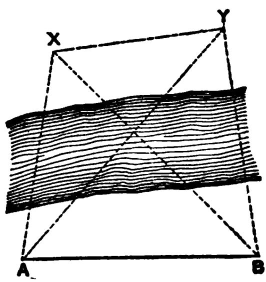


FIG. 14.

The problem of two inaccessible points is illustrated in Fig. 14. Here the distance XY is required, and for this purpose a base line AB is measured in a convenient location, and as nearly parallel to XY as practicable. At A the angles XAB and YAB are observed, and at B the angles ABY and ABX. Then in the triangle XAB,

$$BXA = 180° - XAB - ABX, \quad AX = AB\frac{\sin ABX}{\sin BXA}.$$

Also in the triangle YAB,

$$BYA = 180° - YAB - ABY, \quad AY = AB\frac{\sin ABY}{\sin BYA}.$$

Thus AX and AY are known, and the angle included between them is $XAY = XAB - YAB$; then in the triangle XAY the angles at X and Y can be found by either of the methods of Art. 1, and lastly the distance XY. As a check on the work the sides BX and BY may be computed, and the distance XY be again found from the triangle XBY.

For example, let it be required to find the horizontal distance between two spires X and Y. The base AB is laid off 406.2 feet in length, and the measured angles are $XAB = 83° 47'$, $YAB = 42° 32'$, $ABY = 76° 52'$, and $ABX = 36° 20'$. Then the side BY is found to be 315.2 feet, BX to be 466.83 feet, and their included angle is $40° 32'$. The angles BYX and YXB are next found to be $97° 26'$ and $42° 02'$, respectively Lastly, the required distance XY is 306.0 feet.

Prob. 8. In order to find the horizontal distance between the tops of two peaks a base line 5000 feet long was laid off. At one end of the line the angles between the base and the peaks were 120° and 50°, at the other end of the line they were 95° and 40°. Find the distance between the peaks, and check the computation.

Art. 9. Elevations and Heights.

The difference in level between two points on the ground which are accessible is usually found by means of a leveling instrument and a graduated rod. The level is placed in a horizontal plane by means of its bubble, and horizontal sights are taken upon the rod held vertical at each of the points. Thus in the figure to find the difference in level between A and

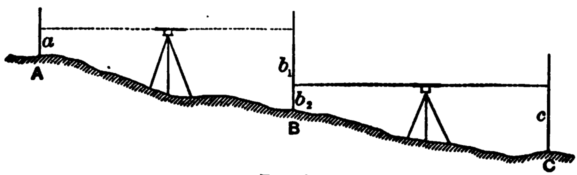


Fig. 15.

B the level is placed between them; the rod is first held at A, and the distance a is read between the foot of the rod and the point where the horizontal line through the level cuts it, the rod is next moved to B and the distance b_1 is there read; then the difference in level of A and B, or the elevation of A above B, is $b_1 - a$. When the difference of level between two points A and C is greater than the length of the rod, the level is set up twice, as shown in Fig. 15; then the difference of level between A and C is $b_1 - a + c - b_2$. This process may be con-

tinued as many times as necessary, and the difference in level between the initial and final points is then the sum of the forward readings minus the sum of the backward readings.

The elevation of a point is its height above sea level or above some datum plane. In running levels it is customary to start from some point, called a bench-mark, whose elevation is known. Thus, in Fig. 15, let the point A be a bench-mark whose elevation is 328.72 feet, and let the reading a be 0.93 feet, b_1 be 10.84 feet, b_2 be 1.03 feet, and c be 11.47 feet. Then the elevation of B is 318.81 feet and the elevation of C is 308.37 feet.

The height of an inaccessible point is usually found by the help of vertical angles together with a measured base and certain horizontal angles. Let it be required to find the height of the top of the flag-pole X above the point Y at the base of the building. In any convenient position let a horizontal base AB be measured, also let the horizontal angles

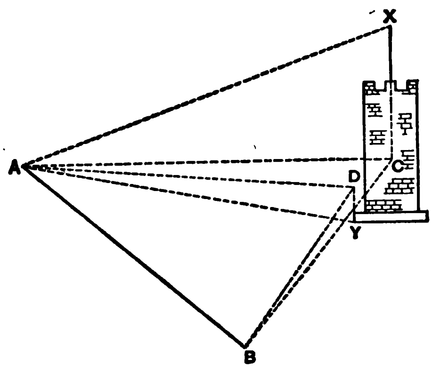


FIG. 16.

CBA and BAC be measured where C is a point vertically below X and at the same elevation as A; in reality no point C is established, but these angles are measured by pointing the instrument at X, the angle CBA being the horizontal projection of the angle XBA. The horizontal angles DBA and BAD are likewise measured where D is a point vertically above Y. At A the vertical angles XAC and YAD are also measured.

In the triangle ABC two angles and one side are now known, and from these the horizontal line AC is computed. Then in the right triangle ACX the side AC and the vertical angle at

A are known, and from these the vertical height XC is computed. Again, in the triangle ABD two angles and one side are known, from which the horizontal side AD is found; then in the right triangle ADY the vertical side DY is computed from AD and the vertical angle at A. Finally, the required height XY is the sum of XC and YD.

As an example, let the base AB be 314.62 feet, $CBA = 40° 17'$, $DBA = 38° 22'$, $BAC = 48° 40'$, $BAD = 46° 57'$, while the vertical angles at A are $XAC = 37° 18'$ and $YAD = 5° 08'$. Then the side AC is

$$AC = 314.62 \frac{\sin 40° 17'}{\sin 91° 03'} = 203.46 \text{ feet,}$$

and in like manner AD is found to be 195.80 feet. Then

$$XC = AC \tan 37° 18' = 154.99 \text{ feet;}$$
$$YD = AD \tan \ 5° 08' = \ 17.59 \quad \text{"}$$

and, lastly, the height XY is $154.99 + 17.59 = 172.6$ feet, the second decimal being omitted, as it is probably inaccurate.

In case that Y is a point on the building above the level of the instrument at A, as may often happen, then XY is the difference of XC and YD. In order to check the work vertical angles may also be observed at B.

Prob. 9. In order to find the difference in height of two peaks, M and N, a base-line AB was laid off 5000 feet long, and the horizontal angles $BAM = 120° 30'$, $BAN = 49° 15'$, $ABM = 40° 35'$, $ABN = 95° 07'$, were read. At A the angle of elevation of M was $17° 19'$, and the angle of elevation of N was $18° 45'$. Compute the difference in height of the two peaks.

Art. 10. Errors of Measurements.

All measurements are subject to errors which may be divided into two classes, systematic or constant errors, and accidental errors. Systematic errors are those that always have the same value under the same circumstances, being due to known causes; for example, if a 100-foot chain be one foot too long, all measurements made with it will be one per cent too short. Accidental errors are those that are equally likely to render the

measurement larger or smaller than the true value, being due to the combination of many unknown causes; for instance, variations in wind, imperfection of eyesight, and other similar causes render a measurement too great or too small.

Systematic or constant errors can be removed from measurements, when their causes are understood, either by a proper method of observing or by applying proper corrections to the numerical results. Methods of doing this for both linear and angular measures will be given in the following chapters.

After all the systematic errors are removed the numerical results are still affected by the accidental errors. As these are equally likely to increase or decrease the true value of the quantity they tend to balance one another, and hence if only one measurement be made it must be accepted as the most probable value. For instance, if one measurement of a line gives 618.5 feet, after the systematic errors are removed, that value must be taken as representing the true value.

When several measurements of a line are made under the same conditions each has the same degree of probability, and hence their arithmetical mean is to be taken as the most probable value; for example, if three measures of a line, made in the same manner, gives 618.5, 619.1, and 618.9 feet, there is no reason for preferring one to the other, and hence one third of their sum, or 618.83 feet, is to be taken as the most probable length.

If the three angles of a triangle are measured with equal care their sum should be 180 degrees. If this is not the case the results are to be adjusted by applying one-third of the error to each of the measured angles. So with a polygon of n sides, when the n interior angles are measured, their sum should equal $180n - 360$ degrees, and if this is not the case one-nth of the error should be applied to each of the measured values in order that their sum may equal the theoretic amount.

When the sides and angles of a field are measured the sum of the northings should equal the sum of the southings, and also the sum of the westings should equal the sum of the eastings. Owing to errors in measurement these conditions will

rarely occur, and hence an adjustment must be made, as explained in Art. 6, to remove the accidental errors.

When three angles AOB, BOC, AOC are measured at a station O with equal care, the sum of AOB and BOC should equal AOC. If this is not the case an adjustment must be made by applying one-third of the error to each angle. For example, let the measured values be $AOB = 32° 16'$, $BOC = 55° 43'$, and $AOC = 87° 57'$;

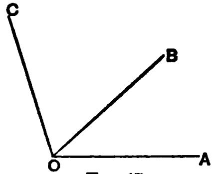


FIG. 17.

then the adjusted values are $AOB = 32° 15' 20''$, $BOC = 55° 42' 20''$, and $AOC = 87° 57' 40''$, which exactly satisfy the theoretic condition. It is always advantageous to measure the three angles even if only two are required, as thus a check is furnished on the work and opportunity is offered to eliminate the accidental errors of the measurements.

The young surveyor should always bear in mind that the results of his measurements in the field are not the true values of the quantities which they represent, but only approximate representations of the true values. He should seek to secure the greatest degree of precision consistent with the tools employed and the end in view. A large part of the land surveys in the United States has been made by rough and imperfect methods, but the time has now come when precision is demanded. Hence care must be taken to make sufficient measurements so that the work can be checked, to remove all systematic sources of error, and finally to adjust the results when possible so that the accidental errors may be largely eliminated. In precise triangulation work the adjustment of measurements is especially important, and the principles and methods for doing this constitute a branch of science known as the method of least squares.

Prob. 10. At a point O four angles are measured as follows: $AOB = 35° \ 07'$, $BOC = 60° \ 43'$, $COD = 22° \ 01'$, $AOD = 117° \ 53'$. Find their adjusted values.

CHAPTER II.

LAND SURVEYING.

ART. 11. CHAINS AND TAPES.

THE chains used in land surveying are made of steel wire and have the joints brazed to prevent opening. Iron chains are seldom used, being heavier and in every way inferior to those made of steel. At intervals of 10 links brass tags are fastened, having one, two, three, or four points, indicating distances of ten, twenty, thirty, or forty links from either end; the middle of the chain is marked by a round tag. The chain is provided, at either end, with brass handles fastened to it by a nut and screw by which the length may be changed a small amount. The length of the chain includes the handles. In using the chain care must be taken to observe whether the distance is greater or less than half a chain, as forty links and sixty links are marked alike, and thirty links from seventy links, as also twenty links from eighty links, must be carefully distinguished.

The chain is folded by bringing the 49th and 51st links together, the 48th and 52d together, and so on until the ends are reached, folding links equidistant from the middle together. To unfold the chain, hold both handles in the left hand and with the right hand throw it horizontally far enough so that it will become taut before it falls.

The chain possesses some advantages over the tape on account of its weight and strength, and because it can be more easily repaired. In chaining through brush the weight of the chain is serviceable in swinging it over the bushes and in making it straight and horizontal. If the chain is broken, a new link may be put in by the surveyor.

Steel tapes are made in various lengths up to 500 feet; those having lengths of 50 feet or 100 feet are generally used in land surveying. The best tapes of these lengths are about 0.4 inches wide and, perhaps, 0.005 inches thick: they are gradu-

ated throughout the entire length into hundredths of a foot, and often the reverse side is divided into rods and links. These tapes are easily broken, and are only used where the value of the land warrants very careful measurements; they rust easily and should be wiped dry after using, and all small spots of rust removed with kerosene.

Tapes used in common land surveying are narrower and thicker than those described above; the first foot from either end is divided into tenths, the first and last five foot spaces are divided into feet, and the tape throughout is marked every five feet. When nickel-plated these tapes require much less attention to keep them from rusting than the finer grades. In nearly every point of difference between such a tape and the best chain the comparison is in favor of the tape; one great advantage is that wear does not increase its length to the same degree as in a chain.

Metallic tapes, so called, are made of cloth, and have strands of fine brass wire interwoven longitudinally. They are divided throughout into tenths of a foot, and are very useful in making short measurements when great accuracy is not required, as in finding the dimensions of buildings, taking offsets to locate paths, brooks, and other details of topography.

To use the tape or chain, two men are required, called respectively the head chainman and rear chainman. The chain is brought into the line and made level with the rear end over the first point; the head chainman, by means of a plumb-bob, finds the spot directly under the front end of the chain, and marks it by a nail or iron pin made for the purpose. This operation is repeated till the end of the line is reached.

If pins are used there should be eleven of them. The head chainman places a pin at the front end of the chain, and this is taken up by the rear chainman after the head chainman has placed a second pin. When the last pin is in the ground the rear chainman delivers his ten pins to the head chainman and the work is continued. Each delivery, which is generally called a tally, thus indicates ten chain lengths.

In using the plumb-bob with the chain, it is best to stand

facing across the line to be measured; the string is held against the proper point on the chain with the thumb and forefinger of the right hand, and the left hand, pressing against them, helps in stretching the chain. The head chainman, after finding approximately where the point will be, should carefully clear away all leaves and grass, and prepare a smooth place on the ground, so that a slight touch of the plumb-bob may be sufficient to mark the point.

In passing along the line the rear end of the chain is allowed to drag along the ground, and just before it reaches the pin the head chainman is notified of the fact by some preconcerted signal, such as "chain" or "chain out"; much time can be saved by stopping the head chainman at just the proper time.

On steep slopes it is best to chain down hill. When the difference in elevation of the ground along the line is more than six or seven feet in a hundred feet, the head chainman carries his end of the chain out as usual and puts it in line; he then goes back to a place which is not more than six feet lower than the rear end of the chain and proceeds in usual manner, except that a part instead of the whole of the chain is used. When the measurement of one of the short divisions is completed, the rear chainman holds the proper division over the point last determined, and the operation is repeated till the front end of the chain is reached. It is unnecessary to record or even to notice the lengths of the divisions, as the end of the chain will be a chain's length from the point of beginning. This operation is called "breaking the chain."

Instead of using the plumb-bob, the horizontal distance is often found in accurate work by measuring along the surface of the ground, and afterwards determining the difference in height of points between which the measurements were taken. The length along the chain then represents the hypothenuse of a right triangle, of which required distance is another side.

A chain should be frequently compared with a standard laid off on a floor or pavement. For common work in land surveying, such a standard may be laid off by a good steel tape which has not been used. For precise work in cities the steel tape

itself should be standardized, which can be done by the department of Weights and Measures of the U. S. Coast and Geodetic Survey at Washington (see Art. 28).

Many surveyors prefer to have a chain a little longer than the standard in order to compensate for lack of level and for lateral deviations. In good work, however, these sources of error should be avoided, and the chain should agree exactly with the standard. If a chain is too long the measured length of a line is too small; thus, if the length 824.5 feet be obtained by a hundred-foot chain which is 0.14 feet too long, the true length of the line is $8.245 (100 + 0.14) = 825.7$ feet. If a chain is too short the measured length is too large; thus if the length 785.8 feet be obtained by a chain which is 0.07 feet too short, the true length of the line is $7.858 (100 - 0.07) = 785.25$ feet.

Prob. 11. A careless surveyor measured a field with a hundred-foot chain, and computed the area to be 8 acres, 12 rods, 146 square feet. It was afterwards found that the chain had lost one link, so that its true length was only 99 feet. If the computations of the surveyor were correct, what is the true area of the field.

ART. 12. THE TRANSIT.

The surveyor's transit consists primarily of two parts; the first, called the alidade, determines the line of sight, and the second, called the limb, affords means of determining the angular deviation of this line from any other. The alidade, including the telescope, the magnetic needle with its graduated circle and the vernier, is attached to a vertical spindle, and may be revolved while the limb remains stationary. The horizontal circle composing the limb is graduated into degrees, and sometimes into thirty minute or twenty minute spaces, and numbered from zero to 360 degrees in both directions. The limb is mounted upon a hollow cylindrical annulus which surrounds the spindle of the alidade. The instrument is supported by three legs, called the tripod, which are fastened together at the top by the tripod head.

The device used to measure fractional amounts of the divisions of the limb is called a vernier. Verniers are used either

on straight or circular scales, the former being employed on level rods and the latter on transits. In Fig. 18 is shown a vernier for a straight scale, where the length of the vernier is the same as the length of nine spaces of the limb. The vernier itself is divided into ten equal parts. Let a be the length of

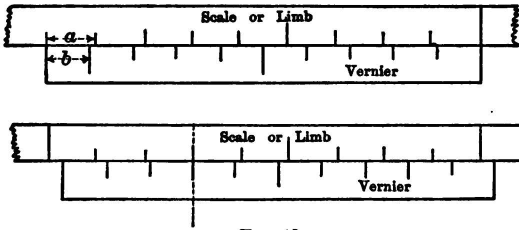


Fig. 18.

one space on the limb, and b the length of one space on the vernier. On a level rod a is $\frac{1}{100}$th of a foot, then b is $\frac{1}{10}$th of $\frac{9}{100}$th of a foot, hence

$$a - b = \tfrac{1}{100} - \tfrac{9}{1000} = \tfrac{1}{1000} \text{ feet};$$

and thus the space between the first division of the limb and the first division of the vernier in Fig. 18 is $\frac{1}{1000}$ of a foot, or one-tenth of a space of the limb.

If the vernier in the first diagram of Fig. 18 is moved until its first division coincides with the first division of the limb a distance of $\frac{1}{10}a$ or $\frac{1}{1000}$ feet has been passed over. If the third divisions coincide, as the second diagram, the vernier has moved a distance of $\frac{3}{10}a$ or $\frac{3}{1000}$ feet. Thus in moving the vernier fractional parts of the smallest space of the limb are read with precision by noting what division of the vernier coincides with a division of the limb.

If the length of the vernier is equal to 19 spaces of the limb and it is divided into 20 parts, the distance $a - b$ will be one-twentieth of one space of the limb, or a degree of precision twice as high as before. Hence a general rule for finding the smallest amount indicated by the vernier is this: Divide the value of the smallest space of the limb by the number of spaces on the vernier.

A vernier can be also made by making its length equal to 11

spaces of the limb and dividing it into 10 equal parts, or by making its length equal to 21 spaces of the limb and dividing it into 20 parts. Such an arrangement is called a retrograde vernier, and is not commonly used.

The verniers used on transits are, of course, circular instead of straight, and the divisions on the limb are degrees and fractions of degrees instead of feet, but the principles do not differ from those stated above. Such verniers are usually made double for convenience in reading angles in either direction. Such a vernier is shown in Fig. 19. Here it is seen that the zero point on the vernier, in moving from the right to the left, has passed the point *a*, which is 66° 30′, and is at *b*. By using

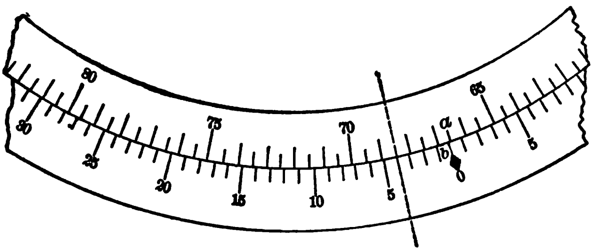


FIG. 19.

the vernier it is possible to measure the space *a b*. In the figure the limb is divided into thirty minute spaces, the vernier is of the same length as twenty-nine of these spaces, and is divided into thirty spaces. Hence the smallest amount indicated by such a vernier will be the difference between the lengths of a space on limb and on the vernier, or one minute. By referring to the figure it is seen that the fourth division on the vernier to the left of zero coincides with one on the limb, hence the zero point has moved four minutes after passing the point *a*, and the reading is 66° 30′ + 04′ or 66° 34′.

In using the double vernier the beginner may be in some doubt as to which part to use. This can be guarded against by reading that side which is farthest away from zero on the limb, in the direction that the vernier has been turned.

The precision of the work done by an instrument depends as much upon the care taken of it as upon its original excellence.

In carrying the transit to and from work, care must be taken that the tripod is firmly attached; the telescope should be turned in line with the axis of the instrument, but not too rigidly clamped; the cap should be placed over the objective and the needle lifted from the centre pin. The instrument, while being carried, is held on the shoulder by the hand just in front with the elbow close to the side; in this way there is more freedom of movement and the least liability to accident.

In setting up the instrument it is, in most cases, better to put two legs down hill and one leg up hill. The instrument is lifted bodily and set, as nearly as may be, over the point, with the plates parallel and horizontal. In bringing the transit into exactly the required position it is only necessary to remember that the plumb-bob will follow the direction in which either leg is made to move—toward it or away from it according as the leg is carried out or in. It is not well to force the tripod feet further into the ground than is necessary for rigidity; some tripods are wisely furnished with lugs to receive the pressure from the foot; thus the tripod head is relieved of much unnecessary strain.

After the instrument has been set up with the plumb-bob over the point, the next step is to level the plates. The instrument is first turned so that the bubble tubes are parallel to the lines through the two opposite leveling screws; it is then leveled by turning the screws in opposite directions; this will be accomplished when the thumbs, in turning, move either toward or from each other. The bubble will be seen to move in the direction in which the left thumb moves. After all the leveling screws are brought to a bearing on the plates by turning one screw in each pair, they should only be turned in pairs and in opposite directions; in this way the bearing upon the plates will be preserved and the screws and plates will not become strained.

Suppose the transit to be set over the point O in Fig. 17 and that it is desired to measure the horizontal angle AOB. The telescope is directed, with the vernier clamped, toward either of the points B or A, and the limb clamped; the vernier is

then read and unclamped, and the telescope is directed toward the other point, the alidade clamped, and the vernier read again. It is evident that, as the vertical plane of the telescope and the vernier are relatively immovable, the angular distance passed over by the zero point on the vernier and by the plane of the telescope are the same, or the angle *AOB*. Hence, to measure an angle, readings of the vernier are made before and after the angle is turned, and the difference is taken. In ordinary work it is usual to set the vernier at zero before turning the angle, in which case the reading after the second sight has been taken is the angle itself.

It is only necessary to follow the above directions to correctly measure any angle, but the operation can seldom be done by a beginner so that no errors are involved. It is readily seen that the accuracy of the measurement of an angle depends upon the following:

The adjustment of the transit.
Setting the instrument over the exact point it is desired to have it occupy.
The reading of the vernier.
The bisection of the points toward which the telescope is directed.
The movement of the alidade due to defects in clamping.

In land surveying where angles are only read to the nearest minute these errors should be made as small as possible by seeing that the transit is in adjustment, that it is set over the exact centre of the station, that the vernier is accurately read, that the signals sighted upon are correctly placed and truly bisected, and that care is taken in using the clamps. Directions for adjusting a transit are given in Art. 27, but a beginner should never attempt to make them until he has used the instrument sufficiently to become thoroughly acquainted with all the manipulations.

In precise work where angles are needed to fractions of a minute the last three sources of error mentioned above, as well as some others, may be largely eliminated by the method of repetitions described in Art. 28. In land surveying repetitions are unnecessary, but it will be well to check each angle by

measuring also its explement. Thus, if the angle AOB is read by pointing first on A and then on B, let the angle BOA be read by pointing first on B and then on A; the sum of the two angles should be 360° 00′.

An engineer's transit mainly differs from a surveyor's transit in having a vertical arc and a level bubble attached to the telescope for the determination of heights and elevations. Some engineers' transits have verniers reading to half-minutes, while transits for triangulation work sometimes read to twenty seconds or to ten seconds.

Prob. 12. If the limb is divided into 20-minute spaces, show how the vernier must be made in order to read one minute? in order to read 20 seconds? Give diagrams of these verniers.

ART. 13. THE MAGNETIC NEEDLE.

Most of the early land surveys of the United States were made by the compass. The compass is an instrument like the surveyor's transit, but without graduated limb and telescope; the place of the latter is supplied by vertical sights, while angles are read by bearings of the magnetic needle. All the remarks here made regarding the magnetic needle apply equally to the compass and to the transit, although in the case of the transit the needle is used less than the graduated limb and vernier.

The compass plate is usually graduated to half-degrees; the north and south points, lettered N and S, are marked 0°, and the graduation runs from each in both directions to the east and west points which are marked 90°. The letters E and W are, however, on the west and east sides respectively, of the compass plate, in order that the direction of a line as read from the end of the needle may agree with its actual direction. The direction of a line as determined by the needle is called its magnetic bearing. The bearing is expressed by two of the letters N, E, S, or W, with the number of degrees which the line varies from the magnetic meridian; thus N 35° E, which is read north thirty-five degrees east, means a line whose direction is thirty-five degrees east of north; also S 70° W indicates

a line whose magnetic direction is seventy degrees west of south.

When the bearings of several lines are taken at the same point the angles between them are known. For example, let the bearing of AC be $N\,8\tfrac{1}{2}°\,E$, and that of AD be $N\,46°\,E$, then the angle CAD is $37\tfrac{1}{2}$ degrees. Also if the bearing of AF be $S\,52\tfrac{1}{2}°\,E$, then the angle DAF is $81\tfrac{1}{2}$ degrees. The student should deduce his own rule for finding the angle from the bearings by drawing figures for a few special cases.

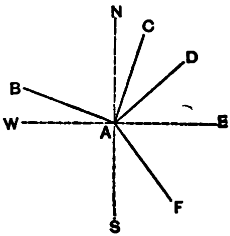


FIG. 20.

When the bearings of several courses are given the angles between them are also known. Thus, in Fig. 21 let the bearing of AB be $N\,42°\,E$, and that of BC be $S\,29\tfrac{1}{2}°\,E$; then the angle ABC is $71\tfrac{1}{2}°$. Here it is best to reverse the bearing of the first line, and thus consider both as taken at the point B where the bearing of BA is $S\,42°\,W$.

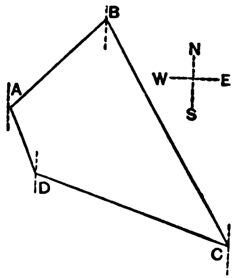


FIG. 21.

The magnetic needle is, at the best, a rough and imperfect tool for measuring angles or for determining the directions of lines. The bearings can be read to quarters or eighths of a degree, but owing to the variations to which the needle is subject, a line will have different bearings at different times. The magnetic meridian at most places deviates from the true meridian, and the angle between them is called the declina tion of the needle. On the Atlantic coast of the United States the declination is to the west of the true meridian, while on the Pacific coast it is to the east, but its amount is very different in different places, as will be seen from the isogonic map of the United States for 1915 inserted at page 128 of this Handbook. An isogonic line is a curve passing through all places which have the same magnetic meridian. Thus in 1915 the line of zero declination passes near Columbns, Ohio, and Charleston,

Ga., and during that year the magnetic meridian coincided with the true meridian at all places on that line. These isogonic lines are now slowly shifting westward.

The secular variation of the magnetic needle is an oscillatory movement by which the declination varies back and forth from a mean value. The time of this oscillation in the United States is between two and three centuries, but a complete cycle has not yet been observed. For example, at New York, N. Y., the early observations indicate that in 1657 the needle was at its extreme western declination of 9½ degrees; this slowly decreased so that about 1795 it reached the minimum value of 4½

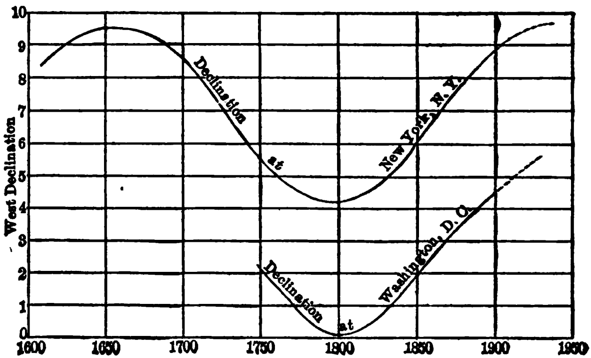


FIG. 22.

degrees; during the nineteenth century it has slowly increased and will probably reach the extreme western declination about 1933, the total period of the cycle thus being 276 years. Fig. 22 shows clearly to the eye these variations in declination, as also those at Washington, D. C., where the minimum value was observed in 1810, while the maximum will probably occur in 1927.

The value of the declination for 1915 may be ascertained approximately from the isogonic map above referred to. Its value at any date may be found for a large number of places by means of the formulæ deduced by the U. S. Coast and Geodetic Survey, and given in the report for 1895, pages 167 to 320. For example, the formula for Bethlehem, Pa., is

$$D = 5^\circ.27 + 3^\circ.05 \sin (1^\circ.46m - 34^\circ.8),$$

in which D denotes west declination and m is the number of years counted from Jan. 1, 1850. If it be required to find the declination for April 30, 1887, the value of m is 37.3 years, and then,

$$D = 5^\circ.27 + 3^\circ.05 \sin 19^\circ.7 = 6^\circ.50 \text{ west.}$$

From the formula also can be found the values and the dates of the maximum and minimum declinations. The greatest declination will occur when the angle $1^\circ.46m - 34^\circ.8$ equals 90°, as the sine is then unity; this gives $D = 8^\circ.32$ and $m = 85.5$ years, so that the time of this occurrence will probably be in the year 1935. The least declination obtains when the sine is minus unity, and this gives $D = 2^\circ.22$, and $m = -37.8$, which corresponds to the year 1812.

The daily variation of the needles is a small oscillation ranging from 5 to 10 minutes in different seasons and places. It is smaller in the winter than in the summer, and less in the southern part of the United States than in the northern part. Soon after sunrise the north end of the needle is at its most easterly deviation from the magnetic meridian. A westerly motion then begins, and about half-past ten o'clock it coincides with that meridian; the westerly motion continues until about half-past one o'clock in the afternoon when the most westerly deviation is reached. The easterly motion is then slowly resumed and by the next morning the needle again reaches its most easterly deviation. Table III, at the end of this book, gives the mean values of the daily variation for each hour of the day and each month of the year at Philadelphia, Pa., as also instructions for finding it for other places in the United States.

In addition to the secular and daily variations the magnetic needle is also subject to an annual variation of about $1\frac{1}{2}$ minutes, and to other smaller variations caused by the moon and sun. Magnetic storms cause sudden variations of considerable amount. These minor variations, however, are of little importance in land surveying, compared to the local attraction that is liable to occur in rocky regions and which often causes discrepancies of several degrees in the bearings of a line taken at points only a few hundred feet apart. The method of

eliminating the effect of local attraction is explained in the next article.

Prob. 13. The formula for the west declination at New Brunswick, N. J., is

$$D = 5^\circ.11 + 2^\circ.94 \sin (1^\circ.30m + 4^\circ.2).$$

Find the values of the maximum and minimum declinations with the dates of their occurrence. Find also the probable value of the declination on June 15, 1896.

Art. 14. Field Work.

The field work in land surveying may be divided into two classes, original surveys, and resurveys. The first class includes not only the case of lands opened for the first time for settlement, but also the staking out and division of lands, and all surveys which are made without particular reference to former records. Resurveys, on the other hand, are those made to trace boundaries that have been lost, and they require the knowledge of the former work which are either stated in deeds on maps, or in the records of towns or counties. In both cases the field work requires the measurement of such lines and angles as will enable a complete map of the property to be made, and the areas of the several portions to be computed.

A field party usually consists of three or four men, the surveyor who reads the angles or bearings and takes the notes, two chainmen, and perhaps an axman who sets the necessary stakes and poles and also assists with the tape. The poles which are used for ranging out the lines and to sight upon in measuring angles are generally about an inch in diameter, about eight feet long, each alternate foot being painted red and white, and they are pointed with steel to enable them to be easily set in the ground. In surveying a field it is an old custom for the party to go around the boundaries "in the direction of the sun," that is, so as to keep the field on the right hand. The bearings of lines can thus be written on a sketch in a natural order around the entire circuit.

It frequently happens that a surveyor is obliged to employ as chainmen men who have had no experience in such work. In

this event it is well, even after having given them full instructions, that he should be constantly with them for several hours in order to ensure that the proper degree of precision shall be attained. Chaining indeed is far more difficult to do accurately than is the measurement of angles.

The point where a transit is set for the purpose of reading angles is called a station. In the survey of a field the corners are also often called stations, these being the initial points from which the linear measurements are taken. A line whose bearing is known is frequently called a course.

If the surveyor is provided with a transit it is advised that angles should be always measured, and only such bearings be taken as are necessary to check the work or to verify former records. If he has only a compass the bearings of the lines must be taken, but care should be exercised to avoid the errors due to local attraction. Fortunately the influence of this can be eliminated by always reading the back bearings of lines as well as their forward bearings. In doing this the instrument should be set at the ends of the lines so that the back bearing of one line and the forward bearing of the next one may be read at the same station. The bearings at one point being assumed to be correct, all the others can then be adjusted so as to be relatively correct.

As an example of the elimination of the effect of local attraction let the bearing of AB be taken at A in Fig. 9, and also the back bearing of EA; then at B let the bearings of BA and BC be taken, and so on. Let the results obtained be those which are given in the second and third columns of the table.

Course.	Bearing.	Back Bearing.	Adjusted Bearing.	Azimuth.
AB	N 37° 15′ E	S 38° 00′ W	N 37° 15′ E	37° 15′
BC	S 78 08 E	N 77 45 W	S 78 53 E	101 07
CD	S 33 45 W	N 33 15 E	S 32 37 W	212 37
DE	N 14 37 W	S 15 30 E	N 15 15 W	344 45
EA	N 82 30 W	S 82 15 E	N 82 15 W	277 45

Now assume that there is no local attraction at A, then the bearing of AB and the back bearing of EA are correct. To adjust the other values proceed in order from A to B; at B the

result 38° 00′ is 45′ too large, hence 45′ must be subtracted from all SW and NE lines starting from *B* and the same amount must be added to all SE and NW lines; thus the adjusted bearing of *BC* is 78° 53′. Next the result 77° 45′ taken at *C* is seen to be 1° 08′ too small, and this must be applied to the forward bearing of *CD*, giving the adjusted bearing as S 32° 37′ W. Thus proceeding, the adjusted bearing of *EA* comes out N 82° 15′ W, and this, being the reverse of the back bearing taken at *A*, is a check on the correctness of both the field work and the adjustment.

The azimuth of each line is easily found from its adjusted bearing. If the meridian be taken to correspond with the magnetic meridian the results given in the last column of the table are the azimuths. They are found by adding or subtracting each bearing either to or from 180° or 360°, as the case may require.

The interior angles of a field are readily computed either from the adjusted bearings or from the azimuths of the lines. It is, however, no proof of the correctness of the field work if the sum of these angles equals the proper theoretic sum, for it will be found that any bearings whether correct or incorrect will give the correct amount. On the other hand if the angles be measured in the field with the transit, a valuable check is obtained by taking their sum which will only equal the theoretic sum in very good work. In such cases if no serious error is thought to exist the observed values should be adjusted by the method of Art. 10.

One of the most important details of the field work is the keeping of the notes. Nearly every surveyor has a system of his own for recording the measurements taken in the field, so no one method can be said to be the standard; the essential point is that they shall be readily legible to any person who is to use them. Better results will probably be obtained by making a sketch in the field book, showing objects in their relative positions and having the dimensions to be used in plotting marked on the sketch itself, than by a more elaborate system of symbols and abbreviations.

If the survey covers but a small area, as one or two lots of

town property, all the notes should be recorded on one sketch, which may, to make the scale larger, be extended across two pages. In the survey of a large tract it will be better to devote a page to one course; repeating, as the leaves are turned, part of the notes of one page on the next.

The notes should be made with a medium hard pencil and a straight-edge be used in drawing all lines intended to be straight. All writing should be in upright capitals, and no script should be used. Distances along the line are usually inclosed in a circle or parenthesis, and are written on a line perpendicular to the base. It will be generally more convenient to begin the notes at the foot of the page, as by so doing one can glance from the book to the field and see corresponding lines having the same direction and in front. Samples of field notes are given in Art. 15. The best books for notes have both sides of the leaves ruled alike with light-blue lines into squares about an eighth of an inch on a side. Such books are substantially bound in leather and cost about fifty cents.

Prob. 14. Find the adjusted bearings of the sides of the following field, assuming the bearing of *BC* to be correct.

Course.	Bearing.	Back Bearing.	Length in Chains.
AB	S 12° 15′ W	N 12° 30′ E	5.62
BC	N 76 45 W	S 76 45 E	3.28
CD	N 12 15 W	S 12 07 E	2.24
DE	N 47 37 W	S 48 00 E	3.05
EF	N 24 30 E	S 24 15 W	2.29
FA	S 75 15 E	N 75 00 W	6.40

Also compute the area of the field in acres, roods, and rods.

Art. 15. Survey of a Farm.

Fig. 31 is a reduced copy of a farm map plotted from the field notes of a survey. The farm is seen to comprise three divisions separated from each other by fences, and it is desired to locate the interior division lines as well as the boundaries, and also to mark the edge of the wood-land and the course of the brook.

The principal lines of the survey, usually called traverse-

lines, are measured outside or inside the boundaries according to circumstances; thus it is natural that measurement along the highway should be easier than along the inside of the fence, while another line might be more easily measured inside the boundary when the ground is there clear from trees. These traverse-lines should always be parallel and near to the boundary lines so that the lengths of the latter may be obtained with precision.

The manner of keeping the field-notes is shown in the following sketches (Figs. 23–30). On the first page of the note-book is given the date of the survey, the names of the surveyor and all his assistants, and also a sketch of the traverse-lines with letters at each station for the purpose of reference. On the second and succeeding pages of the note-book are the notes of the traverses. These are made by beginning at the bottom of the page and working upward, so that the surveyor always has the objects in the same relative position as the sketches.

The survey is begun by setting the transit over *B* and selecting stations *A* and *D*. The interior angle *ABD* is read and recorded on the margin of the page, and as a check the exterior angle is also measured and written under the first; if the sum of the two angles is within one minute of 360 degrees, the first angle is recorded on an arc between *AB* and *BD*, as shown in Fig. 24; if such agreement does not occur, the angles should be observed again. The chain is then drawn from *A* to *B*, and offsets taken with the tape to locate the ends of the boundary line and the corners of the buildings; the sides of the buildings and the width of the highway are also measured with the tape. The distances from *A* along the traverse are noted opposite to each offset, and the offsets themselves are always measured perpendicular to the traverse-line. The magnetic bearing of *AB* is taken and recorded on it, while the length of the boundary line is seen from the distances noted opposite the offsets taken at its ends.

The instrument is now carried forward to *D*, where the angle *BDE* is measured, and then the traverse-line *DE* is run parallel to the next side of the field. Thus the traverse-lines

1

Farm of George Webster
Riverside, Pa.

Surveyed by
John Doe, C.E.
September 15, 1900.

Jas. Flynn }
Wm. Roe } *Chainmen*

A. Webster, Axeman.

Declination of Magnetic
Needle 7°04′ W.

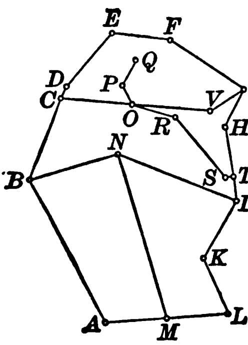


FIG. 23.

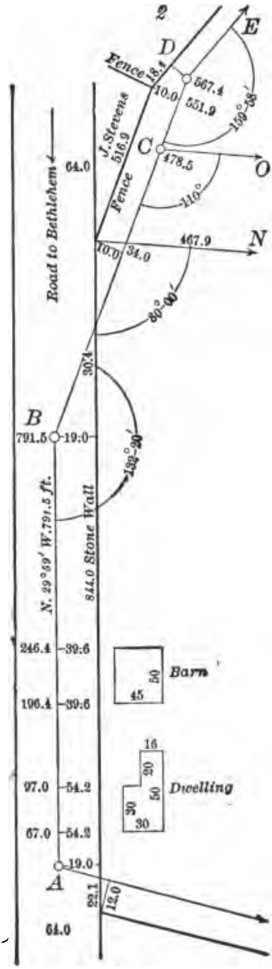


FIG. 24.

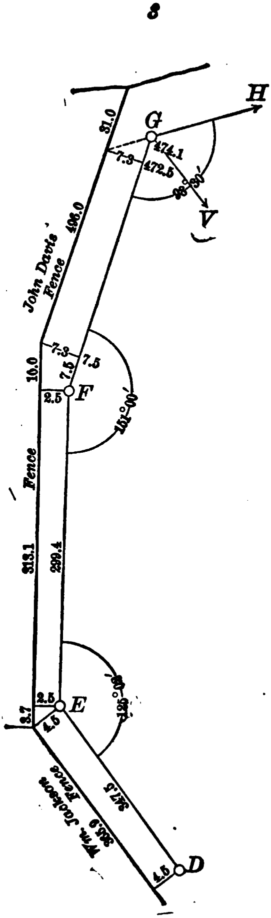

3
H
G
31.0
474.1
7.3
472.5
98° 30′
V
406.0
John Davis' Fence
7.3
7.5
7.5
10.0
2.5
F
151° 00′
Fence
313.1
299.4
2.5
E
3.7
4.6
Wm. Jackson Fence
365.9
347.5
4.5
D

FIG. 25.

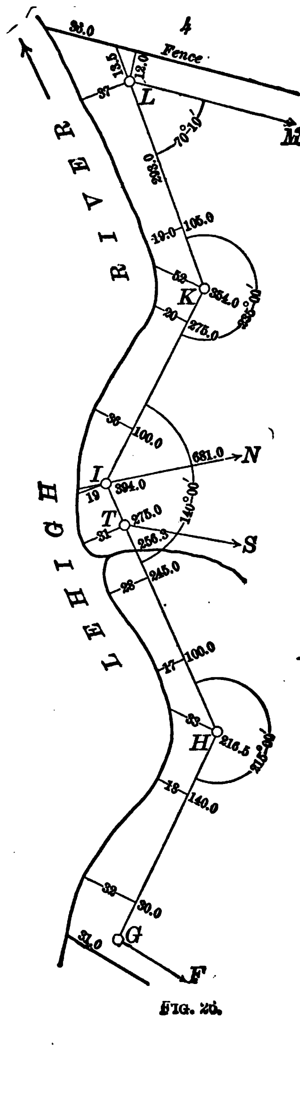

4
33.0
Fence
13.5
12.0
37
L
70°10′
M
208.0
19.0
105.0
52
K
354.0
235°00′
20
275.0
36
100.0
681.0
N
I
19
394.0
140°00′
T
275.0
31
256.3
S
28
245.0
17
100.0
33
H
216.5
215°00′
18
140.0
32
30.0
31.0
G
F
LEHIGH RIVER

FIG. 26.

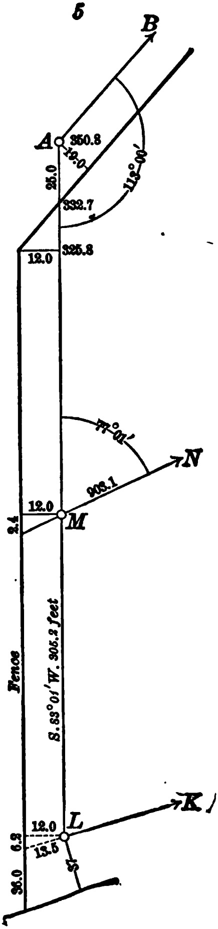

B
A
350.8
19.0
25.0
113°00′
332.7
325.8
12.0
77°01′
N
903.1
12.0
M
2.4
Fence
S.83°01′W. 305.2 feet
K
L
12.0
6.2
13.5
36.0
37

Fig. 27.

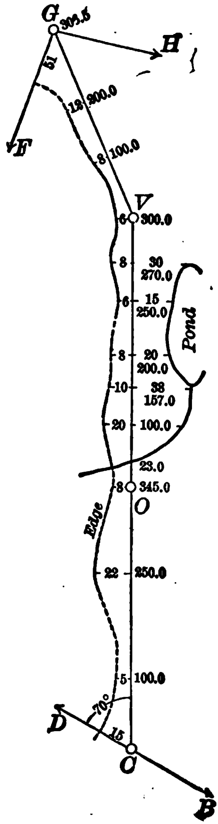
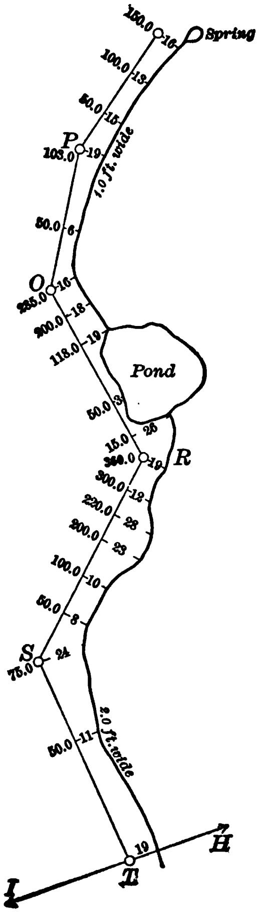
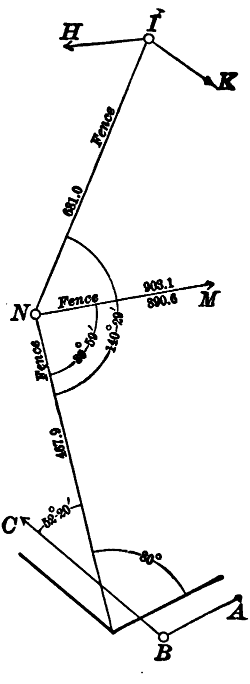

G
305.5
H
51
F
18
200.0
8
100.0
V
6
300.0
8
30
270.0
6
15
250.0
Pond
8
20
200.0
10
38
157.0
20
100.0
23.0
8
345.0
O
Edge
22
250.0
5
100.0
70°
D
15
C
B

Fig. 28.



Spring
150.0
16
100.0
13
50.0
15
P
103.0
19
1.0 ft. wide
50.0
6
O
235.0
16
200.0
18
118.0
19
Pond
50.0
3
15.0
26
360.0
19
R
300.0
12
220.0
28
200.0
23
100.0
10
50.0
8
S
75.0
24
50.0
11
2.0 ft. wide
19
H
T
I

FIG. 29.



H
I
K
Fence
631.0
N
Fence
903.1
390.6
M
140° 20′
Fence
467.9
52° 20′
C
80°
A
B

FIG. 30.

around the farm complete the polygon $ABDEFGHIKLMA$, and the interior angles of this polygon should equal twice as many right angles as the polygon has sides minus four right angles. A page of the note-book should be assigned to the description of some of the principal stations or corners of the farm, so that they may be found in case of a resurvey. The names of the owners of the adjoining fields should also be ascertained and recorded. The secondary traverse $COVG$ is run to locate the edge of the woods, while OPQ and $ORST$ locate the brook and the pond.

Great care should be taken to make the field-notes clear and complete so that they may be plotted by a person who has not seen the farm. In the above notes five angles were inadvertently omitted in Fig. 29; their values are $ITS = 114° 00'$, $TSR = 220° 15'$, $SRO = 144° 30'$, $ROP = 230° 30'$, and $OPQ = 220° 00'$. Magnetic bearings should be taken on at least two of the traverse-lines, back and front readings being made so as to detect any local attraction. The surveyor should remember that the notes should not only be sufficient to plot and describe the boundaries of the farm, but also be so complete that the area of each part or lot can be computed.

Prob. 15. Find the bearings and lengths of each of the lines of the closed traverse $MNIKLM$ from the field-notes in Figs. 28–30, and compute its area.

ART. 16. OFFICE WORK.

Office work embraces computations and the drawing of maps. The method of computing the area of a polygon has been explained in Art. 6. It is, however, rarely practicable to have the lines of the survey coincide with the boundaries of the field or farm, and hence the areas of the trapezoids between the offsets are to be separately computed as explained in Art. 8, and these are added to or subtracted from the area of the polygon, as the case may require. All computations should be checked so that the results may be relied upon.

In order to facilitate the work of plotting the map the latitudes and longitudes of the principal stations are often com-

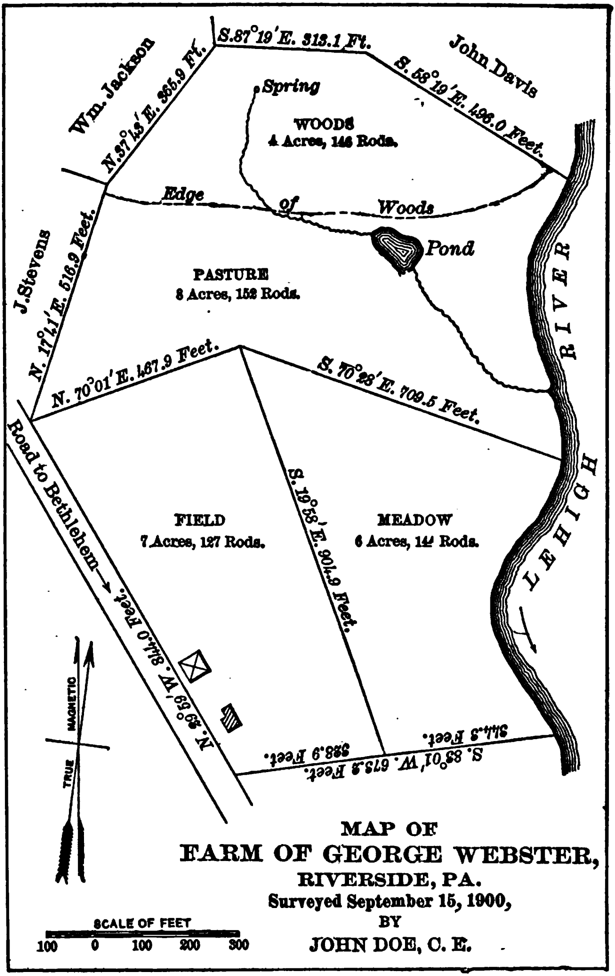

S.87°19'E. 313.1 Ft.
John Davis
Wm. Jackson
N.37°43'E. 365.9 Ft.
Spring
S.58°19'E. 496.0 Feet.
WOODS
4 Acres, 146 Rods.
Edge of Woods
J.Stevens
N. 17°41'E. 516.9 Feet.
Pond
PASTURE
8 Acres, 152 Rods.
RIVER
N. 70°01'E. 467.9 Feet.
S. 70°28'E. 709.5 Feet.
Road to Bethlehem
S. 19°58'E. 904.9 Feet.
FIELD
7 Acres, 127 Rods.
MEADOW
6 Acres, 14 Rods.
LEHIGH
N. 39°59'W. 844.0 Feet.
MAGNETIC
TRUE
S. 83°01'W. 673.2 Feet.
328.9 Feet.
344.3 Feet.
MAP OF
FARM OF GEORGE WEBSTER,
RIVERSIDE, PA.
Surveyed September 15, 1900,
BY
JOHN DOE, C. E.
SCALE OF FEET
100 0 100 200 300

FIG. 31.

puted. For example, in Art. 6, Fig. 10, it is most convenient to take the point A as the origin of coordinates. The latitude and longitude of B are then the same as the latitude and longitude differences of AB. For the station C and D,

$$\begin{aligned}
\text{Lat. } C &= 799.94 + 249.98 = 1049.92 \\
\text{Long. } C &= 0.00 + 433.07 = 433.07 \\
\text{Lat. } D &= 1049.92 - 84.53 = 965.39 \\
\text{Long. } D &= 433.07 + 181.29 = 614.36
\end{aligned}$$

and in like manner the latitude and longitude of each station is found from those of the preceding station by simply adding or subtracting the adjusted latitude and longitude differences of the line.

To plot the field to a suitable scale, one of two methods is pursued: the sides of the polygon are laid off in succession by the angle with the preceding course, and the length of the course; or each corner is located independent of all the others by means of its previously computed co-ordinates.

In plotting by the first method the angles are laid off either by the protractor, or by their natural sines or tangents. Before using the protractor the azimuths of all the courses with reference to any one of them are computed. The direction of this course is drawn and the protractor is placed in position upon it and fastened; all the azimuths are pricked off around the edge of the protractor and the latter is removed. The directions of all the courses have now been plotted and they may be transferred to any part of the paper by using triangles. The direction of any course as AB is drawn in the desired position on the paper and its length measured by the proper scale; the direction of BC as determined by the protractor is transferred till it passes through B, and the position of station C found by measuring on this line the length of BC. In like manner all the courses are plotted and the accuracy of the work is proved if the point A, plotted in order after the others, coincides with the position assumed for it at first.

To lay off an angle by means of its natural sine an arc is drawn whose radius is 10 on any scale. A chord to this arc whose length is the sine of half the angle, measured with a

scale twice as large as before, will subtend the angle at the center. Thus to plot the angle ABC of 40°, with B as a center, an arc is drawn with a radius of 10 to the scale of, say, 20 feet to the inch; with the intersection of this arc and AB as a center strike an arc with a radius 3.42 on the scale of 10 feet to the inch, cutting the first arc at C, then ABC is the required angle.

To plot the same angle by using its tangent, mark a distance 10 to any convenient scale from B toward A; at that point erect a perpendicular, whose length is 8.39 to the same scale, to C, and ABC is the angle desired.

The first method of plotting a map has the merit of being easy and rapid, but, as each point is established with reference to the preceding one, any error in the location of a station will affect the position of all that are fixed after that one, and it is to overcome this difficulty that the method by co-ordinates is used.

After the coordinates of the stations have been computed by taking the algebraic sum of the latitude and longitude projections of the preceding courses, the origin and axes of coordinates are plotted upon the paper. If the map is a large one the utmost care must be taken to make the angle between the axes exactly 90°; the right angle is first drawn in the usual way and then verified by measuring the hypothenuse of the triangle as large as the limits of the drawing will allow. Parallel to these axes lines are drawn dividing the paper into squares 100 feet, 200 feet, or 1000 feet on a side, according to the scale of the drawing, the object being to bring every point on the map within the length of the scale from two of these lines. The stations may now be located by measuring their coordinates from the nearest parallels and the accuracy tested by the length of the sides. In plotting the houses, fences, and brooks, the scale is placed on the traverse-line and all the distances along its length, to points where offsets are taken, are measured without moving it; the offsets are then measured and the figures completed.

The finished map should contain full information concerning the date of survey, scale of map, names of owners of adjoining

property, and of the surveyor; if a portion of the plan has been compiled from other maps that fact should be stated and references given. The title, meridian point, and border are, in a measure, an opportunity for the exercise of artistic skill on the part of the draftsman, but legibility and simplicity must not be sacrificed for ornament. A title of Roman letters, well done, always presents a good appearance, and without other decoration, will be in good taste on maps both large and small. The meridian is usually represented by an arrow having the head at the north end, and by an elongated *S* at the south; the lines should be very light, that the direction may be well defined. When both the true and magnetic meridians are shown, the former is represented by a full arrow and the latter by one having but one side of the head drawn. The appearance of the border is sometimes improved by geometrical figures or some simple ornament in the corners, but a departure from the practice of using simply a light line on the inside and a heavy one outside, with a space between them as wide as the heavy line, will be for the worse oftener than for the better.

Prob. 16. Compute the coordinates of the stations for Fig. 23, and plot the map of the farm on a scale of 100 feet to one inch.

Art. 17. Random Lines.

A random line is a line run out in order to find a lost corner, or to locate a boundary line which has become obliterated. For example in Fig. 32, let *A* be a given corner and let it be known from an old record that a certain line *AP* was once established having a bearing N 41° 30′ W and a length of 32 chains. No traces of this line or of the corner *P* are now visible, and it is required, if possible, to relocate them. Between the date of the old survey and the present one the declination of the needle has changed several

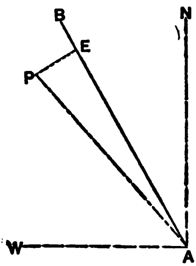


Fig. 32.

degrees, perhaps, and the first duty of the surveyor is to consider this question carefully and ascertain the probable amount

of change, so as to determine the present probable bearing of the line. Suppose that the result of this inquiry leads to N 38° 15′ W as this bearing.

Starting at the marked corner A the surveyor runs a random line AB on the bearing N 38° 15′ W, and measures along that line a distance of 32 chains, or 2112 feet, to a point B. He then proceeds to look over the ground on both sides of B for the lost corner, which is described in the old record as a marked tree, a stump, a pile of stones, or a monument. If it is impossible to find a trace of it nothing further can be done from the data in hand. If, however, it is found at P, a perpendicular PE is dropped upon the line AB and its length is measured, as also the distance BE. The distance AE is thus known, and from the right triangle the angle EAP can be computed and the present magnetic bearing of AP be determined. For example: Suppose that PE is found to be 37.4 feet, while AE is 2110.5 feet, then

$$\tan EAP = \frac{PE}{AE} = \frac{37.4}{2110.5} = 0.01772,$$

whence $EAP = 1° 01'$, and hence the present magnetic bearing of AP is N. 39° 16′ W. The distance AP is

$$AP = \frac{2110.5}{\cos 1° 01'} = 2110.8 \text{ feet},$$

which indicates, if the present work is accurate, that the old survey was in error by 1.2 feet. However, it is a principle of law that established corners and monuments must control resurveys, and hence the new record for the line AP is N 39° 16′ W 2110.8 feet.

Intermediate points on the line AP may now be established by starting at A and running it out with the new bearing. A quicker way, however, is to lay off perpendiculars from the stakes previously set on the line AE, marking their lengths proportional to the distances from A. For instance, if it be required to mark a point at the middle of AP, the perpendicular to be erected at the middle of AE will be 18.7 feet in length.

Random lines are also frequently used to find the bearing and distance between two points which are not intervisible.

For example, let G and H in Fig. 33 be two such points. Starting at G let a line GA be run in a direction which is approximately toward H. On arriving at A, where H can be seen let AH be run. Suppose that GA is N 42° 15′ E, 714.5 feet; and that AH is N 1° 08′ W, 210.5 feet. It is required to find the length and bearing of GH.

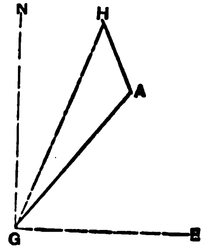


FIG. 33.

For this purpose the length of each line is multiplied by the sine and cosine of its bearing, and the results tabulated as below. The principle that the sum of the northings equals the sum of the southings, and the sum of the eastings equals the sum of the westings (Art. 7), gives 739.4 feet for the southing of HG and 476.2 feet as its westing. Dividing the second of these by the first gives the tangent of

Course.	Bearing.	Length.	Northing.	Southing.	Easting.	Westing.
GA	N 42° 15′ E	714.5	528.9		480.4	
AH	N 1 08 W	210.5	210.5			4.2
HG				(739.4)		(476.2)
			739.4	739.4	480.4	480.4

the angle between HG and the meridian, while the square root of the sum of their squares is the length of HG. Thus the bearing of HG is S 32° 47′ W, and that of GH is N 32° 47′ E, while the length is 879.5. This length can also be found by dividing 739.4 by the cosine of 32° 47′, or by dividing 496.2 by the sine of 32° 47′.

Prob. 17. In order to find the direction and distance between two points K and L, the following lines are run: KA, S 87° 37′ W, 930.57 feet; AB, West, 621.03 feet; BL, S 88° 15′ W, 82.78 feet. Compute the bearing and length of KL, and locate the point where it crosses AB.

ART. 18. RESURVEYS.

When several lines of the boundary of a farm or town have become obliterated and the corners lost, it is often necessary to make a resurvey in order to re-establish them. If the corners

can be found or be located by reliable evidence they must be accepted as correct even if the recorded bearings and lengths of the lines indicate different points. It sometimes happens that some corners can be found while others cannot. In such cases a series of random lines is to be run with the old bearings, or with the old bearings corrected for the change in declination of the needle between the two dates.

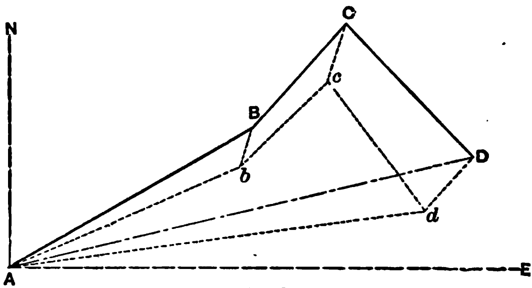


FIG. 34.

As an example let the records in an old deed give the bearings and lengths of three lines as follows:

Ab,	N 60° E,	10 chains;
bc,	N 45 E,	4 chains;
cd,	S 45 E,	8 chains.

There being no definite data at hand to determine the change in magnetic declination between the dates of the two surveys, the lines *AB*, *BC*, and *CD*, are run with the given bearings and distances from the known corner *A*. The old corners *b* and *c* cannot be found, but on arriving at *D* the old corner *d* is discovered at a point distant 20.4 links and S 12° W from *D*. It is required to locate the old corners *b* and *c*.

By the method explained in Arts. 7 and 17, the bearings and the lengths of the lines *DA* and *dA* may be computed. These are:

DA,	S 82° 47′ W,	17.29 chains;
dA,	S 83 26 W,	17.22 chains.

Now the error *Dd* between the two corners is due to two causes: first, to a constant difference in the magnetic bear-

ings of the two surveys; and second, to a difference in the lengths of the chains used. The first cause swings the polygon $AbcdA$ around the point A by a small angle. The second cause alters the lengths of the sides in a constant ratio. The difference between the bearings of DA and dA is the constant angle, while the ratio of the lengths of these lines is the constant ratio. To find the bearings of the old lines, therefore, each of the given bearings is to be corrected by the amount

$$83° \, 26' \backsim 82° \, 47' = 0° \, 39',$$

and to find the lengths of the old lines each of the given lengths is to be multiplied by

$$\frac{17.22}{17.29} = 0.996.$$

All of this reasoning supposes that the new work is done with such precision that the errors in chaining must be regarded as being in the old survey.

Applying these corrections the adjusted bearings and lengths of the old lines are

Ab,	N	60° 39′		E,	9.96 chains;
bc,	N	45	39	E,	3.99 chains;
cd,	S	44	21	E,	7.97 chains,

and with these new data the lines may be rerun and the corners b and c be located, a check on the field work being that the last line should end exactly at the old corner d.

It is, however, not difficult to compute the lengths and bearings of Bb and Cc, so that b and c may be located from the points B and C. The principle for doing this is that the polygons $ABCDA$ and $AbcdA$ are similar. Thus the triangles ABb and ADd are similar; hence the length of Bb is

$$Bb = Dd \frac{AB}{AD} = \frac{20.4 \times 10}{17.29} = 11.8 \text{ links.}$$

Also the angle ABb equals the angle ADd, or 70° 47′; hence the bearing of Bb is S 10° 47′ E. In like manner, the triangle ACc being similar to ADd, the length and bearing of Cc can be found, the length and bearing of AC being first computed. The distance Cc is 16.4 links, and its bearing is

S 15° 03′ E. The lines *Bb* and *Cc* are now run from *B* and *C*, and thus the most probable location of the old corners *b* and *c* is made.

Prob. 18. The record of an old survey reads as follows: Commencing at a post marked No. 5 and running N 62° E, 14.00 chains, to a stake marked *A*; thence running N 43½ E, 8.00 chains, to a stake *B*; thence N 5° W, 12.00 chains, to a stake *C*; thence N 72¼° E, 10.25 chains, to a stake *D*; thence S 12° W, 6.43 chains, to a stone marked No. 3. On rerunning the lines the end of the last one, instead of being at the stone No. 3, was 0.62 chains due East from it. Find the adjusted bearings and lengths of the old lines; also find the distance and direction from each station of the new survey to the corresponding one of the old survey.

ART. 19. TRAVERSING.

The term traverse, which was originally associated with navigation, is in common use by surveyors to define a series of lines whose lengths and relative directions are known. For example in Fig. 23 the lines *TS*, *SR*, *RP*, constitute a traverse run for the purpose of locating a brook. Traversing is particularly applicable to the survey of long and circuitous routes through territory presenting natural obstructions to long sights. It is almost univerally adopted in filling in the interior of maps which are based upon a system of triangulation. As examples of traversing may be mentioned the survey of highways and railroads, river banks, shores of lakes, and property boundaries. In the United States Government surveys, when the traverse is run to mark the division between private estates and a body of water retained as public property it is called a Meander Line.

The most approved method of running a traverse is that in which the graduated plate, or limb, of the transit is so set at each station that the azimuth of each line there observed can be directly read. If the survey is made in a locality where no system of latitudes and longitudes has been established, the magnetic meridian may be taken as the meridian of the azimuths. At the first station the vernier is set at zero and by

means of the lower motion the instrument is turned so that the north end of the needle points to the *N* on the compass limb. The lower plate being then clamped the upper one is unclamped; now if a sight be taken at any object the reading on the vernier will be the azimuth corresponding to the bearing of that object. The last sight and reading taken at the first station is toward the second station of the traverse line. The instrument is then placed over the second station and the vernier set at the back azimuth of the first station; the azimuth of any line from the second station will now correspond with its bearing as before. The readings of the needle are recorded as a rough check on the azimuths, with which they should agree to the nearest eighth of a degree.

For example, at the station *A* let the bearing of *AB* be N 74° 15′ E, and let its azimuth be 74° 15′. On placing the instrument at *B*, the vernier is set at 254° 15′, a sight taken on *A*, and the lower plate clamped. The azimuth of *BC* being 143° 02′, the vernier is set at 323° 02′ on arriving at *C* and the limb placed in proper position by sighting back to *B*. The telescope is not reversed during any part of the work. At each of the stations sights may be taken to surrounding objects, and if the distance to an object is measured this together with its azimuth locates it with respect to the station.

Bearing.	Azimuth.	Distance.	Object Sighted.
NOTES	AT STATION	*B*	
S 74° 15′ W	254° 15′	528.3	Station *A*
	325 42	250.	Large pine tree
	196 24		NE corner of John Doe's House
	194 10		SE corner of J.Doe's same House
S 87° 00′ E	143 02	490.7	Station *C*
NOTES	AT STATION	*C*	
N 87° 05′ W	323° 02′	490.7	Station *B*
	280 13		NE corner of John Doe's House
	276 15		SE corner of J.Doe's same House
	104 07	98 5	Fence corner
S 42° 45′ E	137 15	504.6	Station *D*

The field notes, if offsets are taken from the traverse lines are best kept as in Figs. 24–31, the bearing of a line being written upon one side of it and the azimuth upon the other side.

If no offsets are taken a form like that given above may be used. It is seen that the large pine tree is located by azimuth and distance, at station *B*, as also is the fence corner at station *C*. The house of John Doe, however, is located by azimuths taken from both *B* and *C*, the line *BC* forming a base by which its distance from either end can be computed.

It is always desirable that a traverse should have a check upon its accuracy. In a closed traverse like that around the boundaries of a farm this is obtained, since the sum of the northings must equal the sum of the southings, and the sum of the eastings that of the westings. In Fig. 23, the traverse *CNOPQG*, which begins at *C* and ends at *G*, is checked in the field on arriving at *G*, for the azimuth of *GH* must agree with that previously obtained; also in computation the differences of latitude and longitude between *C* and *G* must agree with those obtained from the main polygon.

It should be remarked that the object of taking the bearings is merely to check gross errors in the azimuths during the progress of the field work, and that an experienced engineer will usually prefer to take but few readings of the needle. If a true meridian has been established in the neighborhood of the survey the azimuths should be reckoned from it instead of from the magnetic meridian.

Prob. 19. Compute from the above notes the length of the west side of John Doe's house. Obtain the same distance without computation by plotting the notes.

Art. 20. United States Public Land Surveys.

The system adopted by the United States Government on May 20, 1785, for the survey of the public land which had been acquired from time to time, consists in dividing it into squares, called townships, six miles on a side, by meridians and east and west lines. A north and south row of townships is called a range. The townships are divided into square miles, called sections, which are subdivided into half and quarter sections.

The work of surveying the government land is begun by

carefully running a north and south line, called the principal meridian, and an east and west line called the standard parallel. Standard parallels and accurate guide meridians are run to divide the territory into 24 mile squares, and the principal meridians are at long intervals—100 miles or more. On these lines every mile is marked by a stake or monument and called a section corner; every sixth section corner is called a township corner and is differently marked.

On the standard parallel the township corners are next marked; from each of these marks range lines are run to intersect the standard parallel next north. Owing to the convergence of meridians toward the pole, the points of their intersections with the standard parallel will not be at the township corners, but a little nearer the principal meridian; as the full six miles have been measured on the standard parallels, the convergence is corrected at each of those lines.

From the township corners on the principal meridian, east and west lines are run joining the range lines already fixed. The townships thus marked are six miles north and south by six miles, less the meridional convergence in the distance to the standard parallel, east and west.

Parallel to the eastern boundaries of the several townships, section lines through the section corners are run for five miles, then from the points where they intersect the fifth east and west section lines, oblique lines are run to the points previously established on the northern boundary of the township; when, however, the northern boundary of the township is one of the standard parallels, the section meridians are run directly the full six miles instead of deflecting at the fifth east and west line.

The convergence of the meridians is given, very nearly, by the following rules of geodesy:

The angular meridional convergence equals the difference in longitude into the sine of the latitude.

The linear convergence equals the distance along the meridian into the sine of the angular meridional convergence.

The townships are divided into 36 sections, numbered from

1 to 36, as shown in Fig. 35. The sections themselves are subdivided and designated as in Fig. 36; *a* represents the various ways of dividing an entire section, and *b* shows the method when a portion of the section is obstructed by water. In cases of this kind it is usual to add to an adjacent lot the salable part of the obstructed quarter section, and to state the total number of acres in both; but when only a small portion of the quarter section is unsalable it retains its own name, is called fractional, and the number of acres in it are given.

6	5	4	3	2	1
7	8	9	10	11	12
18	17	16	15	14	13
19	20	21	22	23	24
30	29	28	27	26	25
31	32	33	34	35	36

N

S

FIG. 35.

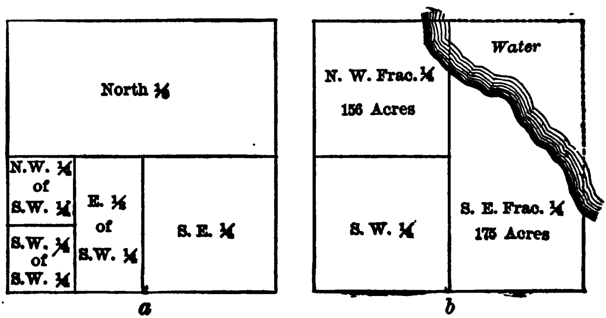


FIG. 36.

The methods of running the principal meridians and standard parallels are founded on the science of geodesy. The rules governing the running of township and section lines may be found in "Instructions to the Surveyors General of Public Lands," issued by the Land Office of the Interior Department, Washington, D. C. The principles of this chapter and the last are, however, directly applicable to the surveying and mapping of townships, sections, and their subdivisions.

Prob. 20. Compute the length of the northern and southern boundaries of a township in latitude 46° 30′, the southern boundary being 18 miles north of a standard parallel.

CHAPTER III.

LEVELING AND TRIANGULATION.

ART. 21. THE LEVEL.

The Engineer's Level consists of a line of sight parallel to a spirit level and perpendicular to a vertical axis. The line of sight is fixed in a telescope by cross-hairs as in the transit. The spirit level is attached to the under side of the telescope and is protected except on top by a metal tube. The telescope is supported on vertical forks, called Ys (from which fact the instrument is called the Y level), and is clamped to them by collars which may be raised, allowing the telescope to be turned on its axis or taken out entirely. The Ys, which may be lengthened or shortened by screws for the purpose, are fastened to a horizontal bar which is rigidly attached to the vertical axis. The instrument is provided with leveling screws and mounted upon a tripod.

The Dumpy Level differs from the ordinary form in having the telescope firmly fixed on the horizontal bar so it cannot be turned either on its axis or end for end. This level is superior to the Y type in every point of difference, being less costly, lighter, and more permanent in its adjustment. The superiority claimed for the Y level is the ease of adjustment by means of its movable telescope, but if such an advantage exists it is extremely slight.

The parts of the level of most importance are the telescope and the bubble. The character of the work to be done will determine whether or not magnifying power in the telescope is more desirable than illumination of the field of view and what was said on this subject in connection with the transit applies as well to the level. The upper part of the inside surface of the bubble tube is carefully ground in the form of a longitudinal circular curve, and upon the radius of this curve depends what is known as the sensitiveness of the level. If the radius of curvature of the bubble is large it will be very sensitive;

that is, a slight vertical displacement of the telescope will cause a considerable motion of the bubble. If the radius of curvature is short the bubble is not sensitive. A very sensitive bubble is not desirable since much time will then be lost in leveling the instrument.

The level rod is a graduated scale for measuring the vertical distance between the horizontal plane through the line of sight and that through the point upon which the rod is held. Target rods are used in precise work, and self-reading rods in cases where elevations need to be determined only to tenths of a foot. The target rod has a vernier on its movable target by which readings to the thousandth of a foot are taken by the rodman ; the New York rod, the Boston rod, and the Philadelphia rod are the most common forms in use. Self-reading rods have figures and graduations distinct enough to be read by the leveler as he sights through the telescope. A self-reading rod is divided into tenths of a foot, but if the figures are properly made readings to hundredths of a foot can easily be taken ; the numbers marking the tenths should be 0.06 feet long and so placed that half the length is above and half below the line. The numbers marking the feet are 0.10 feet long, and each is bisected by the foot-mark.

Prob. 21. Sketch a part of a target rod showing a vernier reading 5.027 feet. Sketch a self-reading rod according to the above directions.

Art. 22. Adjustments of a Level.

The adjustment of an instrument consists in bringing the various parts into their proper relative positions so that all the geometrical conditions necessary for good work may be observed. When an instrument is received from the maker it should be in perfect adjustment, and with proper care it will remain so for a long time. It should, however, be examined at frequent intervals, and if found out of adjustment at any time, should be at once put into proper condition. The following description of the adjustments of the Y level follows the order in which they should be made.

Parallax.—This is an improper condition of focusing due to the fact that the image does not fall in the plane of the cross-hairs. To ascertain if it exists, direct the telescope upon the sky and focus the eyepiece so that the cross-hairs are perfectly distinct. Then turn the telescope upon the object which is to be observed, and focus the object glass until the image is perfectly distinct. Move the eye from side to side and note whether there is any apparent movement of the cross-hairs and image. If any is seen the two operations are to be repeated until all parallax is removed. This adjustment depends upon the eye of the observer, and when made for one person may not be correct for another.

Collimation.—The line of sight, or collimation, should not deviate from the optical axis of the telescope. To ascertain if an error in collimation exists, loosen the collars on the Y's and focus the telescope upon a distant object. Slowly revolve the telescope in the Y's and note whether the intersection of the cross-hairs remains on the same point. If the horizontal hair deviates from the point adjust it by moving it over half the apparent error, by means of the capstan screws on the top and bottom of the telescope. If the vertical hair deviates adjust it by moving it over half the apparent error by means of the capstan screws on the sides of the telescope. The instrument is, of course, to be clamped while making this adjustment, but it need not be leveled.

The Attached Bubble.—The level bubble attached to the telescope must be parallel to the line of sight. To ascertain if this is the case, span the collars, carefully level the instrument and clamp it; lift the telescope out of the Y's, turn it end for end, and replace it. If the bubble does not settle in the middle turn the screws above and below one end of the bubble-tube so as to bring the bubble half way back. Next see if the bubble is in the same plane as the telescope by slowly revolving the latter in the Y's and noting whether the bubble runs away from the middle; if it does correct half the apparent error by the screws on the sides of the other end of the bubble-tube. Repeat these operations until perfect adjustment is secured.

The Horizontal Bar.—The telescope and level-bubble should be parallel to the horizontal bar supporting the Y's, or perpendicular to the vertical axis of the instrument. To ascertain if this is the case after the preceding adjustments have been made, level the instrument and revolve it 180 degrees on the vertical axis. If the bubble runs toward one end, the Y on that end is too high, and the screws at the end of the horizontal bar are moved so as to correct one half of the apparent error. Then repeat the operation until the bubble remains in the middle of the scale for all positions of the telescope.

In adjusting an instrument great care must be taken not to turn the screws too tight, as by so doing the threads soon become injured. No student or beginner should be allowed to adjust a level or transit until he has become well acquainted with all its parts by actual use. The parallax adjustment, however, is an exception, since this varies for different eyes, and each student should see that this is made every time he uses the instrument.

The dumpy level cannot be adjusted by the above methods since the horizontal bar and telescope are rigidly connected. Both the bubble and the horizontal cross-hair are, however, movable. It is necessary, (*a*) that the bubble should be perpendicular to the vertical axis and (*b*) that the line of sight should be parallel to the bubble. The adjustment (*a*) is made exactly like that above described for the horizontal bar of the Y level. The adjustment (*b*) is made by the peg method of Art. 26, except that the horizontal cross-hair is moved instead of the bubble.

Prob. 22. Give the reasons for each of the adjustments of the Y level.

Art. 23. Comparison of Levels.

In buying an instrument it is desirable that the surveyor should be able to make such an examination as will indicate whether it is a good one of its class or whether it is the kind that he needs. The following tests, which are useful in addition to those of the last article, will be found valuable in

selecting an instrument, or in comparing one with another. In making them the instrument should be in good adjustment.

Magnifying Power.—The magnifying power of a telescope may be obtained by dividing the focal length of the object glass by that of the eyepiece. As these, however, cannot be closely measured the following method is usually preferable: Place a rod, on which the divisions are very plainly marked, about 25 yards from the instrument and focus the telescope upon it. Turn the line of sight slightly away from the rod and focus the other eye upon it. Slowly turn the telescope again toward the rod, when the small image as seen by that eye will appear projected upon the larger one seen through the telescope. If, for instance, 100 divisions seen by the naked eye appear to cover 5 divisions seen by the other eye through the telescope, then the magnifying power is $100 \div 5 = 20$. A high magnifying power implies a small field of view and hence is not desirable. For a surveyor's transit or level a magnifying power of from 15 to 20 is sufficient; for an engineer's transit it should be from 20 to 25, and for an engineer's level perhaps from 25 to 30.

Spherical Aberration.—This is a defect caused by combining lenses of different curvatures, so that objects on the sides of the field of view are seen less distinctly than those in the center. To test the object glass for this defect, cover the outer edge with an annular ring of paper and focus upon a distant object; then remove the ring and cover the central part of the glass; if no change of focus is needed the glass has no spherical aberration. To test the eyepiece, sight to a heavy black line drawn on white paper and held near the side of the field of view; if it appears perfectly straight the eye glass is a good one.

Chromatic Aberration.—This is a defect caused by combining lenses of improper varieties of glass so that yellow or purple colors appear on the edges of the field. To test a telescope for this defect, focus it upon a bright distant object and slowly move the object glass out and in; if no colors are observed around the edges of the field of view the telescope is free from this defect.

Definition.—The ability to show images with sharp, clear outlines is a valuable quality in a telescope. It may be tested by comparing the distinctness of the image with that of the object as seen by the eye at such a distance that it will seem the same in size as the image. Ordinary print when read by the eye and through the glass with equal ease should appear equally distinct.

Size of Field.—The angular diameter of the field of view is usually about one degree. The value for any telescope may be closely obtained by laying off a distance of 57.3 feet from the object glass, placing two pins in the ground at the extreme sides of the field, and measuring the distance between them in feet; this will be the size of the field of view in degrees. (Art. 2.)

Sensitiveness of Bubble.—For very fine work the radius of curvature of a level bubble should be about 100 feet, for ordinary good work 50 feet is preferable, and for common work 25 feet will do. To determine this radius let the instrument be set up and leveled, so that two screws will be in the line of sight to a target rod placed 100 feet or more away. Let one end of the bubble be made to coincide with one of the division marks at a and a reading be taken on the rod at A. Then by the two screws let the telescope be raised in a vertical plane until the end of the bubble reaches the next division at b, when a second reading is taken on the rod at B. Now, if R be the radius of the level bubble and D the distance from the instrument to the rod, $R : D :: ab : AB$ very nearly. The distance AB is the difference of the readings on the rod, while ab is the length of one space of the bubble scale; thus D is known. For example, let the rod be 150 feet from the instrument, the two rod readings be 3.704 and 3.745 feet, and the bubble scale have 8 spaces in one inch, one space thus being $\frac{1}{96}$ of a foot long. Then

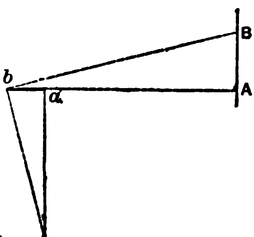


FIG. 37.

$$R = \frac{D \times ab}{AB} = \frac{150}{0.041 \times 96} = 38.1 \text{ feet,}$$

which is the radius of the level bubble. The operation should now be repeated using a different distance *D*, and the mean of several results be taken as a final value.

Prob. 23. A level bubble has a radius of 125 feet and its scale has 10 spaces in an inch. What error in leveling will result at a distance of 250 feet if the bubble is 1¼ spaces out of level?

Art. 24. Leveling.

A Level Surface is that of a fluid at rest, and a Level Line is the intersection of such a surface with a vertical plane. The line of sight through the telescope of a properly leveled and adjusted leveling instrument, when revolved around the vertical axis, generates a plane which, for short distances, practically coincides with the level surface through the instrument.

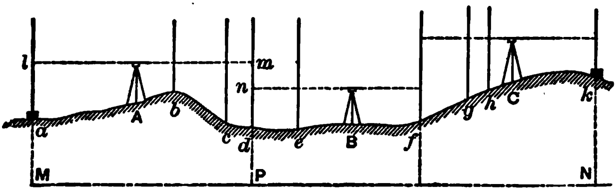


Fig. 38.

The amount of deviation between the two surfaces, due to the curvature of the earth and to refraction, varies as the square of the horizontal distance from the instrument and at one mile is about .57 feet.

The field work of leveling consists in finding the relative elevations of two or more points. The elevations are referred to an assumed surface called the Datum Plane, or simply Datum, which is so selected that all points whose elevations are required shall be above it. A mean sea level is frequently taken as the datum plane. A Bench Mark is a monument, rock or other permanent object whose elevation above the datum has been determined. The method of carrying on the field work can best be explained by Fig. 38. The line *MN* represents the datum plane; *a* is a bench mark whose elevation is known; *b, c, d, e, f,* are points whose elevations are desired;

A, B, and C are the successive positions of the instrument. The positions of the rod are indicated by the vertical lines and the lines of sight by the horizontal dotted ones. The instrument is leveled at A and the reading al, on the bench mark at a, is taken; this is called a Back Sight and is added to the elevation Ma, to get the Height of Instrument. The rod readings at b, c, and d, subtracted from the height of instrument will give the elevations of those points above the datum MN; such readings are called Fore Sights. If the distance Ad is as far as can be seen, the rod is kept at d, which is called a Turning Point; the instrument is carried forward to B, and the back sight dn is taken; the new height of instrument is then $Pd + dn$, and fore sights at e and f, are taken to determine the elevations of the stations e and f. The instrument may then be carried forward to C and the elevations of g, h, and k determined in a similar manner. If the instrument is always set midway between the turning points, the errors in rod readings, due to the non-adjustment of the instrument and to the curvature of the earth, will be confined to the intermediate points as b, c, and e; this fact should always be remembered as upon it depends, in a great measure, the accuracy of the work. The turning points are not necessarily taken at places whose elevation is desired, but may be at any convenient location, either on or off the lines; they should be so selected that an unobstructed view of the rod may be had from any probable position which may be selected as the next place for the instrument, and be upon firm objects which cannot be readily disturbed while the instrument is being carried forward.

The field notes are kept as shown below; they are usually on the left-hand page of the note book while the opposite page is devoted to remarks. The first column gives the name or number of the point where the rod is placed; such a point is called a Station. If the stations are in a continuous line, as along the middle of a road, the distances between them are given in the second column. The back sights are given in the next column; then the height of instrument, foresight, and elevation, in the order named. This arrangement will be found most convenient in making the additions, for the height of instrument and

the subtractions for the elevations. It is seen that the rod is read to thousandths of a foot on the bench marks and turning points and to hundredths of a foot on the other points. In work of less precision than that in towns and cities the rod

Station	Dist.	B.S.	H.I.	F.S.	Eleva.	Remarks.
a	0	6.320	590.994	-	584.674	Bench mark on monu-
b	150			2.12	583.87	[ment No. 51.
c	200			6.38	584.61	
T.P.*d*		3.561	584.243	10.312	580.682	On rock 50 ft. N.E. of *c*
e	280			1.20	583.04	
T.P. *f*	400	10.617	594.317	0.548	583.700	On rock.
g	475			5.82	588.50	
h	500			4.16	590.16	
k	584			3.245	591.072	B.M. on stump oak tree

readings are frequently taken only to hundredths on the benches and turning points and to tenths on the others. The final elevation of the bench mark k may be checked thus:

$$584.674 + 20.498 - 14.100 = 591.072$$

in which 20.498 is the sum of the back sights on the benches and turning-points and 14.100 is the sum of the fore sights on such points. (Art. 9.)

When levels are run merely to find the difference in elevation of two points a and k (Fig. 38) the column of distances is not needed in the notes, and there are no intermediate stations b, c, e, g, h. It is well, even in such cases, to fill out the column of height of instrument in the field, and to check the final result in the manner indicated above. The main note book is always kept by the leveler, but the rodman should also keep a book in which he records all readings on benches and turning points, finding their elevations and the heights of instrument so as to check the computations of the leveler.

Prob. 24. Explain, with a diagram, why it is that precision in levelling is promoted by setting the instrument midway between the turning points.

Art. 25. Contours and Profiles.

In Art. 2 it was stated that the dimensions of a field are the horizontal projections of the actual boundary lines and that

the area is that included between the projections of the boundaries. It is evident that a map made under these conditions, while giving a clear idea of the shape and size of the property, will convey no information as to the character of the surface, whether high and uneven or flat and low. These distinctions would be evident if the elevations of very many points in the field were written at the proper places on the map, but so many figures would render other features of the map indistinct, and hence another plan of indicating the elevations has been adopted. If the surface of the ground were cut by a series of horizontal planes at equal distances apart, the intersection of each plane and the ground would be an irregular line connecting all points having the elevation of that plane. These intersections called Contour Lines, are plotted on the map and show at a glance the elevations and slopes of all parts of the field with a precision dependent upon the nearness of the planes to each other. A clear conception of the utility of the contour lines as the means of judging of the features of a surface is formed by considering the surface of a lake as the intersecting plane. The shore line is the contour having the elevation of the surface of the lake; if the water were to fall a certain distance, the horizontal movement of the shore line would depend, not only upon the vertical fall of the surface of the water, but also upon the declivity of the ground, being small where the latter is steep and great where it is nearly flat. Hence the slope of the ground is judged to be abrupt where the map shows the contour lines near together, while the slope is slight when they are far apart.

The position of the contour lines is not generally located in the field, but elevations are taken at points where the slope of the ground changes, or often at stakes set at regular intervals by the transit and chain. These elevations are then plotted in pencil on the map and the positions of points at the elevation of any contour are found by interpolating between two plotted elevations one of which is above and one below the required point; the contour lines are then drawn by connecting points of equal elevation by a curve; the elevation of the contour is marked on it and the plotted figures erased. Let the field

ABCD, Fig. 39, be divided into squares 100 feet on a side and elevations taken at all the corners as shown, and let it be required to locate the even ten-foot contours. Beginning at any, as the upper right-hand corner, the ground along the upper line is seen to fall from elevation 133 to 122 in 100 feet, hence the 130 foot contour is $\frac{3}{11}$ of the length of the square from the corner, and the 120 foot contour is seen to be $\frac{2}{12}$ of the distance from the second corner toward the third. In like manner all the lines are gone over and the contours are then sketched in.

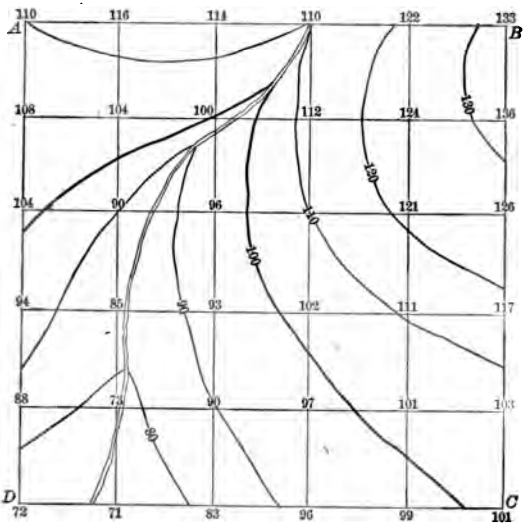


FIG. 39.

If the ground is very uneven many complications will arise in drawing the contours from the plotted elevations, and the following general rules will be useful in preventing errors: Contour lines never cross each other; every contour on one side of the map must either be found on one of the other sides, or a second time on the first one; a contour not crossing any side of the map is one continuous line, returning into itself; a contour line never branches, forming a loop; the number of contours between two others whose elevations are alike is either two, four, or some other even number.

The intersection of the surface of the ground by a vertical surface is called the Profile along that line. The profile is made by taking the elevations at known intervals along the desired course with the level; these intervals are plotted to any suitable scale, and at each point where an elevation was taken an ordinate is laid off whose length is the elevation at that point. The utility of the profile is increased by making the vertical larger than the horizontal scale, as by so doing the relative differences in elevation are made much more apparent. The profile is very important in determining the grade and the probable expense of building streets, railroads, sewers and drains. In the case of a street profiles of the middle and side lines are plotted together, using ink of different colors if necessary to distinguish the three lines, and the suitable position for the finished grade is selected; profiles at right angles to the street line, or cross-sections, at suitable distances, as every 50 feet, are plotted, and on them is marked the position of the grade line; the area between the latter and the surface indicates the amount of excavation or embankment necessary.

The profile of any line on a contour map can be drawn without any additional field work, since the elevations of the intersections of the line and the contours are known from the height of the contours themselves. Thus the profile of a line through the middle of the upper row of squares in Fig. 39 would be made by first drawing the line in pencil across the map, then the elevation at the right end is 130; at about 115 feet, going toward the left, the elevation is 120; 70 feet further 110; and so on across the map. The vertical distances on a profile are usually plotted on a scale from 5 to 20 times as large as the horizontal scale.

Prob. 25. Draw the profiles of the ground along the lines *AB* and *CD* in Fig. 39, making the vertical scale ten times the horizontal scale. Draw also the profile on the line *BC*.

Art. 26. Adjustments of a Transit.

The adjustment of the telescope for parallax, described in Art. 22, must be made every time it is used. With care in

handling the following additional adjustments of the transit will only need attention at rare intervals, but the instrument should be frequently tested to see if it is in order.

Plate Bubbles.—The plane of each small level bubble must be parallel to the horizontal plate. To find if this is the case, carefully level the instrument, turn the alidade through about 180 degrees, and note whether the bubble is still in the middle of the scale. If not, move the capstan screws at the end of the bubble tube until one half the apparent error is corrected. Then level the instrument again and repeat the operation. The other plate bubble is adjusted in the same way.

Collimation.—The line of sight must be perpendicular to the horizontal axis of the telescope. To find if this is the case, set up the transit on nearly level ground and sight on a well-defined distant object, reverse the telescope and place a pin about 300 feet from the instrument in the opposite direction; revolve the alidade, sight to the same object, reverse the telescope, and note if the line of sight strikes the pin. If not, set another pin in the line of sight by the side of the first, measure the distance between them and place a third pin at the middle of that distance. Then turn the capstan screws on the side of the telescope until the vertical cross-hair has moved one half the distance from the second to the third pin. Next pull up all the pins and repeat the operation until adjustment is secured.

Horizontal Axis.—The horizontal axis of the transit telescope must be parallel to the horizontal plate, or in other words the standards must be of equal height. To find if this is the case, level the plate bubbles, elevate the telescope as high as practicable and sight to a sharply defined object, depress the telescope and mark a point on the ground at about the same elevation as the instrument; then reverse the telescope, take another sight upon the same object and mark another point on the ground. If these points do not coincide, move the screws at the top of one of the standards until the vertical hair bisects the distance between the points. Next repeat the operation until the adjustment is perfect.

Attached Bubble.—The attached level bubble must be paral-

lel to the line of sight of the telescope. To ascertain if this is the case, set up the instrument and level the telescope; drive a stake A about a foot from the plumb-bob, hold a level rod upon it, and take the rod reading a_1 by sighting through the large end of the telescope, or by measuring to the end of the middle of the axis of the telescope. Drive another stake B about 400 away and take the rod reading b_1. Next set the instrument as near B as possible, take the rod reading b_2 upon it, and the rod reading a_2 upon A. Now if $a_1 - b_1$ equals $a_2 - b_2$, the lines of sight are horizontal, and the attached bubble is in ad-

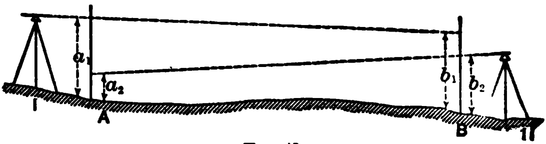


FIG. 40.

justment. If not, without moving the level, set the rod on the stake A, clamp the target so that the rod reads

$$\tfrac{1}{2}(a_1 + a_2 + b_2 - b_1),$$

set the horizontal cross-hair on the target, and then move the bubble into the middle of the tube by the screws for that purpose at the end. The operation is then to be repeated until perfect adjustment is secured. This is called the peg method of adjustment.

Vertical Arc.—After the preceding adjustments are made, the vernier of the vertical arc should read 0° 00′ when the attached bubble is level. If this is not the case, the vernier may be moved by the screws at its ends until the zero points coincide. This adjustment is not very satisfactory, and instead of making it, the correction may be noted and applied to each angle when it is read, being positive for angles above and negative for angles below the horizontal when the vernier is too far toward the objective end of the telescope.

Magnetic Needle.—The number and freedom of the oscillations of the needle indicate the strength of its magnetism. If the needle becomes sluggish it may be remagnetized by passing over it, toward each end, the pole of a magnet by which that

end is attracted, returning the magnet for each stroke through a circle of about one foot diameter. The straightness of the needle is tested by reading the angle between the two ends, first with the needle is its normal position, then when turned end for end; the difference is double the real error and the needle should be bent by that amount. After the needle has been straightened, the two ends will be 180° apart, if the pin upon which it rests is in the center of the circle. If this is not the case, clamp the instrument in any position and bend the pin till the ends of the needle are opposite corresponding points; then turn the instrument through 90° and again make the correction.

Prob. 26. Give the reasons for each of the above adjustments, drawing a figure in each case.

Art. 27. Comparison of Transits.

The tests of the telescope and its attached level, described in Art. 23, may be applied also to the transit. All the tests of adjustments, given in Art. 26, should likewise be made upon a transit which the engineer is about to purchase. In addition to these there are others relating to the graduated circle which will here be explained. It is often incorrectly assumed that the larger and heavier the instrument the more accurate work it is capable of doing. There is some truth in this with respect to the level, but very little as respects the transit. For ordinary work a transit is large enough if it has a circle four inches in diameter. Such a circle can be made to read to half-minutes, and be practically as easily read as if its diameter were six inches. Moreover, the extra weight of the larger sizes does not materially affect the stability of the transit as that is mainly governed by the stiffness of the tripod and head. For the purposes of the land surveyor, a plain transit,—that is, one without attached bubble and vertical arc,—is perhaps sufficient. For work in towns and cities the engineers' transit, which has the level bubble and vertical arc and also two verniers, is to be preferred. Unless there be two verniers the following tests of the graduated circle cannot be made.

Angular Distance of Verniers.—The angular distance between the zeros of the two verniers should be exactly 180 degrees, but it sometimes varies from this by half a minute, owing to lack of care by the maker. To ascertain its amount the observer must be able to estimate halves or quarters of a minute; this is not difficult if the two lines on each side of the one that apparently coincides are also regarded. Vernier *A* is set exactly at 0° and then the amount which vernier *B* exceeds or lacks of 180° is read. Next, vernier *A* is set exactly at 20° and the amount which vernier *B* exceeds or lacks of 200° is read. The process is continued at intervals of twenty degrees over the entire circle, and the results are tabulated in the second and fourth columns of the table below, the plus and minus signs denoting the excess and deficiency of the supplement of the angle n as read on vernier *B*. The table is so arranged that the values of n from 0° to 180° are in the first column, while those from 180° to 360° are in the third column, and the respective discrepancies for the two parts of the circle are called d_1 and d_2. The next step is to take the means of the corresponding values of these discrepancies, observing the

n	d_1	n	d_2	$\frac{d_1+d_2}{2}$	$\frac{d_1-d_2}{2}$
0°	− 45″	180°	+ 45″	0″.0	− 45.0
20	− 15	200	+ 45	+ 15 .0	− 30.0
40	− 30	220	+ 30	0 .0	− 30.0
60	00	240	+ 45	+ 22 .5	− 22.5
80	− 15	260	+ 45	+ 15 .0	− 30.0
100	00	280	+ 30	+ 15 .0	− 15.0
120	+ 60	300	00	+ 30 .0	+ 30.0
140	+ 60	320	− 30	+ 15 .0	+ 45.0
160	+ 60	340	− 45	+ 7 .5	+ 52.5

$D = +120.0.$

algebraic signs, and place them in the fifth column. The sum of these is $D = +120''.0$, and the angular distance of the verniers is 180 degrees plus one-ninth of D, or,

$$\text{Angular distance of verniers} = 180° + \tfrac{1}{9}D = 180°\ 00'\ 13'',$$

which shows that an error of 13″ exists. A more reliable result can be obtained by taking readings at intervals of ten de-

grees around the circle, in which case the sum D is to be divided by eighteen.

Eccentricity.—If the center of the alidade, to which the verniers are attached, does not coincide with the center of the graduated plate, it will revolve around the latter in a small circle. When the vernier is on a line joining these centers there is no error, but for any other position all the readings are affected by a greater or less error of eccentricity. The last column in the above table, which is found by taking the means of the differences of the two sets of discrepancies, shows roughly the errors of eccentricity. From it there appears to be no error when vernier A reads about 105° or 285°, and a maximum error at about 160° or 340°. A closer estimate of these quantities can, however, be made, and the distance between the two centers be computed. Let each of the quantities in the last column be multiplied by the sine of the angle in the first column and the algebraic sum of the products be called s. Let each quantity be also multiplied by the cosine of the angle, and the algebraic sum of the products be called t. Using only two decimals in the sines and cosines, these values are found to be $s = -20''.4$ and $t = -208''.3$. Then the probable angle n_0 at which no error of eccentricity exists is found by

$$\tan n_0 = -\frac{t}{s} = -10.2,$$

whence $n_0 = 95\frac{1}{2}°$. Also the probable maximum value of the error of eccentricity is, if m be the number of readings on half the circle,

$$E = -\frac{2t}{m \sin n_0} = 46''.5.$$

Lastly, the radius of the circle in which the center of the alidade revolves round the center of the limb is to be found. Let R be the radius of the graduated limb, which in this case is $2\frac{1}{2}$ inches; then the radius of eccentricity is

$$r = \tfrac{1}{2}RE \sin 1'' = 0.00028 \text{ inches},$$

which is the distance between the two centers. Although this is a very small quantity, it yet produces sensible errors in the readings.

By taking several sets of readings in the manner described

a fair idea can be obtained of the angular distance between the verniers and of the effect of eccentricity on readings in different parts of the circle. The theory of errors of eccentricity is not given here, as it belongs properly to higher surveying, but it has been thought well to explain the method of procedure in order to enable the owner of a transit to investigate its weaknesses. It fortunately happens that in precise angle measurements the effect of these sources of error can be largely eliminated by the method of repetitions described in Art. 30.

Prob. 27. Test two transits by the above methods and write a report giving the observations and computations in full, and comparing the two instruments.

ART. 28. STANDARD TAPES.

In town and city surveying linear measurements of a high degree of precision are often necessary, and it is also very important that all measures should be referred to the same standard. A steel tape duly certified by the Bureau of Weights and Measures at Washington, is the most convenient standard, and it should not be used for any purpose except for the comparison of other tapes. The standard tape is certified to be correct at a given temperature when under a given pull; or the error of its length is stated for a given temperature and pull. The coefficient of expansion, or the relative change in length for one degree Fahrenheit, should also be stated in order to render comparisons at other temperatures possible. For example, a certain tape 400 feet long is stated to be a standard at 56 degrees Fahrenheit when under a pull of 16 pounds, and its coefficient of expansion is given as 0.00000703. At a temperature of 49 degrees the length of this tape will be

$$400 - 0.00000703 \times 7 \times 400 = 399.980 \text{ feet;}$$

at a temperature of 70 degrees its length will be

$$400 + 0.00000703 \times 14 \times 400 = 400.039 \text{ feet.}$$

To compare another tape with the standard it is necessary to know its coefficient of expansion also. In order to determine this the tape should be stretched out on the floor of a large

room whose temperature can be varied or be kept tolerably uniform. With a spring balance at each end it is pulled to the proper tension, the thermometer noted, and a certain length marked on two tin plates temporarily fastened on the floor. The temperature is then raised or lowered, and the operation again repeated. The change of length as marked on the tin plates is accurately measured, and this divided by the total length and by the number of degrees of change gives the coefficient of expansion. For example, suppose that at a temperature of 41 degrees a length of 60 feet is marked off, and that this is done again at a temperature of 79 degrees, the pull being the same in both cases, and the change in length being 0.016 feet. Then the coefficient of expansion is

$$(0.016 \div 60) \div (79 - 41) = 0.00000701.$$

Owing to the delicacy of this operation, a single result is not reliable, and hence a number of observations should be made under different conditions and the mean of the various results be taken for the final coefficient.

The operation of comparing a tape with a standard consists in laying off the same distance by both and thus determining the temperature at which the former is correct. The pull on the tape may be selected to agree with its size, but the pull on the standard must always be the given assigned pull. As an example, let the standard be exactly 400 feet long at 56 degrees Fahrenheit when under 16 pounds pull, and its coefficient of expansion be 0.00000703. Let the tape to be tested be 300 feet long, its coefficient of expansion being 0.00000690. With the standard 300 feet is laid off with the pull of 16 pounds, and the temperature is noted as 63 degrees. With the tape 300 feet is also laid off under a pull of 18 pounds, the temperature being noted as 64 degrees. The second distance is found to be 0.039 feet longer than the first. Now let t be the temperature at which the tape is correct under 18 pounds pull, then

$$300[1 + 0.00000690(64° - t)] - 300[1 + 0.00000703(63° - 56°)] \\ = 0.039,$$

from which t is found to be 38 degrees. The tape is therefore a standard at 38 degrees Fahrenheit when under 18 pounds

pull, and a measurement l made by it at any other temperature T will have the true value $l + 0.00000690(T - 38°)l$.

If the tape is to be used under different pulls its coefficient of stretch, or relative change in length for one pound pull, should also be determined. The operation for doing this is similar to that above described for the coefficient of expansion, except that the temperature should be constant and the pull be varied. For example, let a length of 300 feet be marked off at 15 pounds pull and again at 19 pounds pull, and let the change in length be 0.026 feet. Then the coefficient of stretch is $(0.026 \div 300) \div (19 - 15) = 0.0000216$. Any length l made under a pull P, other than the standard pull of 18 pounds, will then have the true value $l + 0.0000216(P - 18)l$, provided the standard temperature of 38 degrees exists.

Sometimes the tape is stretched over two supports A and B, and thus, owing to the sag, the measured distance is too long.

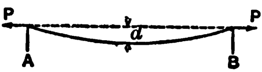


Fig. 41.

Let l be the distance read on the tape under a pull P, let d be the deflection or sag at the middle, and w the weight of the tape per linear foot. The curve of the tape is closely that of a parabola, and if L be the horizontal distance $L = l - \frac{8}{3}\frac{d^2}{l}$, very nearly. Also taking moments at the middle of the span $Pd = \frac{1}{2}wl \cdot \frac{1}{4}l$. Eliminating d from these two equations the adjusted length is found $L = l - \frac{1}{6}\left(\frac{wl}{2P}\right)^2 l$. For example, let $w = 0.0066$ pounds per foot, $P = 16$ pounds, and $l = 309.851$ feet, then $L =$ 309.642 feet. If the distance AB be subdivided into n equal spaces by stakes whose tops are on the same level as those at A and B, then $L = l - \frac{1}{6}\left(\frac{wl}{2nP}\right)^2 l$. For instance, if $n = 7$, then for the above data $L = 309.847$ feet.

To recapitulate: Let t be the temperature and p the pull at which a tape is a standard, let T be the temperature and P the pull at which a measurement l is taken, let e be the coefficient of expansion and s the coefficient of stretch, let w be the

weight of the tape per linear foot, and if sag exists let n be the number of equal spaces in the distance l. Then

$$\begin{aligned} \text{Correction for temperature} &= +\, e(T-t)l; \\ \text{Correction for pull} &= +\, s(P-p)l; \\ \text{Correction for sags} &= -\frac{1}{24}\left(\frac{wl}{nP}\right)^2 l. \end{aligned}$$

For example, let $t = 56$ degrees, $p = 16$ pounds, $e = 0.00000703$, $s = 0.00001782$, $w = 0.0066$ pounds per foot; let a distance 309.845 feet be measured at a temperature of $49\frac{1}{2}$ degrees under a pull of 20 pounds, there being 7 subdivisions in the line. Then the correction for temperature is -0.0142 feet, that for pull $+0.0221$ feet, and that for sag -0.0028 feet. The adjusted measured distance is hence 309.850 feet.

Lastly, if the measurement is made upon a slope it must be reduced to the horizontal by multiplying it by the cosine of the angle of slope. It is, however, generally best to find the difference of elevation of the two ends of the line by leveling. If h be this difference and L the length on the slope, the horizontal distance is $\sqrt{L^2 - h^2}$. For instance, if the length 309.850 feet has 2.813 feet as the difference of level of the ends, then the horizontal distance is 309.838 feet.

Prob. 28. A tape is a standard at 41 degrees Fahrenheit when under 16 pounds pull and no sag, its coefficient of expansion being 0.0000069 and its coefficient of stretch 0.000019. Find the pull P so that no corrections will be necessary when measurements are made at a temperature of 38 degrees and with no sags.

Art. 29. Base Lines.

A triangulation necessarily starts from a measured base whose length must be known with precision if the territory to be embraced by the triangles is large. A long steel tape, duly standardized, is the best instrument for making the measurement. The base line should be divided into divisions, each shorter than the length of the tape, and stout posts be set at the ends of the base and at the points of division. On these posts are placed metallic plugs, each having drawn upon it a

fine line at right angles to the direction of the base. The elevations of these plugs should be carefully determined. Each division is then subdivided into equal parts by light stakes set in line and on grade, the distance between the stakes being fifty feet or less. On each stake two small nails may be placed to keep the tape in position.

The measurement should be done upon a cloudy day with little wind, in order to avoid errors due to change in temperature. The tape is suspended over two plugs and upon the intermediate stakes and pulled at both ends by spring balances to the desired tension. At one plug a ten foot mark on the tape is made to coincide with the fine line on the plug, and at the other end a mark is made on the tape directly over the fine line on that plug. The odd distance can then be measured with a separate scale to the nearest thousandth of a foot. Several measures of each division should be made with different pulls, and the temperature be noted at each reading.

The following field notes of a short base measured by students of Lehigh University will illustrate the method of operation. There were three divisions, designated as I, II, and III,

Division.	No. of Subdivisions.	Difference in Elevation of Ends.	Temperature.	Pull.	Observed Distance.	Remarks.
		feet		pounds	feet	
III	7	2.813	51°	16	309.865	Base *EG*.
			50½	18	309.857	Oct. 3, 1888, P.M.
			50½	20	309.842	
			50	16	309.870	
			50	18	309.857	Cloudy, with
			49½	20	309.845	slight wind.
II	7	5.618	48	16	332.746	
			47½	18	332.727	
			47½	20	332.712	
			47	16	332.740	
			47	18	332.726	
			47	20	332.715	
I	6	7.924	47	16	279.850	
			47	18	279.843	
			47	20	279.832	
			48	16	279.848	
			48½	18	279.840	
			48	20	279.837	

the first having six and the others seven subdivisions. The steel tape used was about 400 feet long. It was stated by the

makers to be a standard at 56 degrees Fahrenheit when under a pull of 16 pounds and having no sag. By a series of experiments its coefficient of expansion had been determined to be 0.00000703, its coefficient of stretch 0.00001782, and its weight per linear foot 0.0066 pounds. In order to adjust the field results the expressions deduced in the last article hence are

$$\text{Correction for temperature} = -\ 0.00000703\ (56 - T)l;$$
$$\text{Correction for pull} = +\ 0.00001782\ (P - 16)l;$$
$$\text{Correction for sag} = -\ 0.00001815\ \frac{l^3}{n^2P^2};$$

from which the corrections are computed. For example, for division III, where $n = 7$, the mean of the observed distances

Temp. T.	Pull P.	Observed Distance.	Corrections. Temp.	Corrections. Pull.	Corrections. Sag.	Adjusted Distance.
	lbs.	feet	feet	feet	feet	feet
51°	16	309.865	− 0.0109	0	− 0 0043	309.850
50½	18	.857	− 0.0120	+ 0.0110	− 0.0034	.853
50½	20	.842	− 0.0120	+ 0.0221	− 0.0028	.849
50	16	.870	− 0.0131	0	− 0.0043	.853
50	18	.857	− 0.0131	+ 0.0110	− 0.0034	.8515
49½	20	309.845	− 0.0142	+ 0.0220	− 0.0028	309.850
		mean = 309.856				mean = 309.851
$n = 7$		$h =$ 2.813 feet			Final horizontal distance =	309.838

is 309.856 feet, and this is taken as the value of l in all cases. The corrections being found, the adjusted inclined distances are obtained, and their mean 309.851 is the value of the inclined length. Lastly, this is reduced to the horizontal, giving $\sqrt{309.851^2 - 2.813^2} = 309.838$ feet as the final result.

Proceeding in the same manner with divisions II and I the corrections are found and the sum of the three horizontal distances is 922.223 feet, which is the final result from the field work above given. The probable uncertainty of this result is less than 1 part in 150,000, which shows that work of a high degree of precision can be done with a steel tape whose constants are known.

Prob. 29. Compute the adjusted inclined lengths and the final horizontal lengths of divisions II and I of the above base line.

ART. 30. TRIANGULATION.

The process of triangulation, after the base is measured, consists in observing the angles of all the triangles. The data are thus at hand for computing the lengths of all the sides. If the azimuth of one side is known, or has been obtained by the method of Art. 40, the azimuths of all the other sides are easily found. Lastly, the latitudes and longitudes of the stations of the triangulation are computed (Art. 3).

In triangulation angle measurements are required to have a precision greater than the least reading of the vernier will give, and the method of repetitions is to be used. To illustrate the principle let *LOM* be the angle to be measured. Setting the vernier at 0° 00′ point first on *L*, unclamp the alidade, and point on *M*. Now, without reading the vernier, unclamp the limb, point on *L*, unclamp the alidade, and point on *M*. The vernier has thus traveled twice over the arc, and if it be now read the value of the angle is one half the reading. If, however, a third repetition is made before reading, the value of the angle is one third of the final reading. Thus the effect of repeating an angle is to divide the error of the vernier reading by the number of repetitions. More than four repetitions are, however, not usually advisable, since the effort of clamping is to introduce a constant tendency to error in one direction.

The process of repetition in any important case should be so conducted as to eliminate the effects of the errors of non-adjustment, those due to imperfections of the graduated limb, and those due to pointing and clamping. Errors due to lack of level of the limb and those due to setting the instrument or signals in the wrong position cannot, however, be eliminated, and hence great care should be taken that these do not exist. Errors due to collimation and to the horizontal axis of the telescope may be eliminated by taking a number of repetitions with the telescope in the direct position and an equal number with it in the reverse position. Errors due to angular distance between the verniers and to eccentricity of the graduated limb may be eliminated by reading both verniers and taking their mean. Errors due to inaccurate graduation may be eliminated

by taking readings on different parts of the circle. Errors due to pointing and clamping may be largely eliminated by taking one half of the repetitions in one direction and the other half in the reverse direction.

The following form of field notes shows four sets of measurements of an angle *HOK*, each set having three repetitions. The first and fourth sets are taken with the telescope in the direct position, the second and third with it reversed. The first and second sets are taken by pointing first at *H* and secondly at *K*, the third and fourth are taken by pointing first at *K* and secondly at *H*. At each reading both verniers are read. The vernier is never set at zero, but the reading before beginning the set is taken, this being made to differ by about 90 degrees in the different sets so as to distribute the readings over the entire graduation. After completing a repetition both verniers are again read. In the first and second sets the mean final reading minus the mean initial reading is divided by 3, the number of repetitions, to give the angle as determined by that set. In the third and fourth sets the initial reading minus the final reading is divided by 3. If very accurate work is required four or eight additional sets may be taken on different parts of the circle, and the mean of all will be the probable value of the angle.

Station Observed.	No. of Reps.	Tel. *D* or *R*.	Reading.					Angle.			Remarks.
			°	′	*A* ″	*B* ″	Mean ″	°	′	″	
H	3	*D*	20	04	00	30	15	62	25	10	Angle at station *O*, Sept. 30, 1895, 3 p.m.
K			207	19	30	60	45				
											Brandis Transit, No. 716.
H	3	*R*	110	12	30	30	30	62	25	07	John Doe, observer; R. Roe, recorder.
K			257	27	60	45	52				
K	3	*R*	350	02	00	15	07	62	25	33	Air hazy, no wind.
H			162	43	15	30	22				
K	3	*D*	80	56	15	00	08	62	25	35	80 + 360 = 440°.
H			253	39	00	45	22				Mean of four sets, *HOK* = 62° 25′ 21″.

In repeating angles the following points should be noted: The instrument should never be turned on its vertical axis by taking hold of the telescope or of any part of the alidade; the limb should never be clamped when the verniers are read; the observer should not walk around the instrument to read the verniers, but standing where the light is favorable he should revolve the instrument so as to bring vernier *A* and then vernier *B* before him; the observer should not allow his knowledge of the reading of vernier *A* to influence him in taking that of *B*; care must be taken to turn the clamps slowly and not too tightly. If these precautions be taken the value of an angle

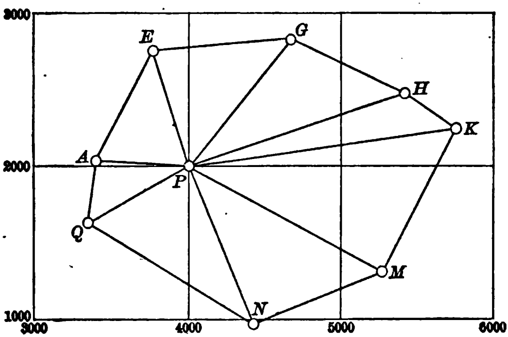


FIG. 42.

can be obtained to a high degree of precision with a transit reading only to minutes.

The stations of the triangulation should be points which are not liable to be lost, such as holes drilled in rocks or in monuments firmly planted in the earth. In the survey of a town, however, some points may be used upon which the transit cannot be set, as for instance church spires, but these must be so selected that they can be seen from many other stations. Care should be taken that all the triangles are well proportioned, and in general this will be secured when no angle is less than 30 degrees or over 150 degrees.

A triangulation forms the framework of a map. All its stations being accurately located, a traverse may start at any one and take the notes necessary for a map of that vciniity, check-

ing the field work, perhaps, by ending at another station. Thus there is no trouble in joining different surveys, for all are connected with the same skeleton framework. In plotting the maps a coordinate system of lines 1000 feet apart is first drawn and upon it the triangulation stations are located; from these the various traverses or stadia lines are laid off as indicated by the field notes. The precision of triangulation work will depend upon the purpose for which it is to be used; for ordinary town or topographical surveys it will perhaps be sufficient if the lengths of the lines and the coordinates of the stations are found to the nearest tenth of a foot.

In Fig. 42 is represented a small triangulation system in which *EG* is the base line and *P* a spire. All the angles, except those at *P*, were observed by the method of repetitions, and a part of the final results of the computations are given in the table below. Here, as in Chapters I and II, the azimuths

Line.	Azimuth.	Distance. feet.	Station.	Latitude. feet.	Longitude. feet.
AQ	186° 49′ 38″	404.57	*A*	2014.83	3406.63
AE	25 36 07	778.95	*E*	2717.30	3743.23
AP	91 25 54	593.55	*G*	2804.40	4661.32
EA	205 36 07	778.95	*H*	2458.20	5379.37
EG	84 34 48	922.22	*K*	2250.76	5733.05
EP	160 18 15	761.87	*M*	1290.02	5266.68
GP	219 25 28	1041.35	*N*	988.38	4435.91
GH	115 44 28	797.15	*Q*	1613.13	3358.54
HP	251 37 29	1453.48			
MP	299 16 15	1452.09			

are counted from the north around through the east, south, and west, while latitudes are positive toward the north and longitudes positive toward the east. This is the usual method in land and town surveying. It should be said, however, that in geodetic work and in extended topographical surveys the azimuths are often counted from the south around through the west, north, and east, while latitudes are taken as positive toward the north and longitudes as positive toward the west.

Prob. 30. Compute the latitude and longitude of *P* from the above data by several different methods.

CHAPTER IV.

TOPOGRAPHIC SURVEYING.

ART. 31. LARGE-SCALE TOPOGRAPHY.

THE scale to which topographic maps are drawn depends upon the use for which they are designed; if it is desired to show a large extent of territory at once, the scale will be determined by the size of the finished map which will be most convenient for use; on the other hand, if it is desired to show a smaller territory but with more minuteness, a larger scale could be adapted to the same size sheet as before. The scale of the map influences the degree of accuracy employed in the field work and also the appearance of the signs used in representing the various topographic features.

Under the term large scale, it is intended to include maps plotted to a scale larger than 400 feet to an inch. Such maps are designed to show the contour lines with from 2 feet to 10 feet intervals, the former distance being applicable in case the country is flat, and the latter where the slopes are abrupt or where less precision is required. All roads and streets, whether highways or on private property, are shown and also the positions of the property lines. Dwellings and other buildings are represented in their true shape and with dimensions drawn to the scale of the map. The positions of isolated trees are located by measurement, as are also the boundaries of woods. If a stream is to be shown, both sides, instead of the middle line alone, are plotted unless the width is so small that one stroke of the pen would cover both sides. It sometimes happens that objects have to be plotted out of proportion to the rest of the map because, mechanically, it is impossible to represent them on the proper scale. It is quite impracticable to plot, or for the eye to distinguish, distances on the map of less than $\frac{1}{100}$ of an inch; if the scale of the map is 200 feet to an inch, $\frac{1}{100}$ of an inch represents 2 feet and hence objects of less size than that are indicated by one line. A specimen of a large-scale topographic map is shown in Fig. 43.

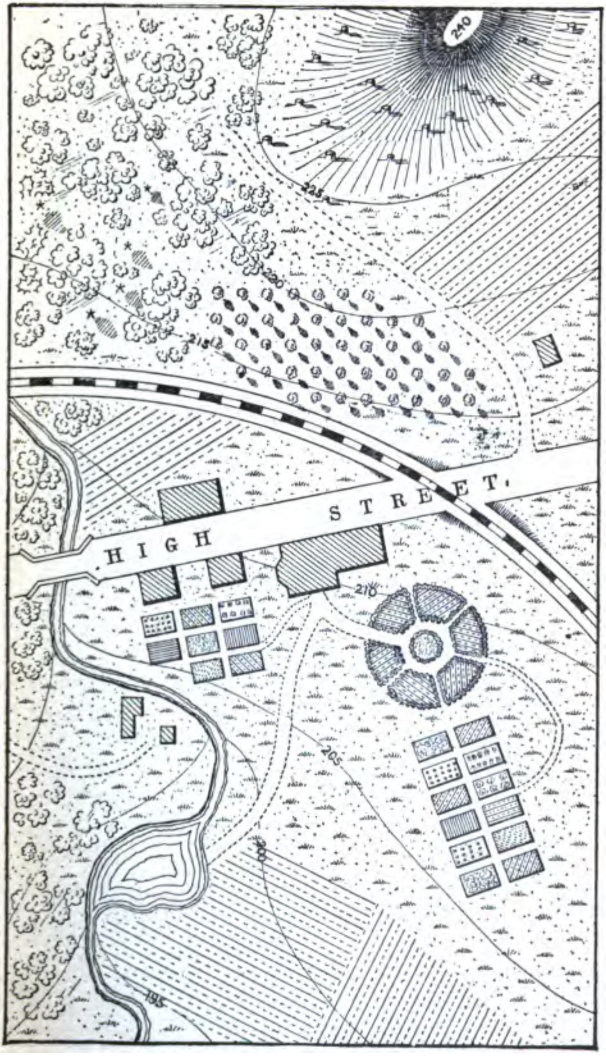


FIG. 43.

The conventional signs used in illustrating topographic characteristics, whether indicating the nature of the ground or of the crops growing upon it, are designed to bear some degree of resemblance to the objects they are to represent; the motive in the use of the signs, however, is to convey information concerning the character rather than the actual appearance of the objects, and hence no attempt is made to draw the signs to the scale of the map, other than to make them of such size and weight as will harmonize with the other parts of the drawing. It is of the first importance that the topographic draftsman be entirely familiar with the exact appearance of the signs he wishes to use; especially is this true if the drawing is to be on a large scale where no marks are made at random, but each one is to perform a definite part in producing the general effect of the whole. Some of the signs in most frequent use are shown in the sketches given in Fig. 44.

Care must be taken that the signs are so made as to avoid a flat appearance, which is a common fault of otherwise well executed drawings. It is a universal custom to consider the light as coming from the direction of the upper left-hand corner, in which case the shadow will be on the lower and right-hand sides of the figures, and accordingly those parts are made with a somewhat heavier stroke. In making the signs for grass the shade is very slight, except in swamps where the shadow is drawn under each tuft, but in case of the forest it is of great importance in relieving the appearance of sameness which the map would otherwise have. In representing water and the shore, it is a common fault to make the line of the latter too light, the distinction between this line and the first shade line of the water should be very marked.

Scales are frequently designated as ratios; thus a scale of $\frac{1}{25000}$ is such that any actual line in the field is 25,000 times as long as its representation on the map. A scale of 400 feet to an inch is the same as 4800 inches to an inch, or $\frac{1}{4800}$ as commonly expressed.

Prob. 31. How many feet are represented by one inch on a scale of $\frac{1}{1000}$? How many acres are represented by one square inch on a scale of $\frac{1}{10000}$?

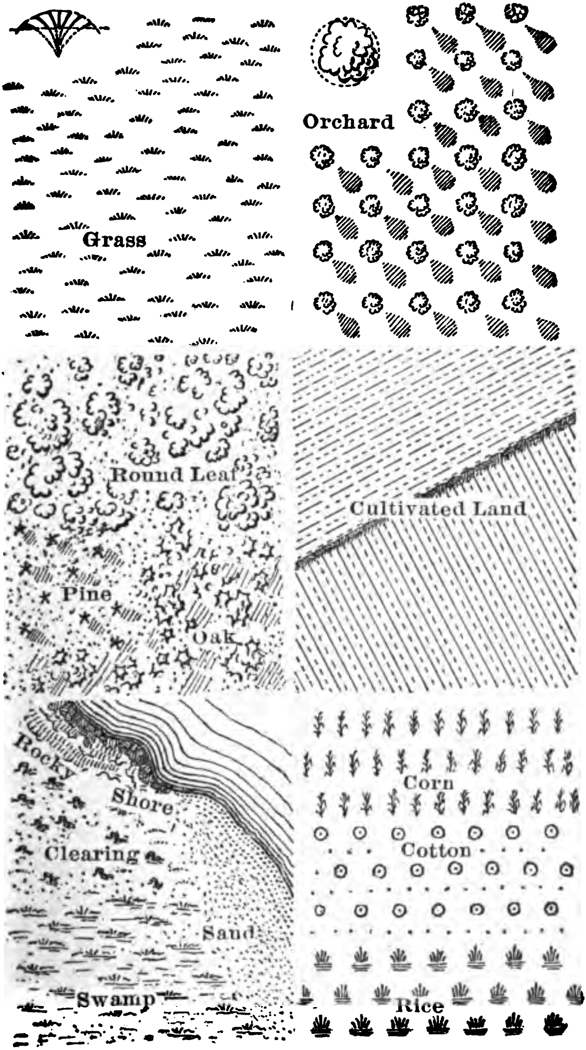

Grass
Orchard
Round Leaf
Cultivated Land
Pine
Oak
Rocky
Shore
Corn
Clearing
Cotton
Sand
Swamp
Rice

FIG. 44.

ART. 32. SMALL-SCALE TOPOGRAPHY.

In surveys covering very large areas the details are made subordinate to the general features of the country. In the previous article several reasons for so doing were stated, and in addition, the usefulness of the maps is not such as to warrant so great expenditure as would be involved in making the maps to a large scale. The saving in the cost is due, partly to the fact that less labor is necessary in plotting the maps, but more especially to the economy of time possible in making the survey, since objects need be located with only such precision as will make the errors on the map unobservable. The smaller the scale the less frequent will be the revisions necessary to keep the maps reliable since the objects subject to change are, for the most part, omitted on the small-scale maps.

The topographic maps made by the United States Coast and Geodetic Survey and by the United States Geological Survey are drawn to the scale of 1 to 62,500, 1 to 125,000, or 1 to 250,000, with corresponding contour intervals of 5 to 50 feet, 10 to 100 feet and 200 to 250 feet. These scales are seen to be approximately one, two, or four miles to the inch. The largest scales are used where the country is most densely populated or where it is flattest. Some small-scale maps show the streams, the state, county, and town divisions, the highways, railroads, and canals; but private ways and property lines are not represented; features of public importance being given, and those of a temporary nature omitted.

The conventional signs used on the small-scale maps are made to present approximately the appearance of those of larger scales when seen from a distance; the details can hardly be distinguished without the aid of a magnifying glass. Buildings are represented simply by black rectangles without much regard to the shape or size of the houses themselves. Isolated trees, small orchards, and groves are not shown, but the boundaries of forests are plotted to scale and the interior is filled in as shown in Fig. 45, with signs similar to those given in Fig. 44, but very much smaller. The highways are

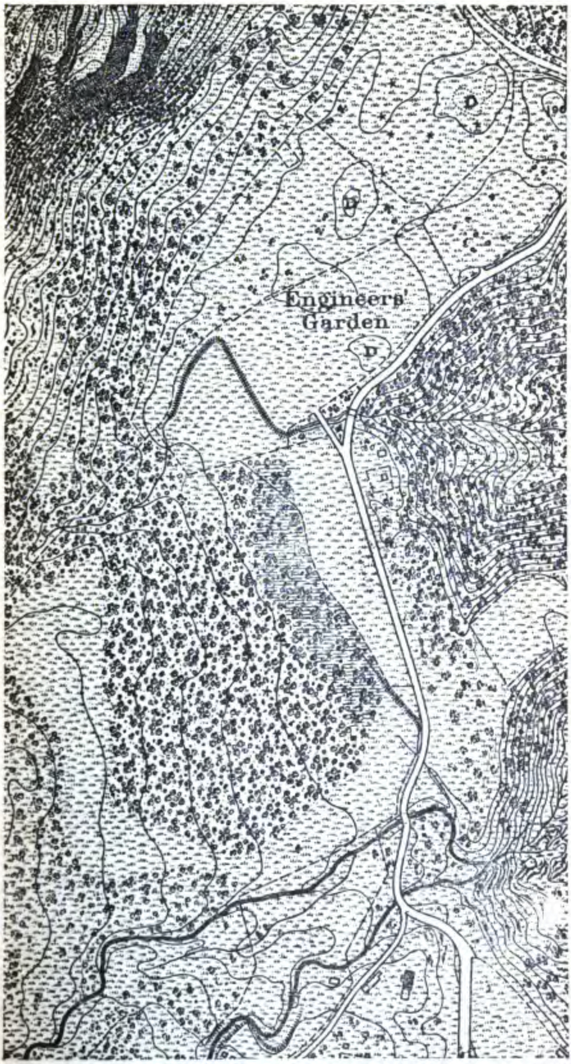


FIG. 45.

represented by parallel lines of uniform distance apart, without regard to the actual width of the road. The scale of Fig. 45 is $\frac{1}{4800}$, while that of Fig. 53 is $\frac{1}{80000}$, both being taken from the maps of the Coast and Geodetic Survey.

The use of colors is not as frequent as formerly, but the appearance of any map is improved and its utility increased by the contrast thus made, if the land be covered with a light wash of burnt sienna with the contour lines of a darker shade of the same color, and the water colored blue; all other marks are in black.

Prob. 32. Draw a profile of the surface as cut out by a vertical plane through the *NE* and *SW* corners of Fig. 45.

ART. 33. THEORY OF THE STADIA.

The fundamental principle of stadia measurements is that of similarity of triangles. In Fig. 46 let T represent a tube having three horizontal hairs and let vertical graduated rods be held in the positions AB and A_1B_1. The eye being at the end E, the distances CE and C_1E of the rod from E are directly

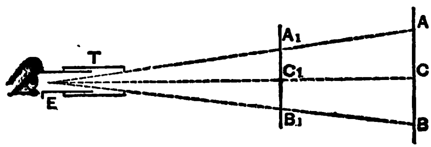


FIG. 46.

proportional to the spaces AB and A_1B_1 apparently intercepted on the rods by the cross-hairs. This simple proportion is modified somewhat in practice by the fact that a telescope replaces the plain tube.

In Fig. 47, the cross-hairs are at a and b, and i is the distance between them. Rays of light supposed to pass outward from a and b are, by refraction of the object glass, made to intersect at O, at a distance from the lens equal to the focal length of the telescope; these rays intersect the rod at A and B, the points upon which the hairs a and b are apparently projected by the eye at E. If the rod is moved to any other

point distant d' from O the space intercepted on the rod by the cross-hairs will have the same relation to AB that d' does to d, because of the similarity of triangles as in Fig. 46. The total distance from the instrument to the rod is $D = c + f + d$; in which c is the distance from the plumb-bob to the object glass and F is the focal length of the telescope. From the figure it is seen that

$$d : AB :: f : i, \quad \text{or} \quad d = R\frac{f}{i};$$

hence

$$D = (c + f) + R\frac{f}{i}$$

From this equation it would appear that the determination of D depends upon very careful measurements of f and i, but

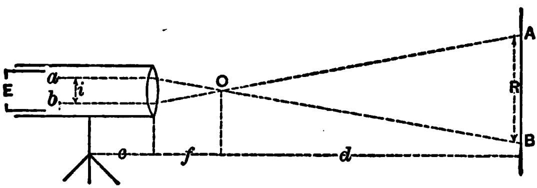


FIG. 47.

such measurements are impracticable and unnecessary since the value of $\frac{f}{i}$ can be determined by trial when c and f are approximately known. The distance c is found by measuring from the axis of the telescope to the middle of the object glass when the telescope is focused for a distance of about 300 feet or a mean of all the distances that are to be measured. When the telescope is focused for an infinite distance f is the space between the object glass and the cross-hairs; this can readily be measured with sufficient accuracy when the focus is for an object a mile or so distant. To find the value of $\frac{f}{i}$, measure from the center of the instrument any convenient distance, as $(c + f) + 200$ feet, along level ground and hold the rod on the point thus found. Sight to the rod and count the number of spaces on it between the upper and lower hairs, then the constant number $\frac{f}{i}$ can be found from the equation

$D = (c + f) + R\frac{f}{i}$. Thus let $c = 5$ inches, $f = 7$ inches, the measured distance to the rod 201 feet, and the space intercepted on the rod 2.02 feet; then

$$201 = (0.48 + 0.52) + 2.02\,\frac{f}{i},$$

or

$$\frac{f}{i} = \frac{200}{2.02} = 99.01.$$

This would be a very awkward factor to use and hence it is desirable to either change the value of i by moving the horizontal hairs, or to substitute another rod on which the graduations are of such size that $\frac{f}{i}$ multiplied by one of the units will equal 100.

To adjust the hairs to fit the rod, measure, on nearly level ground, some convenient distance, as $(c + f) + 200$ feet from the plumb-bob, and sight upon the rod held at that distance from the instrument; move the upper hair, by means of the capstan screw for the purpose, till one space is intercepted on the rod between the upper and middle hairs, then similarly apply the correction to the lower hair. In case an ordinary self-reading level rod is used the cross-hairs would intercept two feet on it when the distance from the instrument is $(c + f) + 200$ feet.

If the cross-hairs are fixed, the rod can be so graduated that the number of spaces intercepted on it by the hairs will always be the number of hundred feet that the rod is from a point $(c + f)$ feet in front of the instrument. Sight to the plain rod held at a distance, say, $(c + f) + 300$ feet from the instrument and mark where the upper and lower hairs intersect the rod; this space divided, in this case, by three is then the unit by which the whole rod is to be graduated. After the units are marked on the rod they are sub-divided into ten or twenty equal parts to aid the eye in estimating distances other than the even hundreds.

When the rod is to be used in surveys which are to be plotted to a small scale, the constant $(c + f)$ is often disregarded and the rod is graduated accordingly. The rod is held at distance from the plumb-bob which is supposed to be about

a mean of all distances to be measured, and so graduated that the rod reading will correctly indicate that particular distance. When the rod is held nearer the instrument the indicated distance is a little too small while distances greater than the mean are slightly too large. If the rod is graduated for 500 feet the maximum error for distances between 100 feet and 1000 feet will be about 1 foot.

If the rod is to be always used in open country where the whole of it can be seen the following method of graduation may be adopted. Hold the rod at 100 feet from the instrument and mark the space intercepted by the cross-hairs, the upper one being sighted to the uppermost mark on the rod or the lower one to the lowest mark; next hold the rod at 200 feet from the instrument, direct the same hair as before to the mark at the end of the rod and note the point intersected by the other hair. The graduations for the entire rod are made in a similar manner by marking the spaces actually intercepted at each successive 100 feet distance from the instrument, one hair always being on the beginning of the graduations.

When the line of sight is inclined to the horizontal it is evident that the distance indicated on the rod is not the required horizontal distance from the instrument. If the rod is held perpendicular to the line of sight, the reading will indicate the inclined distance from the instrument to it; the hori-

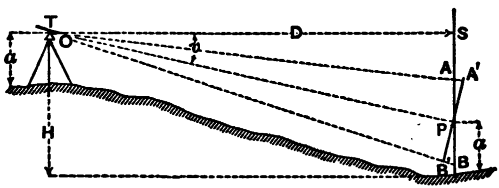


FIG. 48.

zontal distance can then be found if the angle between the line of sight and the horizontal is known. In practice it is found to be impracticable to hold the rod at right angles to the line of sight; it is hence placed vertical and an expression is found by which the horizontal distance is computed from the rod reading and the measured vertical angle v

In Fig. 48, AB is the reading on the vertical rod and $A'B'$ that when the rod is perpendicular to the line of sight. Since the angle AOB is small, no appreciable error will result if $AA'B$ is considered as 90°; then

$$A'B' = AB \cos v.$$

$A'B'$ indicates the distance OP, and $TP = c + f + OP$.

$$TS = TP \cos v = (c + f + AB \cos v) \cos v;$$
$$D = (c + f) \cos v + R \cos^2 v,$$

when R is the distance indicated by the rod reading. The term $(c + f) \cos v$ may always be taken as one foot without any practical error.

The difference in elevation H is found by sighting the middle cross-hair to a point on the rod at the same height a above the ground that the telescope is, and observing the vertical angle v. Thus,

$$PS = TP \sin v = (c + f + AB \cos v) \sin v;$$

or,

$$H = (c + f) \sin v + R \sin v \cos v.$$

For values of v less than 4 degrees the terms $(c + f) \sin v$ may be neglected, and $(c + f)$ may generally be taken as one foot.

Prob. 33. Let $(c + f) = 0.87$ feet, $R = 465$ feet, and $v = 8°, 32'$. Compute the horizontal distance D and the difference in elevation H. What error results if $(c + f)$ is not considered?

Art. 34. Stadia Reductions.

The formulas for D and H, deduced in the last article, involve much labor in computation, and hence Table X is given to facilitate the reductions. As an example of its use, suppose that $(c + f)$ for the instrument is 1 foot, and that a certain rod reading gives 680 feet for a vertical angle of 5° 26'. Then, by the help of the table,

$$D = 0.99 + 6.8 \times 99.10 = 674.9 \text{ feet},$$
$$H = 0.09 + 6.8 \times \ \ 9.43 = \ \ 64.2 \text{ feet},$$

or, $D = 674$ feet and $H = 64.1$ feet if the value of $(c + f)$ is not taken into account.

The work of reducing to horizontal distances and differences

of elevation the results of a single day's work in the field with the stadia is exceedingly tedious, even with the aid of Table X, and many schemes designed to lighten this labor have been suggested. Of these devices the most common are in the form of diagrams or of the slide rule. The objection to diagrams is that lines crossing at very acute angles have an indefinite intersection and separate diagrams have to be constructed for, at most, every ten degrees of vertical angle and also separate ones for horizontal distances and differences of elevation. The slide rule performs the operations with considerable accuracy and dispatch, but the cost of such an instrument prohibits its use in many instances.

In Fig. 49 is shown a sketch of an apparatus whose efficiency has been tested by several years' use and which may be made

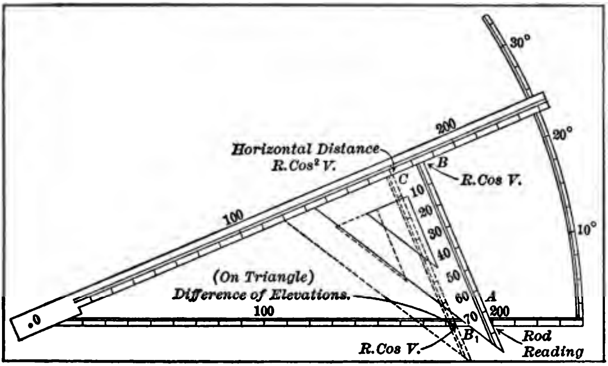


FIG. 49.

by any student of average manual skill. The apparatus consists of a large sheet of heavy paper, a movable wooden arm, and a triangle. Along the lower edge of the paper is a graduation to some convenient scale of equal parts and, about the zero of this as a centre, an arc of a circle is drawn through or near the other end and divided into degrees. The movable arm and the longer of the two perpendicular sides of the triangle are graduated to the same scale as that on the paper.

In making the reduction the movable arm is set to correspond

with the angle of elevation or depression, V, as indicated by the circular arc. The triangle is then placed as shown, so that it crosses the lower scale at the rod-reading on the latter. Since AB is perpendicular to OB the reading on the scale of the arm will be $R \cos V$. The triangle is then moved into the position shown by the dotted lines where the reading on the horizontal scale at B_1 is the same as was noted at B or $R \cos V$. With the triangle in this position the horizontal distance $R \cos^2 V$ may be read at C on the scale of the arm and the difference in elevations at B_1 on the scale of the triangle. The constants for the instrument must be added to these results. Since BC is small, usually less than an inch, the operation consists practically of one setting for the two reductions. The reductions for the transit stations should always be checked by the tables. As an example of reduction let V be 22° 30′ and R be 200 feet. The arm is set at 22° 30′, as shown in Fig. 49, and the triangle is so placed as to intersect the lower scale at the 200 mark. The reading on the arm is seen to be about 185, so the triangle is slipped back till it crosses the lower scale at 185. The reading then at C is about 171 and at B_1 on the triangle is slightly over 70. The horizontal distance and difference of elevation are respectively 171 feet and 70 feet plus corrections for instrumental constants.

The accuracy of the above example does not of course compare with that possible with a full-size apparatus. The particular one described has an arc of 40 inches radius divided into 5-minute spaces, which are large enough to make readings to single minutes practicable. The other divisions are on the scale of 10 feet to the inch, so that tenths of a foot may be easily read. The apparatus was constructed at an expense of less than one dollar, and with it from 140 to 150 reductions per hour have been made. It is better for permanent use to make the graduations on a drawing-board instead of on paper, as the latter is liable to shrink or expand with changes of temperature.

Prob. 34. Construct an apparatus for stadia reductions like that above described, and compare the precision of its work with that of Table X.

ART. 35. FIELD WORK.

The topographic survey of a large territory is preferably based upon a system of triangulation, which will afford numerous checks upon the stadia traverses. The stations should be located, not only to secure well-conditioned triangles, but also so that they may be of the greatest use to the topographers. In a flat wooded country a triangulation system is carried on only at great expense of erecting towers, and in such cases it is sometimes advisable to locate the permanent reference stations by means of carefully conducted traverses. By whatever method they are established, the stations should be near enough together to furnish means of verifying, each day, the work of the topographical parties. The elevations of the stations are to be determined and other bench marks established at proper intervals by precise leveling, in order that the errors arising from the use of the stadia in determining heights may be confined to the short traverse lines between the principal stations.

The transit used in stadia surveying need not be of large size, but there are some features that are especially essential in instruments for this purpose. The telescope should have a perfectly flat field of view, since the lines of sight do not coincide with the optical axis; this defect furnishes the opponents to the use of the stadia with their strongest argument. The vertical arc should be of superior quality, the graduations being upon solid silver, and there should be means of adjusting the vernier so that the reading shall be zero when the telescope is level. A telescope having fixed stadia hairs gives the best results, but can, of course, be used only with a specially prepared rod. The horizontal circle should have its graduations numbered continuously from 0° to 360° in the direction that azimuth is reckoned, and there should be means of setting off the magnetic declination so that the needle may indicate north or south when the line of sight is in the true meridian.

The stadia rod may be of the target variety or self reading; somewhat greater accuracy may perhaps be attained by the

target rod, but the self-reading ones are almost universally used. The rod is of pine, about 4 inches wide, and either 12 or 16 feet

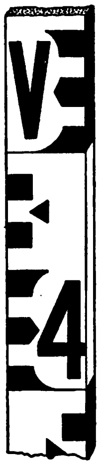


FIG. 50.

in length; it is sometimes stiffened by screwing to the back a longitudinal strip $1\frac{1}{2}$ inches square, while the ends may be protected by a metal band or shoe. There are numerous designs, but the one in Fig. 50 has been known to give good satisfaction at distances as great as 2,000 feet. The five-, ten- and fifteen-foot marks are numbered *V*, *X* and *V* in red, but the other foot-numbers are Arabic and in black. The bottom and top of the numbers are on a level with $0\frac{1}{2}$ and $4\frac{1}{2}$ tenths so as to assist in readings, and the triangle marking $7\frac{1}{2}$ tenths is 1 tenth on a side. The graduations begin at the bottom, so that the rod may be used for leveling as well as for stadia work. The edges of the rod are painted black on the alternate foot-marks as shown. The graduations of the even feet are on the left side of the rod, and those of the odd feet on the right side.

A topographic surveying party is composed of a transit-man or observer, a recorder, one or more rodmen, and axmen, if they are required. In open country, where the topography is not very intricate, one observer can take sights as fast as two or even three rodmen can select points, and the amount of territory covered in a given time is very much increased by the use of the extra rods; in more difficult territory the dispatch with which the work is done depends largely upon the skill of the recorder in keeping his notes and sketches in proper shape, and but one rodman is necessary. The work in the field consists of running traverse-lines between triangulation stations; at each of the transit points along the traverse the topography is taken within a radius of 500 feet to 1000 feet around the entire circle in azimuth. The traverses are so run that when the work is finished the entire territory within the limits of the survey has been covered by these circles. Before starting a traverse-line between two stations the elevations of the stations, the distance between them, and the azimuth of the line

joining them should have been determined. The transit is set over the first station, with the vernier at the azimuth of the line to the next triangulation station, and the telescope directed to some point on that line; the instrument is then oriented, and the line of sight is brought into the meridian by setting the vernier at zero. The needle is allowed to settle and the magnetic declination set off, if there is an arrangement for so doing; otherwise the reading of the needle should be noted. In locating the contours the rod is held at every place where there is a decided change in the slope of the ground; in surveying a small ravine elevations are taken along the valley and along the top of the slope on each side. In work that is to be plotted on a large scale two points on each building are located, and it is well to have the dimensions measured with a tape. The rodman should have a knowledge of what it is desired to show on the map, so that he need not rely upon signals from the observer to select the points where observations are to be taken. When the work around the station has been completed, the rodman selects a suitable place for the next position of the transit and drives a stake there. The observer reorients the transit and reads the distance to the next stake; in determining the azimuth the edge instead of the flat side of the rod is turned toward the instrument. The transit is then set over the new station while the rodman gives a backsight on the last one. The instrument is oriented by directing the telescope to the backsight, with the vernier reading the back azimuth of the line; an easy way to find what the reading should be is to add 180° to azimuths less than that amount and to subtract 180° from those that are greater. The rod reading and the vertical angle should be again observed, and the mean of the two corrected horizontal and vertical distances is taken as the length of the line and the difference in elevation; the reading of the needle may be used to detect any large errors in azimuth. Below is given the manner of recording the notes on the left-hand page; the right-hand page is used for the sketch, which should show all objects located, and be as near to scale as possible. If the sketch is well made, the points where the rod was held are numbered, and

the same numbers appear in the column of stations on the left page without any other explanation. The traverse is finished

SURVEY OF					H. I. at $M = 491.7$	
Instrument at M.	$c + f = 1.00$.		Sept. 24, 1898.		Elev. of $M = 486.6$	
Point.	Azimuth.	Rod Reading.	Vertical Angle.	Hor. Distance.	Diff. Elev.	Elev.
1	84° 12′	907	− 4° 24′			
2	117 05	605	7 18			
3	314 42	245	− 0 47			
N	246 10	723	3 12	721.8	+ 40.3	526.9

by connecting with another station on the triangulation system, which station should be occupied, and the azimuth of the last course be verified, while a check is also obtained on the elevations.

Prob. 35. Fill out the blanks in the above field-notes by the help of Table X.

ART. 36. OFFICE WORK.

The stadia readings taken between stations of the traverses are usually reduced in the field by the assistance of Table X. The topographer thus has the elevations of the stations and is able to check his work whenever it is possible to connect with a station of known elevation. The horizontal distances to minor points and the corresponding differences of level are, however, often left to be filled out in the office. Graphical methods have been devised for making these reductions, but none has become so valuable as to displace the general use of the tables.

The work of making the map, like that in the field, is based upon the triangulation system, the stations of which are carefully plotted by their coordinates as described in Art. 16. The traverse lines are plotted by the protractor, as by this way the work on the map can be done as accurately as the measurements were made in the field. A suitable protractor is one of cardboard 12 inches in diameter which is fastened to the paper

by weights, with the 0° and 180° marks on the meridian; azimuths are transferred to any part of the map by means of triangles or parallel rulers. If the work is carefully done, the traverse lines should close so that the discrepancy is not noticeable on the scale to which it is plotted. The error of closure may, with proper care, be kept less than 1 in 1000, and much better results than this have been attained.

After the traverse lines have been established the topography is plotted by orienting the protractor over each station and pricking off all the azimuths of the readings around it; the protractor is then removed and the corresponding distances are measured on the proper scale. The sketch will show whether the point is merely to locate contours or is on some object to be plotted on the map; in the latter case the house or whatever the object is should be drawn as soon as enough points on it have been established, and all superfluous marks erased; if only the elevation is needed, that is written lightly in pencil. The contours cannot be sketched as fast as the elevations are marked, but this work should not be deferred after enough heights have been plotted to do it intelligently.

What was stated in Art. 16 about the lettering, title, meridian, and border applies as well to topographic drawings and need not be repeated. The execution of the topographic signs is of utmost importance in determining the appearance of the map. While experienced draughtsmen are able to dispense with such help, no student should attempt to make the conventional signs on a map without having before him a good copy. The tendency always is to make the signs much too large and without definite shape. No amount of practice will suffice where a clear knowledge is wanting of just how the figure should look.

Prob. 36. Draw in pencil six horizontal lines and twelve vertical lines on Fig. 43 at equal distances apart. Then make the same number of lines on drawing-paper at distances apart three fourths as great. Copy Fig. 43 on the reduced scale. (As an exercise in contour drawing Fig. 56 may be also copied, the scale being enlarged about one-half.)

Art. 37. The Plane Table.

The plane table is a small drawing-board mounted on a tripod head and tripod like those of the transit. On the board a sheet of paper can be fastened by clamps. On the paper a heavy ruler may be placed in any position. This ruler is furnished with level bubbles, and at its middle has a standard on which is mounted a telescope provided with a vertical arc and an attached bubble. The board, which can be moved in azimuth around the vertical axis of the tripod head, corresponds to the limb of the transit, while the ruler with its attachments corresponds to the alidade. The adjustments of the plane table are in principle the same as those of the transit. (Art. 26).

Although the plane table is an ancient surveying instrument, it is but little used except for topographical work based upon a triangulation. On the paper are plotted the stations of the triangulation, or as many as are contained in the area covered by the paper on the scale used. A common scale used is $\frac{1}{5000}$, so that on a board 24 × 30 inches in size an area of nearly 2 × 2½ miles would be represented. In a thickly settled country a scale of $\frac{1}{2000}$ is often used.

In a topographical survey one of the first uses of the plane table is to locate on the sheet secondary triangulation points

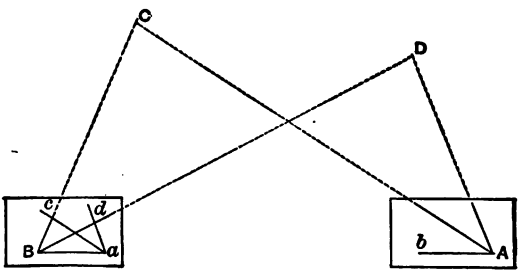


Fig. 51.

such as spires, tall chimneys, or prominent trees. In Fig. 51 this process is illustrated. A and B are two triangulation stations which are plotted on the sheet at a and b, and it is required to locate the two secondary stations C and D. The

table is first set at A, the edge of the alidade ruler placed upon the line ab, the telescope pointed to B, and the table clamped in position. With the edge of the ruler on a the telescope is pointed to C and to D, and indefinite lines drawn in those directions. The table is then set up at B, the edge of the ruler placed upon the line ba, the telescope pointed to A, and the table clamped in position. With the edge of the ruler on b the telescope is pointed to C and to D, and indefinite lines drawn in those directions. The intersection of these with those previously drawn at A gives the points c and d, which are the locations on the sheet of the stations C and D.

The operation of placing the table so that each line on the sheet is parallel to the corresponding line on the ground is called orienting the table. After the table is set up and leveled it must always be oriented; one method of doing this is explained above, and this will apply whenever the table is placed over a point which is plotted on the sheet and from which other plotted points can be seen. The alidade is often provided with a magnetic needle which will give an approximate orientation, the edge of the ruler being placed on a magnetic meridian drawn on the sheet, and the table moved in azimuth until the needle points to N on the compass limb.

When the table is placed at a point on the ground not plotted on the sheet, it is to be oriented in general by the three-point problem. An approximate orientation is first made by the eye or by the magnetic needle. Three stations, A, B, and C, being visible and plotted on the sheet at a, b, and c, it is required to locate the point n corresponding to the point N over which the table is set. Placing the alidade ruler on a, b, and c in succession, and sighting on A, B, and C, lines are drawn on the sheet, and these intersect, if the table is not truly oriented, so as to form a small triangle of error. Now the angle between the lines Aa and Bb will not be sensibly altered by the slight movement necessary to effect orientation; hence the point n must lie on the circumference of a circle passing through a, b, and the point of intersection of these two lines. Similarly, the point n must be on a circumference passing through a, c, and the intersection of Aa and Cc. It is not practicable to draw

these circles on the sheet, but by imagining them to be drawn a close estimate of the point where they intersect can be made, and n be marked on the sheet. Now place the edge of the ruler on this point n, and also on a, move the table until A is seen on the telescope hair, and a closer orientation is secured. Then sighting to B and C, and drawing new lines Bb and Cc, a

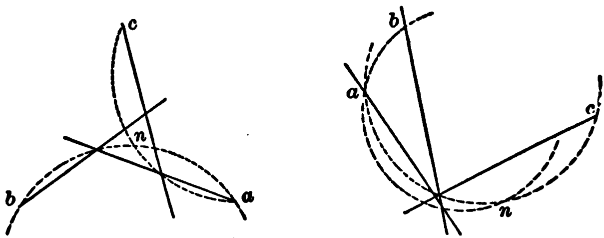


FIG. 52.

smaller triangle of error results, from which a better position of n is found, and on the third trial the triangle of error should entirely vanish, thus giving both a correct orientation and the proper location of n corresponding to N on the ground.

It should be remarked that if the table is set up within the large triangle ABC, as in the first diagram of Fig. 52, the point n falls within the triangle of error. In other cases it falls outside the triangle of error. If N is situated on the circumference of a circle passing through A, B, and C, the problem is indeterminate, and another station D must be observed in connection with two of the others. For a fuller discussion of the three-point method of orientation see "A Treatise on the Plane Table," in Appendix No. 13 of the Report of the U. S. Coast and Geodetic Survey for 1880.

After the plane table is oriented the topography for several hundred feet around the station is put in with the help of the alidade and stadia rods. The alidade ruler gives the direction of any object, and the stadia reading its distance, so that it may be immediately plotted by a scale and a pair of dividers. For an inclined stadia reading the vertical angle is read, and th corresponding horizontal and vertical distances at once taken from a table, the latter giving the elevation of the observed

point above the table, which is noted on the sheet, so that the contours can be afterward sketched. In fact, all the operations are similar to those explained in Art. 33, except that no notes are kept. Traverses may be run along roads, or into localities where no triangulation points are visible, by drawing the lines successively on the sheet and moving the table from one station to another, orienting it by a back sight. Thus the entire map is finished in pencil in the field. The theory of all the operations is simple, but the practice requires some skill and experience, and the sheet is sometimes liable to become injured by dust or rain. Much more topographic work is done with the transit and stadia than with the plane table.

The three-point problem, above mentioned, also arises in secondary triangulation when a new station is to be established by means of angles there measured between lines drawn to three stations, whose positions are given. Thus if the co-ordinates of three stations A, B, and C are given, and N be the station where the angles ANB and BNC are measured, then the co-ordinates of N can be computed. Formulas for doing this are given in works on higher surveying; see Merriman's Precise Surveying and Geodesy (New York, 1899).

Prob. 37. Given two stations A and B, which are plotted on the sheet at a and b. It is required to set the plane-table at two other points D and E, and to locate d and e on the sheet by sighting at A, B, E, and D.

Art. 38. Hydrographic Surveying.

When a topographic survey embraces rivers, harbors, or a part of the coast, the shore-lines are located and plotted by the methods above described. It is also generally necessary to indicate on the map the depths of water at various points, the position of shoals, rocks, and other sub-surface features, and also sometimes to determine the direction and velocity of currents; this part of the work constitutes hydrographic surveying.

Soundings in shallow water are made by means of rods graduated to feet and tenths. When the current is not rapid, a boat may be rowed at a uniform speed in a straight line, which is determined by signals set in range on shore, and soundings be taken at uniform intervals of time. The position of the boat both at the start and finish is located by intersections from other signals on shore or by means of observations with transits. When this line is plotted on the map, it is divided into the same number of spaces as there were time intervals, and at each point of division the corresponding sounding is plotted. If the number of soundings is sufficient, contour curves for different depths below the water-level may be drawn, and thus a clear picture is presented of the bottom surface of the river or harbor

In deep water where a rod cannot be used depths are obtained with a plummet attached to a line, the position of each sounding being located by angles taken either on the boat between signals on the land, or by observers on shore. In the former case the sextant is generally used, two angles being measured between three known stations. This is a case of the three-point problem (Art. 37). In plotting the position from the two observed angles computations are rarely necessary, but three lines may be drawn on tracing-cloth, intersecting at a point and making with each other the given angles; then placing the tracing on the map so that the three lines pass through the given stations the point will fall in the proper position and may be pricked through upon the map.

In all cases of sounding a water-gauge should be erected near the shore for the purpose of observing the variations in the water-level, and thus referring the soundings to the same plane, either of high or of low water. In tidal streams or harbors readings of such a gauge are necessary at quarter-hour intervals.

The sextant is a most useful instrument in all work done in the boat, where indeed measurement of angles with a transit would be almost impracticable. The principle of its use is that an object may be seen both by direct vision and by reflection from a mirror. For instance, in the first diagram of Fig. 53 let *H* and *I* be two parallel mirrors called the horizon glass and

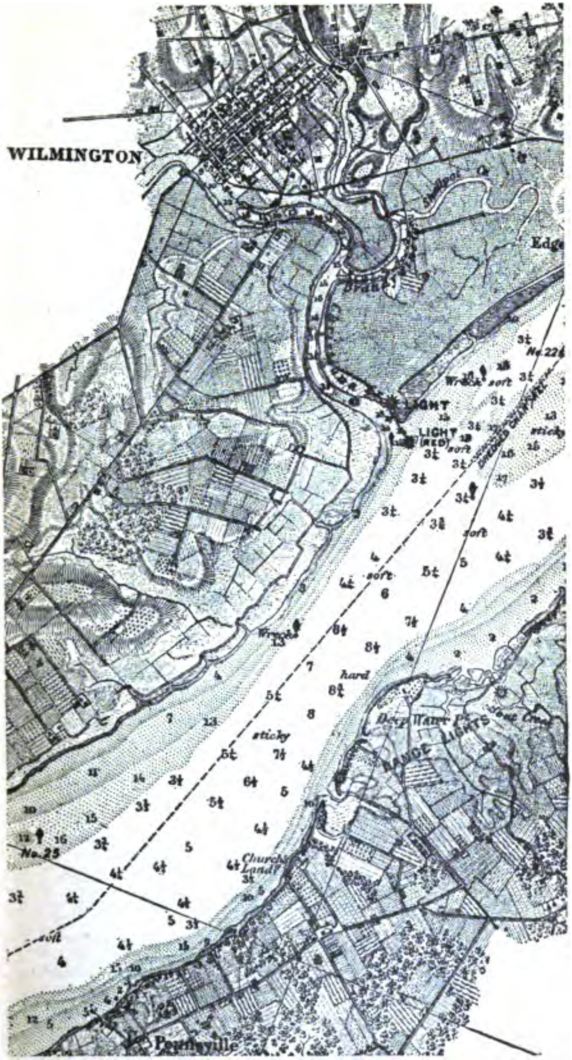

WILMINGTON
LIGHT
LIGHT (RED)
RANGE LIGHTS
Wreck
Deep Water Pt.
No. 25
Church Landing
Pennsville

FIG. 53.

the index glass, the upper part of *H* having an opening in *K*. Then the eye at *E* can see a distant object *S*, both by direct vision in the line *SHE*, and by the reflected ray which follows the path *SIHE*; in this position the two images coincide and the index arm *IA* indicates zero on the graduated limb. In the second diagram the index arm is moved to the position *ID* in order to measure the angle *SET*, between two signals *S* and *T*; in this position *T* is seen by direct vision and *S* by reflection. As the angles of incidence and of reflection are equal on each mirror, the angle *AID* is one half the angle *SET*. The arc is

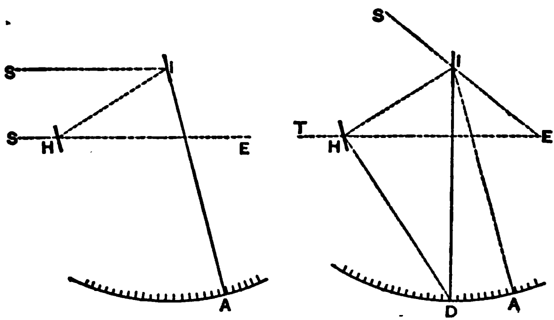


FIG. 54.

hence graduated so that half a degree on it represents a whole degree of the measured angle; thus the reading at *D* gives at once the required angle *SET*.

In measuring a horizontal angle the plane of the sextant should be kept as nearly horizontal as possible. Care should be taken that the reading of the vernier is zero when an object is viewed both by direct and reflected vision, as in the first diagram of Fig. 54; if this is not the case, the index error should be noted and be applied as a correction to the final reading.

The direction of currents may be noted by observing with the sextant the direction taken by a float thrown from a boat, and the velocity of the current may be found by noting the time required for the float to pass over a certain distance. The determination of velocities at points below the surface, and the gauging of streams to ascertain their discharge and mean veloc-

ity, is properly a branch of hydraulics rather than of surveying. Concerning these see Merriman's Treatise on Hydraulics (New York, 1916), Chapter 10.

Fig. 53 shows a part of a hydrographic map of the Delaware River on a scale of $\frac{1}{80000}$, reproduced from the chart of the U. S. Coast and Geodetic Survey. The numbers in the central part of the river show the depths in fathoms at mean low-water spring tides, those on the shaded surface show depths in feet. The various lights and buoys are represented in proper position. The topography of the shores is a fine example of small scale work, although the copy does not fully represent the beauty of the original copper-plate chart.

Prob. 38. Prove that in Fig. 54 the angle *AID*, moved over by the index arm, is one half the observed angle *SET*.

ART. 39. MINE SURVEYING.

Mine surveying is little more than ordinary surveying, rendered difficult by darkness and mud. The main object is to take measurements which will furnish accurate maps of the underground workings, so that the position of every point may be known relatively to points on the surface. These maps are necessary, both for the advantageous development of the mine in driving tunnels, slopes, and gangways, and for the safety of the miners. The maps of the anthracite coal regions of Pennsylvania are required by law to be drawn on a scale of 100 feet to 1 inch, and to be kept up as the work progresses.

Mine maps show the main features of the surface of the ground, such as streets and houses, with all the breakers, slopes, manway and air-shaft openings. The underground workings are shown in horizontal projection and proper position on the same sheet, different-colored inks being sometimes used to distinguish the different veins. Elevations of many points of the underground workings are given in figures, so that the difference of level between them and the surface is at once known, as well as the grades of the gangways and other passages. Sometimes the surface contours are also shown,

and by the help of these, and the elevations of the underground points, profiles and cross-sections may be drawn on different vertical planes.

The general methods of mine surveying are the same as those of land and topographical surveying. The most approved plan is to have on the surface triangulation stations referred to a system of coordinates (Art. 30). At some mines, however, coordinate lines are actually staked out on the surface. Starting at any station, a traverse may be run down a slope and through a gangway, coming out perhaps at another slope or manway, and checking on another triangulation station. This traverse is run by the transit and a long steel tape, two consecutive stations of the traverse being generally nearer together than the length of the tape. Offsets are taken to the sides of the slopes and gangways, and short lines are run up the breasts and openings. Thus all the data are obtained for computing the traverse and constructing the map. Elevations are determined by taking vertical angles, although when convenient the level and rod is sometimes used.

The stations of the underground traverse are placed in the roof on wooden plugs driven into holes drilled for that purpose. On these are hung the plummet lamps to which backsights and foresights are taken. To set up the transit at a station a point on the floor directly beneath the one in the roof is determined by the plumb-bob. A transit for mine surveys should have a shifting plate and adjustable tripod legs, while a universal joint is also often a great convenience. To illumine the cross-wires the transitman holds his copper lamp at arm's-length so that the light may shine into the objective end of the telescope; the same lamp enables him to read the vernier and the magnetic needle. The readings of the magnetic needle, which serve as checks on the horizontal angles, must be taken both backward and forward at each station, as marked local attractions occur in mines. Much time is often wasted in reading the needle; instead it would be better to check the azimuth by taking another angle. The linear measurements are made when the tape is tightly stretched by two men, offsets

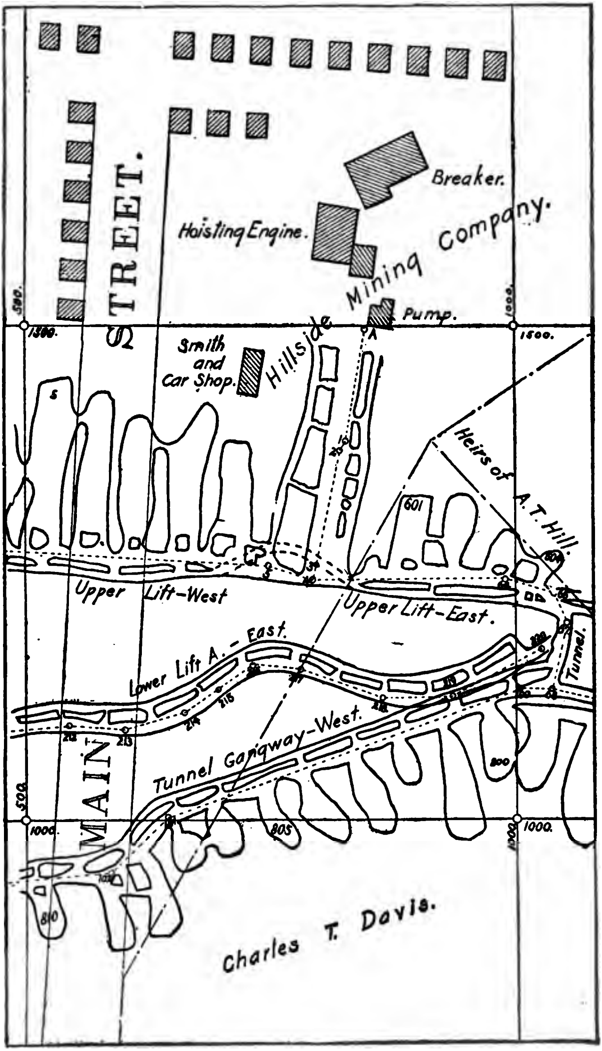

STREET.
MAIN
Breaker.
Hoisting Engine.
Mining Company.
Pump.
Smith and Car Shop.
Hillside
Heirs of A. T. Hill.
Upper Lift-West
Upper Lift-East.
Lower Lift A. - East.
Tunnel Gangway-West.
Tunnel.
Charles T. Davis.
1500.
1500.
1000.
1000.
500.
1000.
500.
1000.
601
800
805
810

FIG. 55.

being taken to the corners of pillars and the sides of the gangways. A mine survey corps usually consists of four or five men, a transitman, two chainmen, and one or two men for offsets and lights.

The form of field-notes may be the same as that given in Art. 15, but instead of measuring the interior angles it is best to carry on the azimuths as explained in Art. 19. Some prefer to reverse the telescopes and measure the deflection angle to the right or left, but this is inferior, in accuracy and convenience to the method of azimuths. The form of notes is subject to so great variations in different localities, that it seems scarcely wise to attempt to give one of them here.

The computation of the coordinates of the stations of the traverse is next made. Lines being drawn on the paper 500 feet apart both vertically and horizontally, the stations are plotted in their proper positions. The offsets are then laid off and the sides of the slopes, gangways, air-passages, and breasts are drawn. The underground traverse-lines are usually plotted in red, and each station designated by its letter or number. The elevations are noted in figures at such stations where they may be likely to be needed. If surface features are to be also given, they are plotted from the notes of an outside survey.

Fig. 55 shows a part of a map of an anthracite coal mine, reduced from the original scale of 100 feet to 1 inch to about half that scale. It shows the buildings around a slope entrance, and the slope with a few gangways and breasts. The fine broken lines are the traverses of the survey and each station has its number; a traverse is seen to start at *A* near the pump house, run down the slope to station 4, and then turn to the west along the upper lift gangway. The long pillars seen in each gangway separate it from the air way. In every fifth breast is written the number by which it is known.

Extended surface surveys in the mining regions come under the head of topography taken with especial reference to geologic features. Fig. 56 shows a small area near Carbondale, Pa., taken from Mine Sheet No. XXI of Part IV of the Atlas of

the Northern Anthracite Coal Field, issued by the Second Geological Survey of Pennsylvania. The scale is 1 inch to 800 feet and the contour interval is 10 feet, the elevations being given with reference to tide water. The coordinate lines, drawn at intervals of 2000 feet, give distances north and east from a

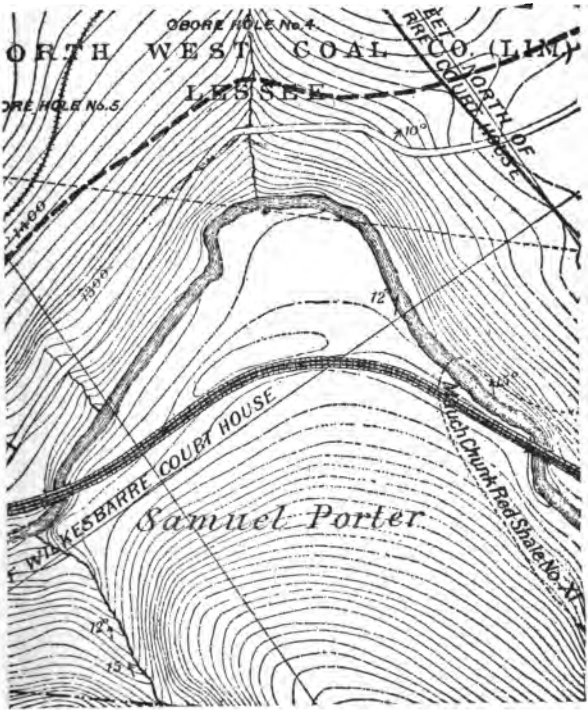


FIG. 56.

monument in the yard of the court-house at Wilkes Barre. Bore-holes, dips of strata, and outcrops of the formations are shown, as also property lines, and names of owners or lessees. The colors on the original map are not reproduced in the copy.

Prob. 29. By surveys and computations the following data were obtained concerning four points in a certain gangway driven around one end of a vein in a coal basin:

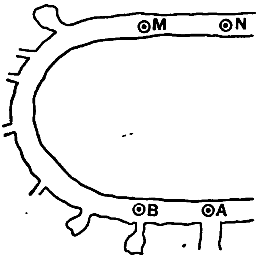


FIG. 57.

Station.	Latitude.	Longitude.
A	$+ 2604.25$	$+ 2428.10$
B	$+ 2597.18$	$+ 2010.43$
N	$+ 3345.65$	$+ 2904.18$

Also, elevation of $A = 783.84$, elevation of $N = 807.90$, azimuth of $MN = 92° 17'$ (S 87° 43′ E). It is desired to drive a tunnel from A to N, and for this purpose the following quantities are required to be found: (1) Length of line AN, (2) azimuth of AN, (3) the horizontal angle BAN, (4) the horizontal angle MNA, (5) the grade of the line AN.

ART. 40. THE TRUE MERIDIAN.

A true meridian is established by actually staking out a line running due north and south, or by determining the true azimuth of a given line. The latter method is preferable in town and city work. From the azimuth found for the one line the azimuths of all other important lines are obtained by traversing or by triangulation. A meridian actually staked out is of no value except for determining the azimuths of lines. Three methods of determining the true meridian will be here explained.

By Polaris and Mizar.—The pole-star Polaris revolves around the pole in a small circle, and crosses the meridian, or culminates, twice each day. Mizar, the middle one of the three stars in the tail of the Great Bear or handle of the Great Dipper, revolves around the pole in a large circle and culminates a few minutes earlier than Polaris. In 1895 Polaris culminates about 50 seconds after it and Mizar are in the same vertical circle, in 1900 about $2\frac{1}{4}$ minutes after, and in 1905 about $4\frac{1}{4}$ minutes after, the annual increase being 21 seconds. To obtain the true meridian set up a transit about a quarter of an hour before the two stars are in the same vertical; the

transit must be in good adjustment, particularly in respect to collimation and horizontal axis of the telescope. Sight alternately upon Polaris and Mizar, and note by a watch the time when they are upon the same vertical. Then, after the expiration of the interval above mentioned, turn the vertical hair upon Polaris, and the line of sight coincides with the true meridian. The error of this method will probably be greater than one minute of angle, as the work must be done at night.

By Polaris.—The time of culmination of Polaris may be ascertained from Table V, and the vertical hair of a transit be set upon it at that instant. But a more accurate method is to observe Polaris at its east or west elongation, following it with the vertical hair until its motion in azimuth ceases. The approximate time of elongation may be found from Table V, and the astronomical azimuth of Polaris at elongation is found from Table VI. Thus the azimuth of the line of sight is known; if a point be marked beneath the plumb-bob and another several hundred feet away in the line of sight, a line is determined whose azimuth is known. By repeating the operation on several days a mean result can be obtained which can be depended upon with an error not exceeding one minute of angle. This work need not be done at night, as Polaris can often be seen by a telescope of moderate power in the daytime.

By the Sun.—With a transit having a solar attachment the true meridian can be found by observing the sun at any time except between 11 A.M. and 1 P.M. Such an attachment can be placed upon any transit at a cost of about fifty dollars. Accompanying it is a pamphlet giving full directions for use and adjustment, together with tables of the declination of the sun for Greenwich noon on each day of the year. Both the transit and the solar attachment should be in correct adjustment in order to do good work in determining the true meridian.

In order to explain the theory of the solar attachment let the upper part of Fig. 58 be a section of the celestial sphere in the plane of the true meridian, N and S being the north and south points of the horizon, P the pole, Z the zenith, Q the celestial equator, and O the place of the sun at noon. Let A be the point where the instrument is set, which may be regarded

as the center of the celestial sphere. Then the angle PAN or its equal QAZ is the latitude of the place of observation. The angle QAO is the declination of the sun, which is positive when the sun is north of the equator from March 21 to September 21, and negative when the sun is south of the equator from September 21 to March 21. The lower part of Fig. 58 is a plan, A being the place of the instrument, NS the true meridian through A, W and E the west and east directions, AO the direction of the sun about 10 o'clock in the morning, and AL a line whose azimuth is required to be found.

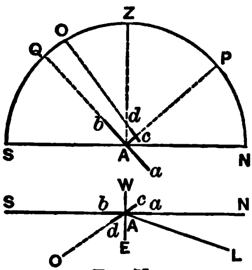


FIG. 58.

Let ab represent the telescope of the transit, placed in the meridian and elevated so as to point to the celestial equator; this will be the case when the angle of elevation SAQ is equal to the co-latitude, or when $SAQ = 90° - QAZ$. Let cd be the telescope of the solar attachment pointing toward the sun; then the vertical angle between ab and cd is equal to the declination of the sun QAO. In this position the solar attachment is like an equatorial telescope, its axis pointing to the pole P, and as the sun moves the telescope cd will follow it along the celestial sphere until the change in declination becomes appreciable.

Before beginning work a list of hourly declination settings is to be prepared by help of the table of declinations which is furnished by the maker of the instrument. This table also gives for each hour the effect of refraction, this refraction always increasing the altitude of the sun. For example, let it be required to find the declination settings for the afternoon of September 19, 1895, for any place where eastern standard time is used. The table gives $+ 1° 28' 54''$ as the declination of the sun at Greenwich noon for that day, and $58''$ as the hourly decrease of declination. The declination at 7 A.M. of eastern standard time is then $+ 1° 28' 54''$, and that at 5 P.M. is $+ 1° 28' 54'' - 10 \times 58'' = + 1° 21' 14''$. Thus the declination

for each hour is found and given in the second column. In the third column is placed the refraction correction as given in the table, and the fourth column gives the final declination settings

Hour.	Declination.	Refraction Correction.	Declination Settings.	Remarks.
1 P.M.	+ 1° 25′ 06″	+ 0′ 48″	+ 1° 25′ 54″	For Eastern
2 P.M.	+ 1 24 08	+ 0 54	+ 1 24 52	Standard Time,
3 P.M.	+ 1 23 10	+ 1 05	+ 1 24 15	September 19,
4 P.M.	+ 1 22 12	+ 1 32	+ 1 23 44	1895.
5 P.M.	+ 1 21 14	+ 2 51	+ 1 23 05	

which are the apparent declinations for the respective hours. The refraction correction is always additive, and hence if the declination is south or negative its numerical value is decreased,

Hour.	Declination.	Refraction Correction.	Declination Settings.	Remarks.
8 A.M.	− 22° 23′ 43″	+ 6′ 31″	− 22° 17′ 12″	For Eastern
9 A.M.	− 22 24 02	+ 2 59	− 22 21 03	Standard Time,
10 A.M.	− 22 24 21	+ 2 11	− 22 22 10	December 5,
11 A.M.	− 22 24 40	+ 1 54	− 22 22 46	1895.

as the example for December 5, 1895, shows; on that day the table gives the declination at Greenwich noon as 22° 23′ 24″ south and the hourly change as 19 seconds.

After this list is made out the observer sets up the transit over the point A in order to find the true azimuth of a line AL (Fig. 58). The telescope is leveled by the attached bubble and pointed approximately toward the south. The declination setting for the hour is next laid off on the vertical arc, depressing the object glass if the declination is positive and elevating it if the declination is negative. The telescope of the solar is then leveled by means of its own bubble, and thus the angle between the two telescopes is the same as the apparent declination of the sun QAO. Both telescopes are then elevated until the vertical arc reads an angle equal to the co-latitude of the place, or SAQ. The solar attachment is next turned on its axis, and the limb of the transit upon its axis, until the sun is seen inscribed in the square formed by the four extreme cross-hairs

in the focus of the solar telescope. When this is the case, the transit telescope is in the plane of the meridian, and if desired a point may be set out in the line AS to mark that meridian.

It will be better, however, to read both verniers on the horizontal circle, then turn the alidade around to L and read both

Time.	Reading on Meridian.	A.	B.	Reading on L.	A.	B.	Angle SAL.	Remarks.
9:15 A.M.	20°19′	00″	30″	182°27′	30″	30″	162° 08′ 15″	Oct. 28, 1895.
9:30	80 00	15	15	242 08	30	00	162 09 00	R. Doe,
9:45	140 59	30	15	303 08	45	15	162 09 08	Observer.
3:15 P.M.	200 01	60	45	2 09	45	30	162 07 45	Mean =
3:30	260 12	45	30	62 21	15	30	162 08 45	162° 08′ 38″
4:00	320 06	00	00	122 14	45	60	162 08 58	Azimuth AL
								= 17° 51′ 22″

verniers again. The angle SAL, which is the azimuth of L, has thus been measured. Repeating again the operation with the solar another value of SAL is determined, and by making several measures, both in the morning and afternoon, the mean result can be relied upon with a probable error of about one minute if the observer be skilled in such work. The above form indicates a method of keeping the field-notes.

By an Altitude of the Sun.—The altitude of the sun may be taken with a common transit, and this, together with the declination of the sun and the latitude of the place, gives the means of computing the azimuth of the sun at the moment of observation. This method is explained in full on page 248.

ART. 41. ISOGONIC MAP OF UNITED STATES.

An Isogonic Line on a map is a curve passing through all places where the magnetic needle has the same declination. The chart on the next page shows these lines for the United States on January 1, 1915. At all places on the line marked 0° the magnetic needle then had no declination; that is, its north end pointed to the true north. East of the 0° the north end of the needle pointed west of the true north and west of the 0° line it pointed west of the true north. Thus at Boston, Mass., the declination in 1915 was about 14° W, and at Helena, Mont., it was about 21° E.


75°
70°
65°
NEW
BRUNSWICK
MAINE
Augusta
Concord
VERMONT
Boston
Providence
Ottawa
Buffalo
Albany
STATUTE MILES
0 100 200 300 400 500
KILOMETERS
0 100 200 300 400 500 1000

[illegible] the 0° line is [illegible] per year. On [illegible] through the [illegible] line there was no [illegible] places east of that [illegible] at all places [illegible] Thus near [illegible] was [illegible] at

[illegible] place [illegible]

TABLE I.

NATURAL SINES AND COSINES

TO

FIVE DECIMAL PLACES.

These isognomic lines are constantly shifting; the 0° line is moving westward at a rate between 1′ and 2′ per year. On the chart two parallel lines are seen extending through the middle west; at all places on that double line there was no yearly change in declination in 1915; at all places east of that double line the west declination was increasing; at all places westward the eastern declination was decreasing. Thus, near Denver, Colo., the east declination in 1915 was decreasing at the rate of about 3′ per year.

A rough estimate of the magnetic declination for any place for any year between 1910 and 1920 can be made by the help of this chart. Thus, for Washington, D.C., the chart gives the declination in 1915 as 6° W and the annual change as 4′.4 W; hence the change in five years was 22′ W or about 0°.4 W, and accordingly the declination in 1910 was approximately 5°.6 W and that in 1920 will be approximately 6°.4 W. An estimate of this kind cannot be relied upon within 0°.3.

TABLE I.

NATURAL SINES AND COSINES

TO

FIVE DECIMAL PLACES.

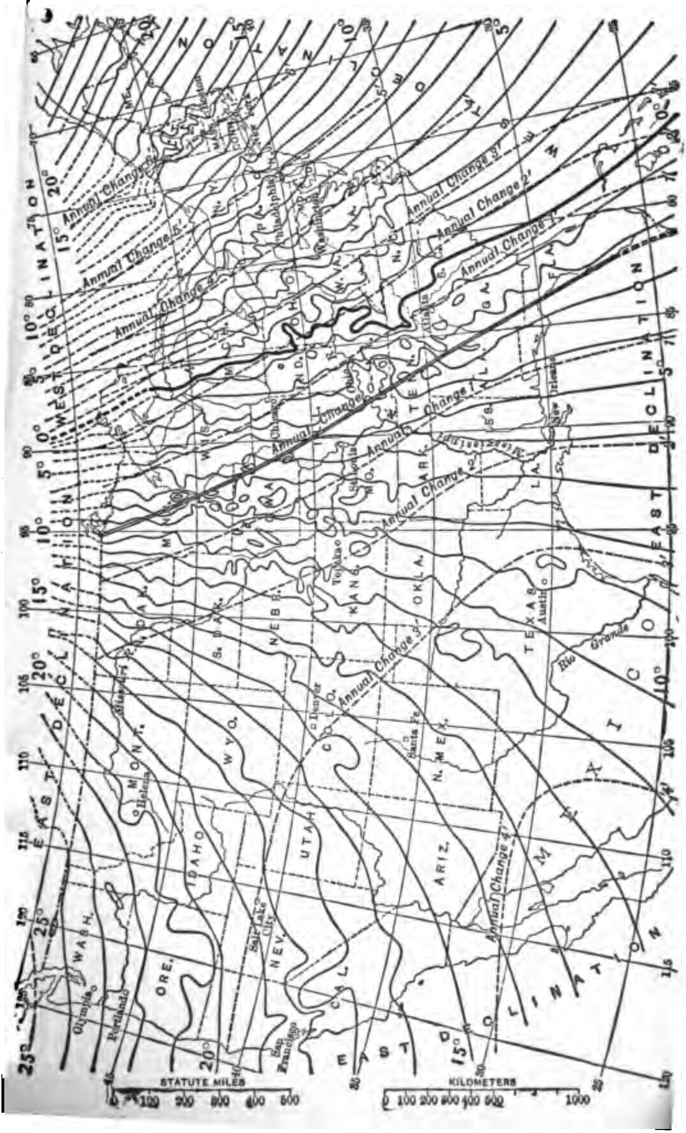
′	0°		1°		2°		3°		4°		
	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	
0	.00000	One.	.01745	.99985	.03490	.99939	.05234	.99863	.06976	.99756	60
1	.00029	One.	.01774	.99984	.03519	.99938	.05263	.99861	.07005	.99754	59
2	.00058	One.	.01803	.99984	.03548	.99937	.05292	.99860	.07034	.99752	58
3	.00087	One.	.01832	.99983	.03577	.99936	.05321	.99858	.07063	.99750	57
4	.00116	One.	.01862	.99983	.03606	.99935	.05350	.99857	.07092	.99748	56
5	.00145	One.	.01891	.99982	.03635	.99934	.05379	.99855	.07121	.99746	55
6	.00175	One.	.01920	.99982	.03664	.99933	.05408	.99854	.07150	.99744	54
7	.00204	One.	.01949	.99981	.03693	.99932	.05437	.99852	.07179	.99742	53
8	.00233	One.	.01978	.99980	.03723	.99931	.05466	.99851	.07208	.99740	52
9	.00262	One.	.02007	.99980	.03752	.99930	.05495	.99849	.07237	.99738	51
10	.00291	One.	.02036	.99979	.03781	.99929	.05524	.99847	.07266	.99736	50
11	.00320	.99999	.02065	.99979	.03810	.99927	.05553	.99846	.07295	.99734	49
12	.00349	.99999	.02094	.99978	.03839	.99926	.05582	.99844	.07324	.99731	48
13	.00378	.99999	.02123	.99977	.03868	.99925	.05611	.99842	.07353	.99729	47
14	.00407	.99999	.02152	.99977	.03897	.99924	.05640	.99841	.07382	.99727	46
15	.00436	.99999	.02181	.99976	.03926	.99923	.05669	.99839	.07411	.99725	45
16	.00465	.99999	.02211	.99976	.03955	.99922	.05698	.99838	.07440	.99723	44
17	.00495	.99999	.02240	.99975	.03984	.99921	.05727	.99836	.07469	.99721	43
18	.00524	.99999	.02269	.99974	.04013	.99919	.05756	.99834	.07498	.99719	42
19	.00553	.99998	.02298	.99974	.04042	.99918	.05785	.99833	.07527	.99716	41
20	.00582	.99998	.02327	.99973	.04071	.99917	.05814	.99831	.07556	.99714	40
21	.00611	.99998	.02356	.99972	.04100	.99916	.05844	.99829	.07585	.99712	39
22	.00640	.99998	.02385	.99972	.04129	.99915	.05873	.99827	.07614	.99710	38
23	.00669	.99998	.02414	.99971	.04159	.99913	.05902	.99826	.07643	.99708	37
24	.00698	.99998	.02443	.99970	.04188	.99912	.05931	.99824	.07672	.99705	36
25	.00727	.99997	.02472	.99969	.04217	.99911	.05960	.99822	.07701	.99703	35
26	.00756	.99997	.02501	.99969	.04246	.99910	.05989	.99821	.07730	.99701	34
27	.00785	.99997	.02530	.99968	.04275	.99909	.06018	.99819	.07759	.99699	33
28	.00814	.99997	.02560	.99967	.04304	.99907	.06047	.99817	.07788	.99696	32
29	.00844	.99996	.02589	.99966	.04333	.99906	.06076	.99815	.07817	.99694	31
30	.00873	.99996	.02618	.99966	.04362	.99905	.06105	.99813	.07846	.99692	30
31	.00902	.99996	.02647	.99965	.04391	.99904	.06134	.99812	.07875	.99689	29
32	.00931	.99996	.02676	.99964	.04420	.99902	.06163	.99810	.07904	.99687	28
33	.00960	.99995	.02705	.99963	.04449	.99901	.06192	.99808	.07933	.99685	27
34	.00989	.99995	.02734	.99963	.04478	.99900	.06221	.99806	.07962	.99683	26
35	.01018	.99995	.02763	.99962	.04507	.99898	.06250	.99804	.07991	.99680	25
36	.01047	.99995	.02792	.99961	.04536	.99897	.06279	.99803	.08020	.99678	24
37	.01076	.99994	.02821	.99960	.04565	.99896	.06308	.99801	.08049	.99676	23
38	.01105	.99994	.02850	.99959	.04594	.99894	.06337	.99799	.08078	.99673	22
39	.01134	.99994	.02879	.99959	.04623	.99893	.06366	.99797	.08107	.99671	21
40	.01164	.99993	.02908	.99958	.04653	.99892	.06395	.99795	.08136	.99668	20
41	.01193	.99993	.02938	.99957	.04682	.99890	.06424	.99793	.08165	.99666	19
42	.01222	.99993	.02967	.99956	.04711	.99889	.06453	.99792	.08194	.99664	18
43	.01251	.99992	.02996	.99955	.04740	.99888	.06482	.99790	.08223	.99661	17
44	.01280	.99992	.03025	.99954	.04769	.99886	.06511	.99788	.08252	.99659	16
45	.01309	.99991	.03054	.99953	.04798	.99885	.06540	.99786	.08281	.99657	15
46	.01338	.99991	.03083	.99952	.04827	.99883	.06569	.99784	.08310	.99654	14
47	.01367	.99991	.03112	.99952	.04856	.99882	.06598	.99782	.08339	.99652	13
48	.01396	.99990	.03141	.99951	.04885	.99881	.06627	.99780	.08368	.99649	12
49	.01425	.99990	.03170	.99950	.04914	.99879	.06656	.99778	.08397	.99647	11
50	.01454	.99989	.03199	.99949	.04943	.99878	.06685	.99776	.08426	.99644	10
51	.01483	.99989	.03228	.99948	.04972	.99876	.06714	.99774	.08455	.99642	9
52	.01513	.99989	.03257	.99947	.05001	.99875	.06743	.99772	.08484	.99639	8
53	.01542	.99988	.03286	.99946	.05030	.99873	.06773	.99770	.08513	.99637	7
54	.01571	.99988	.03316	.99945	.05059	.99872	.06802	.99768	.08542	.99635	6
55	.01600	.99987	.03345	.99944	.05088	.99870	.06831	.99766	.08571	.99632	5
56	.01629	.99987	.03374	.99943	.05117	.99869	.06860	.99764	.08600	.99630	4
57	.01658	.99986	.03403	.99942	.05146	.99867	.06889	.99762	.08629	.99627	3
58	.01687	.99986	.03432	.99941	.05175	.99866	.06918	.99760	.08658	.99625	2
59	.01716	.99985	.03461	.99940	.05205	.99864	.06947	.99758	.08687	.99622	1
60	.01745	.99985	.03490	.99939	.05234	.99863	.06976	.99756	.08716	.99619	0
	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	′
	89°		88°		87°		86°		85°		

′	5°		6°		7°		8°		9°		′
	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	
0	.08716	.99619	.10453	.99452	.12187	.99255	.13917	.99027	.15643	.98769	60
1	.08745	.99617	.10482	.99449	.12216	.99251	.13946	.99023	.15672	.98764	59
2	.08774	.99614	.10511	.99446	.12245	.99248	.13975	.99019	.15701	.98760	58
3	.08803	.99612	.10540	.99443	.12274	.99244	.14004	.99015	.15730	.98755	57
4	.08831	.99609	.10569	.99440	.12302	.99240	.14033	.99011	.15758	.98751	56
5	.08860	.99607	.10597	.99437	.12331	.99237	.14061	.99006	.15787	.98746	55
6	.08889	.99604	.10626	.99434	.12360	.99233	.14090	.99002	.15816	.98741	54
7	.08918	.99602	.10655	.99431	.12389	.99230	.14119	.98998	.15845	.98737	53
8	.08947	.99599	.10684	.99428	.12418	.99226	.14148	.98994	.15873	.98732	52
9	.08976	.99596	.10713	.99424	.12447	.99222	.14177	.98990	.15902	.98728	51
10	.09005	.99594	.10742	.99421	.12476	.99219	.14205	.98986	.15931	.98723	50
11	.09034	.99591	.10771	.99418	.12504	.99215	.14234	.98982	.15959	.98718	49
12	.09063	.99588	.10800	.99415	.12533	.99211	.14263	.98978	.15988	.98714	48
13	.09092	.99586	.10829	.99412	.12562	.99208	.14292	.98973	.16017	.98709	47
14	.09121	.99583	.10858	.99409	.12591	.99204	.14320	.98969	.16046	.98704	46
15	.09150	.99580	.10887	.99406	.12620	.99200	.14349	.98965	.16074	.98700	45
16	.09179	.99578	.10916	.99402	.12649	.99197	.14378	.98961	.16103	.98695	44
17	.09208	.99575	.10945	.99399	.12678	.99193	.14407	.98957	.16132	.98690	43
18	.09237	.99572	.10973	.99396	.12706	.99189	.14436	.98953	.16160	.98686	42
19	.09266	.99570	.11002	.99393	.12735	.99186	.14464	.98948	.16189	.98681	41
20	.09295	.99567	.11031	.99390	.12764	.99182	.14493	.98944	.16218	.98676	40
21	.09324	.99564	.11060	.99386	.12793	.99178	.14522	.98940	.16246	.98671	39
22	.09353	.99562	.11089	.99383	.12822	.99175	.14551	.98936	.16275	.98667	38
23	.09382	.99559	.11118	.99380	.12851	.99171	.14580	.98931	.16304	.98662	37
24	.09411	.99556	.11147	.99377	.12880	.99167	.14608	.98927	.16333	.98657	36
25	.09440	.99553	.11176	.99374	.12908	.99163	.14637	.98923	.16361	.98652	35
26	.09469	.99551	.11205	.99370	.12937	.99160	.14666	.98919	.16390	.98648	34
27	.09498	.99548	.11234	.99367	.12966	.99156	.14695	.98914	.16419	.98643	33
28	.09527	.99545	.11263	.99364	.12995	.99152	.14723	.98910	.16447	.98638	32
29	.09556	.99542	.11291	.99360	.13024	.99148	.14752	.98906	.16476	.98633	31
30	.09585	.99540	.11320	.99357	.13053	.99144	.14781	.98902	.16505	.98629	30
31	.09614	.99537	.11349	.99354	.13081	.99141	.14810	.98897	.16533	.98624	29
32	.09642	.99534	.11378	.99351	.13110	.99137	.14838	.98893	.16562	.98619	28
33	.09671	.99531	.11407	.99347	.13139	.99133	.14867	.98889	.16591	.98614	27
34	.09700	.99528	.11436	.99344	.13168	.99129	.14896	.98884	.16620	.98609	26
35	.09729	.99526	.11465	.99341	.13197	.99125	.14925	.98880	.16648	.98604	25
36	.09758	.99523	.11494	.99337	.13226	.99122	.14954	.98876	.16677	.98600	24
37	.09787	.99520	.11523	.99334	.13254	.99118	.14982	.98871	.16706	.98595	23
38	.09816	.99517	.11552	.99331	.13283	.99114	.15011	.98867	.16734	.98590	22
39	.09845	.99514	.11580	.99327	.13312	.99110	.15040	.98863	.16763	.98585	21
40	.09874	.99511	.11609	.99324	.13341	.99106	.15069	.98858	.16792	.98580	20
41	.09903	.99508	.11638	.99320	.13370	.99102	.15097	.98854	.16820	.98575	19
42	.09932	.99506	.11667	.99317	.13399	.99098	.15126	.98849	.16849	.98570	18
43	.09961	.99503	.11696	.99314	.13427	.99094	.15155	.98845	.16878	.98565	17
44	.09990	.99500	.11725	.99310	.13456	.99091	.15184	.98841	.16906	.98561	16
45	.10019	.99497	.11754	.99307	.13485	.99087	.15212	.98836	.16935	.98556	15
46	.10048	.99494	.11783	.99303	.13514	.99083	.15241	.98832	.16964	.98551	14
47	.10077	.99491	.11812	.99300	.13543	.99079	.15270	.98827	.16992	.98546	13
48	.10106	.99488	.11840	.99297	.13572	.99075	.15299	.98823	.17021	.98541	12
49	.10135	.99485	.11869	.99293	.13600	.99071	.15327	.98818	.17050	.98536	11
50	.10164	.99482	.11898	.99290	.13629	.99067	.15356	.98814	.17078	.98531	10
51	.10192	.99479	.11927	.99286	.13658	.99063	.15385	.98809	.17107	.98526	9
52	.10221	.99476	.11956	.99283	.13687	.99059	.15414	.98805	.17136	.98521	8
53	.10250	.99473	.11985	.99279	.13716	.99055	.15442	.98800	.17164	.98516	7
54	.10279	.99470	.12014	.99276	.13744	.99051	.15471	.98796	.17193	.98511	6
55	.10308	.99467	.12043	.99272	.13773	.99047	.15500	.98791	.17222	.98506	5
56	.10337	.99464	.12071	.99269	.13802	.99043	.15529	.98787	.17250	.98501	4
57	10366	.99461	.12100	.99265	.13831	.99039	.15557	.98782	.17279	.98496	3
58	.10395	.99458	.12129	.99262	.13860	.99035	.15586	.98778	.17308	.98491	2
59	.10424	.99455	.12158	.99258	.13889	.99031	.15615	.98773	.17336	.98486	1
60	.10453	.99452	.12187	.99255	.13917	.99027	.15643	.98769	.17365	.98481	0
′	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	′
	84°		83°		82°		81°		80°		

′	10° Sine	10° Cosin	11° Sine	11° Cosin	12° Sine	12° Cosin	13° Sine	13° Cosin	14° Sine	14° Cosin	′
0	.17365	.98481	.19081	.98163	.20791	.97815	.22495	.97437	.24192	.97030	60
1	.17393	.98476	.19109	.98157	.20820	.97809	.22523	.97430	.24220	.97023	59
2	.17422	.98471	.19138	.98152	.20848	.97803	.22552	.97424	.24249	.97015	58
3	.17451	.98466	.19167	.98146	.20877	.97797	.22580	.97417	.24277	.97008	57
4	.17479	.98461	.19195	.98140	.20905	.97791	.22608	.97411	.24305	.97001	56
5	.17508	.98455	.19224	.98135	.20933	.97784	.22637	.97404	.24333	.96994	55
6	.17537	.98450	.19252	.98129	.20962	.97778	.22665	.97398	.24362	.96987	54
7	.17565	.98445	.19281	.98124	.20990	.97772	.22693	.97391	.24390	.96980	53
8	.17594	.98440	.19309	.98118	.21019	.97766	.22722	.97384	.24418	.96973	52
9	.17623	.98435	.19338	.98112	.21047	.97760	.22750	.97378	.24446	.96966	51
10	.17651	.98430	.19366	.98107	.21076	.97754	.22778	.97371	.24474	.96959	50
11	.17680	.98425	.19395	.98101	.21104	.97748	.22807	.97365	.24503	.96952	49
12	.17708	.98420	.19423	.98096	.21132	.97742	.22835	.97358	.24531	.96945	48
13	.17737	.98414	.19452	.98090	.21161	.97735	.22863	.97351	.24559	.96937	47
14	.17766	.98409	.19481	.98084	.21189	.97729	.22892	.97345	.24587	.96930	46
15	.17794	.98404	.19509	.98079	.21218	.97723	.22920	.97338	.24615	.96923	45
16	.17823	.98399	.19538	.98073	.21246	.97717	.22948	.97331	.24644	.96916	44
17	.17852	.98394	.19566	.98067	.21275	.97711	.22977	.97325	.24672	.96909	43
18	.17880	.98389	.19595	.98061	.21303	.97705	.23005	.97318	.24700	.96902	42
19	.17909	.98383	.19623	.98056	.21331	.97698	.23033	.97311	.24728	.96894	41
20	.17937	.98378	.19652	.98050	.21360	.97692	.23062	.97304	.24756	.96887	40
21	.17966	.98373	.19680	.98044	.21388	.97686	.23090	.97298	.24784	.96880	39
22	.17995	.98368	.19709	.98039	.21417	.97680	.23118	.97291	.24813	.96873	38
23	.18023	.98362	.19737	.98033	.21445	.97673	.23146	.97284	.24841	.96866	37
24	.18052	.98357	.19766	.98027	.21474	.97667	.23175	.97278	.24869	.96858	36
25	.18081	.98352	.19794	.98021	.21502	.97661	.23203	.97271	.24897	.96851	35
26	.18109	.98347	.19823	.98016	.21530	.97655	.23231	.97264	.24925	.96844	34
27	.18138	.98341	.19851	.98010	.21559	.97648	.23260	.97257	.24954	.96837	33
28	.18166	.98336	.19880	.98004	.21587	.97642	.23288	.97251	.24982	.96829	32
29	.18195	.98331	.19908	.97998	.21616	.97636	.23316	.97244	.25010	.96822	31
30	.18224	.98325	.19937	.97992	.21644	.97630	.23345	.97237	.25038	.96815	30
31	.18252	.98320	.19965	.97987	.21672	.97623	.23373	.97230	.25066	.96807	29
32	.18281	.98315	.19994	.97981	.21701	.97617	.23401	.97223	.25094	.96800	28
33	.18309	.98310	.20022	.97975	.21729	.97611	.23429	.97217	.25122	.96793	27
34	.18338	.98304	.20051	.97969	.21758	.97604	.23458	.97210	.25151	.96786	26
35	.18367	.98299	.20079	.97963	.21786	.97598	.23486	.97203	.25179	.96778	25
36	.18395	.98294	.20108	.97958	.21814	.97592	.23514	.97196	.25207	.96771	24
37	.18424	.98288	.20136	.97952	.21843	.97585	.23542	.97189	.25235	.96764	23
38	.18452	.98283	.20165	.97946	.21871	.97579	.23571	.97182	.25263	.96756	22
39	.18481	.98277	.20193	.97940	.21899	.97573	.23599	.97176	.25291	.96749	21
40	.18509	.98272	.20222	.97934	.21928	.97566	.23627	.97169	.25320	.96742	20
41	.18538	.98267	.20250	.97928	.21956	.97560	.23656	.97162	.25348	.96734	19
42	.18567	.98261	.20279	.97922	.21985	.97553	.23684	.97155	.25376	.96727	18
43	.18595	.98256	.20307	.97916	.22013	.97547	.23712	.97148	.25404	.96719	17
44	.18624	.98250	.20336	.97910	.22041	.97541	.23740	.97141	.25432	.96712	16
45	.18652	.98245	.20364	.97905	.22070	.97534	.23769	.97134	.25460	.96705	15
46	.18681	.98240	.20393	.97899	.22098	.97528	.23797	.97127	.25488	.96697	14
47	.18710	.98234	.20421	.97893	.22126	.97521	.23825	.97120	.25516	.96690	13
48	.18738	.98229	.20450	.97887	.22155	.97515	.23853	.97113	.25545	.96682	12
49	.18767	.98223	.20478	.97881	.22183	.97508	.23882	.97106	.25573	.96675	11
50	.18795	.98218	.20507	.97875	.22212	.97502	.23910	.97100	.25601	.96667	10
51	.18824	.98212	.20535	.97869	.22240	.97496	.23938	.97093	.25629	.96660	9
52	.18852	.98207	.20563	.97863	.22268	.97489	.23966	.97086	.25657	.96653	8
53	.18881	.98201	.20592	.97857	.22297	.97483	.23995	.97079	.25685	.96645	7
54	.18910	.98196	.20620	.97851	.22325	.97476	.24023	.97072	.25713	.96638	6
55	.18938	.98190	.20649	.97845	.22353	.97470	.24051	.97065	.25741	.96630	5
56	.18967	.98185	.20677	.97839	.22382	.97463	.24079	.97058	.25769	.96623	4
57	.18995	.98179	.20706	.97833	.22410	.97457	.24108	.97051	.25798	.96615	3
58	.19024	.98174	.20734	.97827	.22438	.97450	.24136	.97044	.25826	.96608	2
59	.19052	.98168	.20763	.97821	.22467	.97444	.24164	.97037	.25854	.96600	1
60	.19081	.98163	.20791	.97815	.22495	.97437	.24192	.97030	.25882	.96593	0
′	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	′
	79°		78°		77°		76°		75°		

′	15° Sine	15° Cosin	16° Sine	16° Cosin	17° Sine	17° Cosin	18° Sine	18° Cosin	19° Sine	19° Cosin	′
0	.25882	.96593	.27564	.96126	.29237	.95630	.30902	.95106	.32557	.94552	60
1	.25910	.96585	.27592	.96118	.29265	.95622	.30929	.95097	.32584	.94542	59
2	.25938	.96578	.27620	.96110	.29293	.95613	.30957	.95088	.32612	.94533	58
3	.25966	.96570	.27648	.96102	.29321	.95605	.30985	.95079	.32639	.94523	57
4	.25994	.96562	.27676	.96094	.29348	.95596	.31012	.95070	.32667	.94514	56
5	.26022	.96555	.27704	.96086	.29376	.95588	.31040	.95061	.32694	.94504	55
6	.26050	.96547	.27731	.96078	.29404	.95579	.31068	.95052	.32722	.94495	54
7	.26079	.96540	.27759	.96070	.29432	.95571	.31095	.95043	.32749	.94485	53
8	.26107	.96532	.27787	.96062	.29460	.95562	.31123	.95033	.32777	.94476	52
9	.26135	.96524	.27815	.96054	.29487	.95554	.31151	.95024	.32804	.94466	51
10	.26163	.96517	.27843	.96046	.29515	.95545	.31178	.95015	.32832	.94457	50
11	.26191	.96509	.27871	.96037	.29543	.95536	.31206	.95006	.32859	.94447	49
12	.26219	.96502	.27899	.96029	.29571	.95528	.31233	.94997	.32887	.94438	48
13	.26247	.96494	.27927	.96021	.29599	.95519	.31261	.94988	.32914	.94428	47
14	.26275	.96486	.27955	.96013	.29626	.95511	.31289	.94979	.32942	.94418	46
15	.26303	.96479	.27983	.96005	.29654	.95502	.31316	.94970	.32969	.94409	45
16	.26331	.96471	.28011	.95997	.29682	.95493	.31344	.94961	.32997	.94399	44
17	.26359	.96463	.28039	.95989	.29710	.95485	.31372	.94952	.33024	.94390	43
18	.26387	.96456	.28067	.95981	.29737	.95476	.31399	.94943	.33051	.94380	42
19	.26415	.96448	.28095	.95972	.29765	.95467	.31427	.94933	.33079	.94370	41
20	.26443	.96440	.28123	.95964	.29793	.95459	.31454	.94924	.33106	.94361	40
21	.26471	.96433	.28150	.95956	.29821	.95450	.31482	.94915	.33134	.94351	39
22	.26500	.96425	.28178	.95948	.29849	.95441	.31510	.94906	.33161	.94342	38
23	.26528	.96417	.28206	.95940	.29876	.95433	.31537	.94897	.33189	.94332	37
24	.26556	.96410	.28234	.95931	.29904	.95424	.31565	.94888	.33216	.94322	36
25	.26584	.96402	.28262	.95923	.29932	.95415	.31593	.94878	.33244	.94313	35
26	.26612	.96394	.28290	.95915	.29960	.95407	.31620	.94869	.33271	.94303	34
27	.26640	.96386	.28318	.95907	.29987	.95398	.31648	.94860	.33298	.94293	33
28	.26668	.96379	.28346	.95898	.30015	.95389	.31675	.94851	.33326	.94284	32
29	.26696	.96371	.28374	.95890	.30043	.95380	.31703	.94842	.33353	.94274	31
30	.26724	.96363	.28402	.95882	.30071	.95372	.31730	.94832	.33381	.94264	30
31	.26752	.96355	.28429	.95874	.30098	.95363	.31758	.94823	.33408	.94254	29
32	.26780	.96347	.28457	.95865	.30126	.95354	.31786	.94814	.33436	.94245	28
33	.26808	.96340	.28485	.95857	.30154	.95345	.31813	.94805	.33463	.94235	27
34	.26836	.96332	.28513	.95849	.30182	.95337	.31841	.94795	.33490	.94225	26
35	.26864	.96324	.28541	.95841	.30209	.95328	.31868	.94786	.33518	.94215	25
36	.26892	.96316	.28569	.95832	.30237	.95319	.31896	.94777	.33545	.94206	24
37	.26920	.96308	.28597	.95824	.30265	.95310	.31923	.94768	.33573	.94196	23
38	.26948	.96301	.28625	.95816	.30292	.95301	.31951	.94758	.33600	.94186	22
39	.26976	.96293	.28652	.95807	.30320	.95293	.31979	.94749	.33627	.94176	21
40	.27004	.96285	.28680	.95799	.30348	.95284	.32006	.94740	.33655	.94167	20
41	.27032	.96277	.28708	.95791	.30376	.95275	.32034	.94730	.33682	.94157	19
42	.27060	.96269	.28736	.95782	.30403	.95266	.32061	.94721	.33710	.94147	18
43	.27088	.96261	.28764	.95774	.30431	.95257	.32089	.94712	.33737	.94137	17
44	.27116	.96253	.28792	.95766	.30459	.95248	.32116	.94702	.33764	.94127	16
45	.27144	.96246	.28820	.95757	.30486	.95240	.32144	.94693	.33792	.94118	15
46	.27172	.96238	.28847	.95749	.30514	.95231	.32171	.94684	.33819	.94108	14
47	.27200	.96230	.28875	.95740	.30542	.95222	.32199	.94674	.33846	.94098	13
48	.27228	.96222	.28903	.95732	.30570	.95213	.32227	.94665	.33874	.94088	12
49	.27256	.96214	.28931	.95724	.30597	.95204	.32254	.94656	.33901	.94078	11
50	.27284	.96206	.28959	.95715	.30625	.95195	.32282	.94646	.33929	.94068	10
51	.27312	.96198	.28987	.95707	.30653	.95186	.32309	.94637	.33956	.94058	9
52	.27340	.96190	.29015	.95698	.30680	.95177	.32337	.94627	.33983	.94049	8
53	.27368	.96182	.29042	.95690	.30708	.95168	.32364	.94618	.34011	.94039	7
54	.27396	.96174	.29070	.95681	.30736	.95159	.32392	.94609	.34038	.94029	6
55	.27424	.96166	.29098	.95673	.30763	.95150	.32419	.94599	.34065	.94019	5
56	.27452	.96158	.29126	.95664	.30791	.95142	.32447	.94590	.34093	.94009	4
57	.27480	.96150	.29154	.95656	.30819	.95133	.32474	.94580	.34120	.93999	3
58	.27508	.96142	.29182	.95647	.30846	.95124	.32502	.94571	.34147	.93989	2
59	.27536	.96134	.29209	.95639	.30874	.95115	.32529	.94561	.34175	.93979	1
60	.27564	.96126	.29237	.95630	.30902	.95106	.32557	.94552	.34202	.93969	0
′	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	′
	74°		73°		72°		71°		70°		

PLATE I. ISOGONIC' MAP OF U. S. FOR 1915.



′	30° Sine	30° Cosin	31° Sine	31° Cosin	32° Sine	32° Cosin	33° Sine	33° Cosin	34° Sine	34° Cosin	′
0	.50000	.86603	.51504	.85717	.52992	.84805	.54464	.83867	.55919	.82904	60
1	.50025	.86588	.51529	.85702	.53017	.84789	.54488	.83851	.55943	.82887	59
2	.50050	.86573	.51554	.85687	.53041	.84774	.54513	.83835	.55968	.82871	58
3	.50076	.86559	.51579	.85672	.53066	.84759	.54537	.83819	.55992	.82855	57
4	.50101	.86544	.51604	.85657	.53091	.84743	.54561	.83804	.56016	.82839	56
5	.50126	.86530	.51628	.85642	.53115	.84728	.54586	.83788	.56040	.82822	55
6	.50151	.86515	.51653	.85627	.53140	.84712	.54610	.83772	.56064	.82806	54
7	.50176	.86501	.51678	.85612	.53164	.84697	.54635	.83756	.56088	.82790	53
8	.50201	.86486	.51703	.85597	.53189	.84681	.54659	.83740	.56112	.82773	52
9	.50227	.86471	.51728	.85582	.53214	.84666	.54683	.83724	.56136	.82757	51
10	.50252	.86457	.51753	.85567	.53238	.84650	.54708	.83708	.56160	.82741	50
11	.50277	.86442	.51778	.85551	.53263	.84635	.54732	.83692	.56184	.82724	49
12	.50302	.86427	.51803	.85536	.53288	.84619	.54756	.83676	.56208	.82708	48
13	.50327	.86413	.51828	.85521	.53312	.84604	.54781	.83660	.56232	.82692	47
14	.50352	.86398	.51852	.85506	.53337	.84588	.54805	.83645	.56256	.82675	46
15	.50377	.86384	.51877	.85491	.53361	.84573	.54829	.83629	.56280	.82659	45
16	.50403	.86369	.51902	.85476	.53386	.84557	.54854	.83613	.56305	.82643	44
17	.50428	.86354	.51927	.85461	.53411	.84542	.54878	.83597	.56329	.82626	43
18	.50453	.86340	.51952	.85446	.53435	84526	.54902	.83581	.56353	.82610	42
19	.50478	.86325	.51977	.85431	.53460	.84511	.54927	.83565	.56377	.82593	41
20	.50503	.86310	.52002	.85416	.53484	.84495	.54951	.83549	.56401	.82577	40
21	.50528	.86295	.52026	.85401	.53509	.84480	.54975	.83533	.56425	.82561	39
22	.50553	.86281	.52051	.85385	.53534	.84464	54999	.83517	.56449	.82544	38
23	.50578	.86266	.52076	.85370	.53558	.84448	.55024	.83501	.56473	.82528	37
24	.50603	.86251	.52101	.85355	.53583	.84433	.55048	.83485	.56497	.82511	36
25	.50628	.86237	.52126	.85340	.53607	.84417	.55072	.83469	.56521	.82495	35
26	.50654	.86222	.52151	.85325	.53632	.84402	.55097	.83453	.56545	.82478	34
27	.50679	.86207	.52175	.85310	.53656	.84386	.55121	.83437	.56569	.82462	33
28	.50704	.86192	.52200	.85294	.53681	.84370	.55145	.83421	.56593	.82446	32
29	.50729	.86178	.52225	.85279	.53705	.84355	.55169	.83405	.56617	.82429	31
30	.50754	.86163	.52250	.85264	.53730	.84339	.55194	.83389	56641	.82413	30
31	.50779	.86148	.52275	.85249	.53754	.84324	.55218	.83373	.56665	.82396	29
32	.50804	.86133	.52299	.85234	.53779	.84308	.55242	.83356	.56689	82380	28
33	.50829	.86119	.52324	.85218	.53804	.84292	.55266	.83340	.56713	.82363	27
34	.50854	.86104	.52349	.85203	.53828	.84277	.55291	.83324	.56736	.82347	26
35	.50879	.86089	.52374	.85188	.53853	.84261	.55315	.83308	.56760	.82330	25
36	.50904	.86074	.52399	.85173	.53877	.84245	.55339	.83292	.56784	.82314	24
37	.50929	.86059	.52423	.85157	.53902	.84230	.55363	.83276	.56808	.82297	23
38	.50954	.86045	.52448	.85142	.53926	.84214	.55388	.83260	.56832	.82281	22
39	.50979	.86030	.52473	.85127	.53951	.84198	.55412	.83244	.56856	.82264	21
40	.51004	86015	.52498	.85112	.53975	.84182	.55436	.83228	.56880	.82248	20
41	.51029	.86000	.52522	.85096	.54000	.84167	.55460	.83212	.56904	.82231	19
42	.51054	.85985	.52547	.85081	.54024	.84151	.55484	.83195	.56928	.82214	18
43	.51079	.85970	.52572	.85066	.54049	.84135	.55509	.83179	.56952	.82198	17
44	.51104	.85956	.52597	.85051	.54073	.84120	.55533	.83163	.56976	.82181	16
45	.51129	.85941	.52621	.85035	.54097	.84104	.55557	.83147	.57000	.82165	15
46	.51154	.85926	.52646	.85020	.54122	.84088	.55581	.83131	.57024	.82148	14
47	.51179	.85911	.52671	.85005	.54146	.84072	.55605	.83115	.57047	.82132	13
48	.51204	.85896	.52696	.84989	.54171	.84057	.55630	.83098	.57071	.82115	12
49	.51229	.85881	.52720	.84974	.54195	.84041	.55654	.83082	.57095	.82098	11
50	.512[illegible]	.85866	.52745	.84959	.54220	.84025	.55678	.83066	.57119	.82082	10
51	.51279	.85851	.52770	.84943	.54244	.84009	.55702	.83050	.57143	.82065	9
52	.51304	.85836	.52794	.84928	.54269	.83994	.55726	.83034	.57167	.82048	8
53	.51329	.85821	.52819	.84913	.54293	.83978	.55750	.83017	.57191	.82032	7
54	.51354	.85806	.52844	.84897	.54317	.83962	.55775	.83001	.57215	.82015	6
55	.51379	.85792	.52869	.84882	.54342	.83946	.55799	.82985	.57238	.81999	5
56	.51404	.85777	.52893	.84866	.54366	.83930	.55823	.82969	.57262	.81982	4
57	.51429	.85762	.52918	.84851	.54391	.83915	.55847	.82953	.57286	.81965	3
58	.51454	.85747	.52943	.84836	.54415	.83899	.55871	.82936	.57310	.81949	2
59	.51479	.85732	.52967	.84820	.54440	.83883	.55895	.82920	.57334	.81932	1
60	.51504	.85717	.52992	.84805	.54464	.83867	.55919	.82904	.57358	.81915	0
′	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	′
	59°		58°		57°		56°		55°		

′	35°		36°		37°		38°		39°		′
	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	
0	.57358	.81915	.58779	.80902	.60182	.79864	.61566	.78801	.62932	.77715	60
1	.57381	.81899	.58802	.80885	.60205	.79846	.61589	.78783	.62955	.77696	59
2	.57405	.81882	.58826	.80867	.60228	.79829	.61612	.78765	.62977	.77678	58
3	.57429	.81865	.58849	.80850	.60251	.79811	.61635	.78747	.63000	.77660	57
4	.57453	.81848	.58873	.80833	.60274	.79793	.61658	.78729	.63022	.77641	56
5	.57477	.81832	.58896	.80816	.60298	.79776	.61681	.78711	.63045	.77623	55
6	.57501	.81815	.58920	.80799	.60321	.79758	.61704	.78694	.63068	.77605	54
7	.57524	.81798	.58943	.80782	.60344	.79741	.61726	.78676	.63090	.77586	53
8	.57548	.81782	.58967	.80765	.60367	.79723	.61749	.78658	.63113	.77568	52
9	.57572	.81765	.58990	.80748	.60390	.79706	.61772	.78640	.63135	.77550	51
10	.57596	.81748	.59014	.80730	.60414	.79688	.61795	.78622	.63158	.77531	50
11	.57619	.81731	.59037	.80713	.60437	.79671	.61818	.78604	.63180	.77513	40
12	.57643	.81714	.59061	.80696	.60460	.79653	.61841	.78586	.63203	.77494	48
13	.57667	.81698	.59084	.80679	.60483	.79635	.61864	.78568	.63225	.77476	47
14	.57691	.81681	.59108	.80662	.60506	.79618	.61887	.78550	.63248	.77458	46
15	.57715	.81664	.59131	.80644	.60529	.79600	.61909	.78532	.63271	.77439	45
16	.57738	.81647	.59154	.80627	.60553	.79583	.61932	.78514	.63293	.77421	44
17	.57762	.81631	.59178	.80610	.60576	.79565	.61955	.78496	.63316	.77402	43
18	.57786	.81614	.59201	.80593	.60599	.79547	.61978	.78478	.63338	.77384	42
19	.57810	.81597	.59225	.80576	.60622	.79530	.62001	.78460	.63361	.77366	41
20	.57833	.81580	.59248	.80558	.60645	.79512	.62024	.78442	.63383	.77347	40
21	.57857	.81563	.59272	.80541	.60668	.79494	.62046	.78424	.63406	.77329	39
22	.57881	.81546	.59295	.80524	.60691	.79477	.62069	.78405	.63428	.77310	38
23	.57904	.81530	.59318	.80507	.60714	.79459	.62092	.78387	.63451	.77292	37
24	.57928	.81513	.59342	.80489	.60738	.79441	.62115	.78369	.63473	.77273	36
25	.57952	.81496	.59365	.80472	.60761	.79424	.62138	.78351	.63496	.77255	35
26	.57976	.81479	.59389	.80455	.60784	.79406	.62160	.78333	.63518	.77236	34
27	.57999	.81462	.59412	.80438	.60807	.79388	.62183	.78315	.63540	.77218	33
28	.58023	.81445	.59436	.80420	.60830	.79371	.62206	.78297	.63563	.77199	32
29	.58047	.81428	.59459	.80403	60853	.79353	.62229	.78279	.63585	.77181	31
30	.58070	.81412	.59482	.80386	.60876	.79335	.62251	.78261	.63608	.77162	30
31	.58094	.81395	.59506	.80368	.60899	.79318	.62274	.78243	.63630	.77144	29
32	.58118	.81378	.59529	.80351	.60922	.79300	.62297	.78225	.63653	.77125	28
33	.58141	.81361	.59552	.80334	.60945	.79282	.62320	.78206	.63675	.77107	27
34	.58165	.81344	.59576	.80316	.60968	.79264	.62342	.78188	.63698	.77088	26
35	.58189	.81327	.59599	.80299	.60991	.79247	.62365	.78170	.63720	.77070	25
36	.58212	.81310	.59622	.80282	.61015	.79229	.62388	.78152	.63742	.77051	24
37	.58236	.81293	.59646	.80264	.61038	.79211	.62411	.78134	.63765	.77033	23
38	.58260	.81276	.59669	.80247	.61061	.79193	.62433	.78116	.63787	.77014	22
39	.58283	.81259	.59693	.80230	.61084	.79176	.62456	.78098	.63810	.76996	21
40	.58307	.81242	.59716	.80212	.61107	.79158	.62479	.78079	.63832	.76977	20
41	.58330	.81225	.59739	.80195	.61130	.79140	.62502	.78061	.63854	.76959	19
42	.58354	.81208	.59763	.80178	.61153	.79122	.62524	.78043	.63877	.76940	18
43	.58378	.81191	.59786	.80160	.61176	.79105	.62547	.78025	.63899	.76921	17
44	.58401	.81174	.59809	.80143	.61199	.79087	.62570	.78007	.63922	.76903	16
45	.58425	.81157	.59832	.80125	.61222	.79069	.62592	.77988	.63944	.76884	15
46	.58449	.81140	.59856	.80108	.61245	.79051	.62615	.77970	.63966	.76866	14
47	.58472	.81123	.59879	.80091	.61268	.79033	.62638	.77952	.63989	.76847	13
48	.58496	.81106	.59902	.80073	.61291	.79016	.62660	.77934	.64011	.76828	12
49	.58519	.81089	.59926	.80056	.61314	.78998	.62683	.77916	.64033	.76810	11
50	.58543	.81072	.59949	.80038	.61337	.78980	.62706	.77897	.64056	.76791	10
51	.58567	.81055	.59972	.80021	.61360	.78962	.62728	.77879	.64078	.76772	9
52	.58590	.81038	.59995	.80003	.61383	.78944	.62751	.77861	.64100	.76754	8
53	.58614	.81021	.60019	.79986	.61406	.78926	.62774	.77843	.64123	.76735	7
54	.58637	.81004	.60042	.79968	.61429	.78908	.62796	.77824	.64145	.76717	6
55	.58661	.80987	.60065	.79951	.61451	.78891	.62819	.77806	.64167	.76698	5
56	.58684	.80970	.60089	.79934	.61474	.78873	.62842	.77788	.64190	.76679	4
57	.58708	.80953	.60112	.79916	.61497	.78855	.62864	.77769	.64212	.76661	3
58	.58731	.80936	.60135	.79899	.61520	.78837	.62887	.77751	.64234	.76642	2
59	.58755	.80919	.60158	.79881	.61543	.78819	.62909	.77733	.64256	.76623	1
60	.58779	.80902	.60182	.79864	.61566	.78801	.62932	.77715	.64279	.76604	0
′	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	′
	54°		53°		52°		51°		50°		

′	40°		41°		42°		43°		44°		′
	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	
0	.64279	.76604	.65606	.75471	.66913	.74314	.68200	.73135	.69466	.71934	60
1	.64301	.76586	.65628	.75452	.66935	.74295	.68221	.73116	.69487	.71914	59
2	.64323	.76567	.65650	.75433	.66956	.74276	.68242	.73096	.69508	.71894	58
3	.64346	.76548	.65672	.75414	.66978	.74256	.68264	.73076	.69529	.71873	57
4	.64368	.76530	.65694	.75395	.66999	.74237	.68285	.73056	.69549	.71853	56
5	.64390	.76511	.65716	.75375	.67021	.74217	.68306	.73036	.69570	.71833	55
6	.64412	.76492	.65738	.75356	.67043	.74198	.68327	.73016	.69591	.71813	54
7	.64435	.76473	.65759	.75337	.67064	.74178	.68349	.72996	.69612	.71792	53
8	.64457	.76455	.65781	.75318	.67086	.74159	.68370	.72976	.69633	.71772	52
9	.64479	.76436	.65803	.75299	.67107	.74139	.68391	.72957	.69654	.71752	51
10	.64501	.76417	.65825	.75280	.67129	.74120	.68412	.72937	.69675	.71732	50
11	.64524	.76398	.65847	.75261	.67151	.74100	.68434	.72917	.69696	.71711	49
12	.64546	.76380	.65869	.75241	.67172	.74080	.68455	.72897	.69717	.71691	48
13	.64568	.76361	.65891	.75222	.67194	.74061	.68476	.72877	.69737	.71671	47
14	.64590	.76342	.65913	.75203	.67215	.74041	.68497	.72857	.69758	.71650	46
15	.64612	.76323	.65935	.75184	.67237	.74022	.68518	.72837	.69779	.71630	45
16	.64635	.76304	.65956	.75165	.67258	.74002	.68539	.72817	.69800	.71610	44
17	.64657	.76286	.65978	.75146	.67280	.73983	.68561	.72797	.69821	.71590	43
18	.64679	.76267	.66000	.75126	.67301	.73963	.68582	.72777	.69842	.71569	42
19	.64701	.76248	.66022	.75107	.67323	.73944	.68603	.72757	.69862	.71549	41
20	.64723	.76229	.66044	.75088	.67344	.73924	.68624	.72737	.69883	.71529	40
21	.64746	.76210	.66066	.75069	.67366	.73904	.68645	.72717	.69904	.71508	39
22	.64768	.76192	.66088	.75050	.67387	.73885	.68666	.72697	.69925	.71488	38
23	.64790	.76173	.66109	.75030	.67409	.73865	.68688	.72677	.69946	.71468	37
24	.64812	.76154	.66131	.75011	.67430	.73846	.68709	.72657	.69966	.71447	36
25	.64834	.76135	.66153	.74992	.67452	.73826	.68730	.72637	.69987	.71427	35
26	.64856	.76116	.66175	.74973	.67473	.73806	.68751	.72617	.70008	.71407	34
27	.64878	.76097	.66197	.74953	.67495	.73787	.68772	.72597	.70029	.71386	33
28	.64901	.76078	.66218	.74934	.67516	.73767	.68793	.72577	.70049	.71366	32
29	.64923	.76059	.66240	.74915	.67538	.73747	.68814	.72557	.70070	.71345	31
30	.64945	.76041	.66262	.74896	.67559	.73728	.68835	.72537	.70091	.71325	30
31	.64967	.76022	.66284	.74876	.67580	.73708	.68857	.72517	.70112	.71305	29
32	.64989	.76003	.66306	.74857	.67602	.73688	.68878	.72497	70132	.71284	28
33	.65011	.75984	.66327	.74838	.67623	.73669	.68899	.72477	.70153	.71264	27
34	.65033	.75965	.66349	74818	.67645	.73649	.68920	.72457	.70174	.71243	26
35	.65055	.75946	.66371	.74799	.67666	.73629	.68941	.72437	.70195	.71223	35
36	.65077	.75927	.66393	.74780	.67688	.73610	.68962	.72417	.70215	.71203	24
37	.65100	.75908	.66414	.74760	.67709	.73590	.68983	.72397	.70236	.71182	23
38	.65122	.75889	.66436	.74741	.67730	73570	.69004	.72377	.70257	.71162	22
39	.65144	.75870	.66458	.74722	.67752	.73551	.69025	.72357	.70277	.71141	21
40	.65166	.75851	.66480	.74703	.67773	.73531	.69046	.72337	.70298	.71121	20
41	.65188	.75832	.66501	.74683	.67795	.73511	.69067	.72317	.70319	.71100	19
42	.65210	.75813	.66523	.74664	.67816	.73491	.69088	.72297	.70339	.71080	18
43	.65232	.75794	.66545	.74644	.67837	.73472	.69109	.72277	.70360	.71059	17
44	.65254	.75775	.66566	.74625	.67859	.73452	.69130	.72257	.70381	.71039	16
45	.65276	.75756	.66588	.74606	.67880	.73432	.69151	.72236	.70401	.71019	15
46	.65298	.75738	.66610	.74586	.67901	.73413	.69172	.72216	.70422	.70998	14
47	.65320	.75719	.66632	.74567	.67923	.73393	.69193	.72196	.70443	.70978	13
48	.65342	.75700	.66653	.74548	.67944	.73373	.69214	.72176	.70463	.70957	12
49	.65364	.75680	.66675	.74528	.67965	.73353	.69235	.72156	.70484	.70937	11
50	.65386	.75661	.66697	.74509	.67987	.73333	.69256	.72136	.70505	.70916	10
51	.65408	.75642	.66718	.74489	.68008	.73314	.69277	.72116	.70525	.70896	9
52	.65430	.75623	.66740	.74470	.68029	.73294	.69298	.72095	.70546	.70875	8
53	.65452	.75604	.66762	.74451	.68051	.73274	.69319	.72075	.70567	.70855	7
54	.65474	.75585	.66783	.74431	.68072	.73254	.69340	.72055	.70587	.70834	6
55	.65496	.75566	.66805	.74412	.68093	.73234	.69361	.72035	.70608	.70813	5
56	.65518	.75547	.66827	.74392	.68115	.73215	.69382	.72015	.70628	.70793	4
57	.65540	.75528	.66848	.74373	.68136	.73195	.69403	.71995	.70649	.70772	3
58	.65562	.75509	.66870	.74353	.68157	.73175	.69424	.71974	.70670	.70752	2
59	.65584	.75490	.66891	.74334	.68179	.73155	.69445	.71954	.70690	.70731	1
60	.65606	.75471	.66913	.74314	.68200	.73135	.69466	.71934	.70711	.70711	0
′	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	Cosin	Sine	′
	49°		48°		47°		46°		45°		

TABLE II.

NATURAL TANGENTS AND COTANGENTS

TO

FIVE DECIMAL PLACES.

′	0°		1°		2°		3°		′
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.00000	Infinite.	.01746	57.2900	.03492	28.6363	.05241	19.0811	60
1	.00029	3437.75	.01775	56.3506	.03521	28.3994	.05270	18.9755	59
2	.00058	1718.87	.01804	55.4415	.03550	28.1664	.05299	18.8711	58
3	.00087	1145.92	.01833	54.5613	.03579	27.9372	.05328	18.7678	57
4	.00116	859.436	.01862	53.7086	.03609	27.7117	.05357	18.6656	56
5	.00145	687.549	.01891	52.8821	.03638	27.4899	.05387	18.5645	55
6	.00175	572.957	.01920	52.0807	.03667	27.2715	.05416	18.4645	54
7	.00204	491.106	.01949	51.3032	.03696	27.0566	.05445	18.3655	53
8	.00233	429.718	.01978	50.5485	.03725	26.8450	.05474	18.2677	52
9	.00262	381.971	.02007	49.8157	.03754	26.6367	.05503	18.1708	51
10	.00291	343.774	.02036	49.1039	.03783	26.4316	.05533	18.0750	50
11	.00320	312.521	.02066	48.4121	.03812	26.2296	.05562	17.9802	49
12	.00349	286.478	.02095	47.7395	.03842	26.0307	.05591	17.8863	48
13	.00378	264.441	.02124	47.0853	.03871	25.8348	.05620	17.7934	47
14	.00407	245.552	.02153	46.4489	.03900	25.6418	.05649	17.7015	46
15	.00436	229.182	.02182	45.8294	.03929	25.4517	.05678	17.6106	45
16	.00465	214.858	.02211	45.2261	.03958	25.2644	.05708	17.5205	44
17	.00495	202.219	.02240	44.6386	.03987	25.0798	.05737	17.4314	43
18	.00524	190.984	.02269	44.0661	.04016	24.8978	.05766	17.3432	42
19	.00553	180.932	.02298	43.5081	.04046	24.7185	.05795	17.2558	41
20	.00582	171.885	.02328	42.9641	.04075	24.5418	.05824	17.1693	40
21	.00611	163.700	.02357	42.4335	.04104	24.3675	.05854	17.0837	39
22	.00640	156.259	.02386	41.9158	.04133	24.1957	.05883	16.9990	38
23	.00669	149.465	.02415	41.4106	.04162	24.0263	.05912	16.9150	37
24	.00698	143.237	.02444	40.9174	.04191	23.8593	.05941	16.8319	36
25	.00727	137.507	.02473	40.4358	.04220	23.6945	.05970	16.7496	35
26	.00756	132.219	.02502	39.9655	.04250	23.5321	.05999	16.6681	34
27	.00785	127.321	.02531	39.5059	.04279	23.3718	.06029	16.5874	33
28	.00815	122.774	.02560	39.0568	.04308	23.2137	.06058	16.5075	32
29	.00844	118.540	.02589	38.6177	.04337	23.0577	.06087	16.4283	31
30	.00873	114.589	.02619	38.1885	.04366	22.9038	.06116	16.3499	30
31	.00902	110.892	.02648	37.7686	.04395	22.7519	.06145	16.2722	29
32	.00931	107.426	.02677	37.3579	.04424	22.6020	.06175	16.1952	28
33	.00960	104.171	.02706	36.9560	.04454	22.4541	.06204	16.1190	27
34	.00989	101.107	.02735	36.5627	.04483	22.3081	.06233	16.0435	26
35	.01018	98.2179	.02764	36.1776	.04512	22.1640	.06262	15.9687	25
36	.01047	95.4895	.02793	35.8006	.04541	22.0217	.06291	15.8945	24
37	.01076	92.9085	.02822	35.4313	.04570	21.8813	.06321	15.8211	23
38	.01105	90.4633	.02851	35.0695	.04599	21.7426	.06350	15.7483	22
39	.01135	88.1436	.02881	34.7151	.04628	21.6056	.06379	15.6762	21
40	.01164	85.9398	.02910	34.3678	.04658	21.4704	.06408	15.6048	20
41	.01193	83.8435	.02939	34.0273	.04687	21.3369	.06437	15.5340	19
42	.01222	81.8470	.02968	33.6935	.04716	21.2049	.06467	15.4638	18
43	.01251	79.9434	.02997	33.3662	.04745	21.0747	.06496	15.3943	17
44	.01280	78.1263	.03026	33.0452	.04774	20.9460	.06525	15.3254	16
45	.01309	76.3900	.03055	32.7303	.04803	20.8188	.06554	15.2571	15
46	.01338	74.7292	.03084	32.4213	.04833	20.6932	.06584	15.1893	14
47	.01367	73.1390	.03114	32.1181	.04862	20.5691	.06613	15.1222	13
48	.01396	71.6151	.03143	31.8205	.04891	20.4465	.06642	15.0557	12
49	.01425	70.1533	.03172	31.5284	.04920	20.3253	.06671	14.9898	11
50	.01455	68.7501	.03201	31.2416	.04949	20.2056	.06700	14.9244	10
51	.01484	67.4019	.03230	30.9599	.04978	20.0872	.06730	14.8596	9
52	.01513	66.1055	.03259	30.6833	.05007	19.9702	.06759	14.7954	8
53	.01542	64.8580	.03288	30.4116	.05037	19.8546	.06788	14.7317	7
54	.01571	63.6567	.03317	30.1446	.05066	19.7403	.06817	14.6685	6
55	.01600	62.4992	.03346	29.8823	.05095	19.6273	.06847	14.6059	5
56	.01629	61.3829	.03376	29.6245	.05124	19.5156	.06876	14.5438	4
57	.01658	60.3058	.03405	29.3711	.05153	19.4051	.06905	14.4823	3
58	.01687	59.2659	.03434	29.1220	.05182	19.2959	.06934	14.4212	2
59	.01716	58.2612	.03463	28.8771	.05212	19.1879	.06963	14.3607	1
60	.01746	57.2900	.03492	28.6363	.05241	19.0811	.06993	14.3007	0
′	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	′
	89°		88°		87°		86°		

′	4° Tang	4° Cotang	5° Tang	5° Cotang	6° Tang	6° Cotang	7° Tang	7° Cotang	′
0	.06993	14.3007	.08749	11.4301	.10510	9.51436	.12278	8.14435	60
1	.07022	14.2411	.08778	11.3919	.10540	9.48781	.12308	8.12481	59
2	.07051	14.1821	.08807	11.3540	.10569	9.46141	.12338	8.10536	58
3	.07080	14.1235	.08837	11.3163	.10599	9.43515	.12367	8.08600	57
4	.07110	14.0655	.08866	11.2789	.10628	9.40904	.12397	8.06674	56
5	.07139	14.0079	.08895	11.2417	.10657	9.38307	.12426	8.04756	55
6	.07168	13.9507	.08925	11.2048	.10687	9.35724	.12456	8.02848	54
7	.07197	13.8940	.08954	11.1681	.10716	9.33155	.12485	8.00948	53
8	.07227	13.8378	.08983	11.1316	.10746	9.30599	.12515	7.99058	52
9	.07256	13.7821	.09013	11.0954	.10775	9.28058	.12544	7.97176	51
10	.07285	13.7267	.09042	11.0594	.10805	9.25530	.12574	7.95302	50
11	.07314	13.6719	.09071	11.0237	.10834	9.23016	.12603	7.93438	49
12	.07344	13.6174	.09101	10.9882	.10863	9.20516	.12633	7.91582	48
13	.07373	13.5634	.09130	10.9529	.10893	9.18028	.12662	7.89734	47
14	.07402	13.5098	.09159	10.9178	.10922	9.15554	.12692	7.87895	46
15	.07431	13.4566	.09189	10.8829	.10952	9.13093	.12722	7.86064	45
16	.07461	13.4039	.09218	10.8483	.10981	9.10646	.12751	7.84242	44
17	.07490	13.3515	.09247	10.8139	.11011	9.08211	.12781	7.82428	43
18	.07519	13.2996	.09277	10.7797	.11040	9.05789	.12810	7.80622	42
19	.07548	13.2480	.09306	10.7457	.11070	9.03379	.12840	7.78825	41
20	.07578	13.1969	.09335	10.7119	.11099	9.00983	.12869	7.77035	40
21	.07607	13.1461	.09365	10.6783	.11128	8.98598	.12899	7.75254	39
22	.07636	13.0958	.09394	10.6450	.11158	8.96227	.12929	7.73480	38
23	.07665	13.0458	.09423	10.6118	.11187	8.93867	.12958	7.71715	37
24	.07695	12.9962	.09453	10.5789	.11217	8.91520	.12988	7.69957	36
25	.07724	12.9469	.09482	10.5462	.11246	8.89185	.13017	7.68208	35
26	.07753	12.8981	.09511	10.5136	.11276	8.86862	.13047	7.66466	34
27	.07782	12.8496	.09541	10.4813	.11305	8.84551	.13076	7.64732	33
28	.07812	12.8014	.09570	10.4491	.11335	8.82252	.13106	7.63005	32
29	.07841	12.7536	.09600	10.4172	.11364	8.79964	.13136	7.61287	31
30	.07870	12.7062	.09629	10.3854	.11394	8.77689	.13165	7.59575	30
31	.07899	12.6591	.09658	10.3538	.11423	8.75425	.13195	7.57872	29
32	.07929	12.6124	.09688	10.3224	.11452	8.73172	.13224	7.56176	28
33	.07958	12.5660	.09717	10.2913	.11482	8.70931	.13254	7.54487	27
34	.07987	12.5199	.09746	10.2602	.11511	8.68701	.13284	7.52806	26
35	.08017	12.4742	.09776	10.2294	.11541	8.66482	.13313	7.51132	25
36	.08046	12.4288	.09805	10.1988	.11570	8.64275	.13343	7.49465	24
37	.08075	12.3838	.09834	10.1683	.11600	8.62078	.13372	7.47806	23
38	.08104	12.3390	.09864	10.1381	.11629	8.59893	.13402	7.46154	22
39	.08134	12.2946	.09893	10.1080	.11659	8.57718	.13432	7.44509	21
40	.08163	12.2505	.09923	10.0780	.11688	8.55555	.13461	7.42871	20
41	.08192	12.2067	.09952	10.0483	.11718	8.53402	.13491	7.41240	19
42	.08221	12.1632	.09981	10.0187	.11747	8.51259	.13521	7.39616	18
43	.08251	12.1201	.10011	9.98931	.11777	8.49128	.13550	7.37999	17
44	.08280	12.0772	.10040	9.96007	.11806	8.47007	.13580	7.36389	16
45	.08309	12.0346	.10069	9.93101	.11836	8.44896	.13609	7.34786	15
46	.08339	11.9923	.10099	9.90211	.11865	8.42795	.13639	7.33190	14
47	.08368	11.9504	.10128	9.87338	.11895	8.40705	.13669	7.31600	13
48	.08397	11.9087	.10158	9.84482	.11924	8.38625	.13698	7.30018	12
49	.08427	11.8673	.10187	9.81641	.11954	8.36555	.13728	7.28442	11
50	.08456	11.8262	.10216	9.78817	.11983	8.34496	.13758	7.26873	10
51	.08485	11.7853	.10246	8.76009	.12013	8.32446	.13787	7.25310	9
52	.08514	11.7448	.10275	9.73217	.12042	8.30406	.13817	7.23754	8
53	.08544	11.7045	.10305	9.70441	.12072	8.28376	.13846	7.22204	7
54	.08573	11.6645	.10334	9.67680	.12101	8.26355	.13876	7.20661	6
55	.08602	11.6248	.10363	9.64935	.12131	8.24345	.13906	7.19125	5
56	.08632	11.5853	.10393	9.62205	.12160	8.22344	.13935	7.17594	4
57	.08661	11.5461	.10422	9.59490	.12190	8.20352	.13965	7.16071	3
58	.08690	11 5072	.10452	9.56791	.12219	8.18370	.13995	7.14553	2
59	.08720	11.4685	.10481	9.54106	.12249	8.16398	.14024	7.13042	1
60	.08749	11.4301	.10510	9.51436	.12278	8.14435	.14054	7.11537	0
′	85° Cotang	85° Tang	84° Cotang	84° Tang	83° Cotang	83° Tang	82° Cotang	82° Tang	′

′	8° Tang	8° Cotang	9° Tang	9° Cotang	10° Tang	10° Cotang	11° Tang	11° Cotang	′
0	.14054	7.11537	.15838	6.31375	.17633	5.67128	.19438	5.14455	60
1	.14084	7.10038	.15868	6.30189	.17663	5.66165	.19468	5.13658	59
2	.14113	7.08546	.15898	6.29007	.17693	5.65205	.19498	5.12862	58
3	.14143	7.07059	.15928	6.27829	.17723	5.64248	.19529	5.12069	57
4	.14173	7.05579	.15958	6.26655	.17753	5.63295	.19559	5.11279	56
5	.14202	7.04105	.15988	6.25486	.17783	5.62344	.19589	5.10490	55
6	.14232	7.02637	.16017	6.24321	.17813	5.61397	.19619	5.09704	54
7	.14262	6.91174	.16047	6.23160	.17843	5.60452	.19649	5.08921	53
8	.14291	6.99718	.16077	6.22003	.17873	5.59511	.19680	5.08139	52
9	.14321	6.98268	.16107	6.20851	.17903	5.58573	.19710	5.07360	51
10	.14351	6.96823	.16137	6.19703	.17933	5.57638	.19740	5.06584	50
11	.14381	6.95385	.16167	6.18559	.17963	5.56706	.19770	5.05809	49
12	.14410	6.93952	.16196	6.17419	.17993	5.55777	.19801	5.05037	48
13	.14440	6.92525	.16226	6.16283	.18023	5.54851	.19831	5.04267	47
14	.14470	6.91104	.16256	6.15151	.18053	5.53927	.19861	5.03499	46
15	.14499	6.89688	.16286	6.14023	.18083	5.53007	.19891	5.02734	45
16	.14529	6.88278	.16316	6.12899	.18113	5.52090	.19921	5.01971	44
17	.14559	6.86874	.16346	6.11779	.18143	5.51176	.19952	5.01210	43
18	.14588	6.85475	.16376	6.10664	.18173	5.50264	.19982	5.00451	42
19	.14618	6.84082	.16405	6.09552	.18203	5.49356	.20012	4.99695	41
20	.14648	6.82694	.16435	6.08444	.18233	5.48451	.20042	4.98940	40
21	.14678	6.81312	.16465	6.07340	.18263	5.47548	.20073	4.98188	39
22	.14707	6.79936	.16495	6.06240	.18293	5.46648	.20103	4.97438	38
23	.14737	6.78564	.16525	6.05143	.18323	5.45751	.20133	4.96690	37
24	.14767	6.77199	.16555	6.04051	.18353	5.44857	.20164	4.95945	36
25	.14796	6.75838	.16585	6.02962	.18384	5.43966	.20194	4.95201	35
26	.14826	6.74483	.16615	6.01878	.18414	5.43077	.20224	4.94460	34
27	.14856	6.73133	.16645	6.00797	.18444	5.42192	.20254	4.93721	33
28	.14886	6.71789	.16674	5.99720	.18474	5.41309	.20285	4.92984	32
29	.14915	6.70450	.16704	5.98646	.18504	5.40429	.20315	4.92249	31
30	.14945	6.69116	.16734	5.97576	.18534	5.39552	.20345	4.91516	30
31	.14975	6.67787	.16764	5.96510	.18564	5.38677	.20376	4.90785	29
32	.15005	6.66463	.16794	5.95448	.18594	5.37805	.20406	4.90056	28
33	.15034	6.65144	.16824	5.94390	.18624	5.36936	.20436	4.89330	27
34	.15064	6.63831	.16854	5.93335	.18654	5.36070	.20466	4.88605	26
35	.15094	6.62523	.16884	5.92283	.18684	5.35206	.20497	4.87882	25
36	.15124	6.61219	.16914	5.91236	.18714	5.34345	.20527	4.87162	24
37	.15153	6.59921	.16944	5.90191	.18745	5.33487	.20557	4.86444	23
38	.15183	6.58627	.16974	5.89151	.18775	5.32631	.20588	4.85727	22
39	.15213	6.57339	.17004	5.88114	.18805	5.31778	.20618	4.85013	21
40	.15243	6.56055	.17033	5.87080	.18835	5.30928	.20648	4.84300	20
41	.15272	6.54777	.17063	5.86051	.18865	5.30080	.20679	4.83590	19
42	.15302	6.53503	.17093	5.85024	.18895	5.29235	.20709	4.82882	18
43	.15332	6.52234	.17123	5.84001	.18925	5.28393	.20739	4.82175	17
44	.15362	6.50970	.17153	5.82982	.18955	5.27553	.20770	4.81471	16
45	.15391	6.49710	.17183	5.81966	.18986	5.26715	.20800	4.80769	15
46	.15421	6.48456	.17213	5.80953	.19016	5.25880	.20830	4.80068	14
47	.15451	6.47206	.17243	5.79944	.19046	5.25048	.20861	4.79370	13
48	.15481	6.45961	.17273	5.78938	.19076	5.24218	.20891	4.78673	12
49	.15511	6.44720	.17303	5.77936	.19106	5.23391	.20921	4.77978	11
50	.15540	6.43484	.17333	5.76937	.19136	5.22566	.20952	4.77286	10
51	.15570	6.42253	.17363	5.75941	.19166	5.21744	.20982	4.76595	9
52	.15600	6.41026	.17393	5.74949	.19197	5.20925	.21013	4.75906	8
53	.15630	6.39804	.17423	5.73960	.19227	5.20107	.21043	4.75219	7
54	.15660	6.38587	.17453	5.72974	.19257	5.19293	.21073	4.74534	6
55	.15689	6.37374	.17483	5.71992	.19287	5.18480	.21104	4.73851	5
56	.15719	6.36165	.17513	5.71013	.19317	5.17671	.21134	4.73170	4
57	.15749	6.34961	.17543	5.70037	.19347	5.16863	.21164	4.72490	3
58	.15779	6.33761	.17573	5.69064	.19378	5.16058	.21195	4.71813	2
59	.15809	6.32566	.17603	5.68094	.19408	5.15256	.21225	4.71137	1
60	.15838	6.31375	.17633	5.67128	.19438	5.14455	.21256	4.70463	0
′	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	′
	81°		80°		79°		78°		

′	12° Tang	12° Cotang	13° Tang	13° Cotang	14° Tang	14° Cotang	15° Tang	15° Cotang	′
0	.21256	4.70463	.23087	4.33148	.24933	4.01078	.26795	3.73205	60
1	.21286	4.69791	.23117	4.32573	.24964	4.00582	.26826	3.72771	59
2	.21316	4.69121	.23148	4.32001	.24995	4.00086	.26857	3.72338	58
3	.21347	4.68452	.23179	4.31430	.25026	3.99592	.26888	3.71907	57
4	.21377	4.67786	.23209	4.30860	.25056	3.99099	.26920	3.71476	56
5	.21408	4.67121	.23240	4.30291	.25087	3.98607	.26951	3.71046	55
6	.21438	4.66458	.23271	4.29724	.25118	3.98117	.26982	3.70616	54
7	.21469	4.65797	.23301	4.29159	.25149	3.97627	.27013	3.70188	53
8	.21499	4.65138	.23332	4.28595	.25180	3.97139	.27044	3.69761	52
9	.21529	4.64480	.23363	4.28032	.25211	3.96651	.27076	3.69335	51
10	.21560	4.63825	.23393	4.27471	.25242	3.96165	.27107	3.68909	50
11	.21590	4.63171	.23424	4.26911	.25273	3.95680	.27138	3.68485	49
12	.21621	4.62518	.23455	4.26352	.25304	3.95196	.27169	3.68061	48
13	.21651	4.61868	.23485	4.25795	.25335	3.94713	.27201	3.67638	47
14	.21682	4.61219	.23516	4.25239	.25366	3.94232	.27232	3.67217	46
15	.21712	4.60572	.23547	4.24685	.25397	3.93751	.27263	3.66796	45
16	.21743	4.59927	.23578	4.24132	.25428	3.93271	.27294	3.66376	44
17	.21773	4.59283	.23608	4.23580	.25459	3.92793	.27326	3.65957	43
18	.21804	4.58641	.23639	4.23030	.25490	3.92316	.27357	3.65538	42
19	.21834	4.58001	.23670	4.22481	.25521	3.91839	.27388	3.65121	41
20	.21864	4.57363	.23700	4.21933	.25552	3.91364	.27419	3.64705	40
21	.21895	4.56726	.23731	4.21387	.25583	3.90890	.27451	3.64289	39
22	.21925	4.56091	.23762	4.20842	.25614	3.90417	.27482	3.63874	38
23	.21956	4.55458	.23793	4.20298	.25645	3.89945	.27513	3.63461	37
24	.21986	4.54826	.23823	4.19756	.25676	3.89474	.27545	3.63048	36
25	.22017	4.54196	.23854	4.19215	.25707	3.89004	.27576	3.62636	35
26	.22047	4.53568	.23885	4.18675	.25738	3.88536	.27607	3.62224	34
27	.22078	4.52941	.23916	4.18137	.25769	3.88068	.27638	3.61814	33
28	.22108	4.52316	.23946	4.17600	.25800	3.87601	.27670	3.61405	32
29	.22139	4.51693	.23977	4.17064	.25831	3.87136	.27701	3.60996	31
30	.22169	4.51071	.24008	4.16530	.25862	3.86671	.27732	3.60588	30
31	.22200	4.50451	.24039	4.15997	.25893	3.86208	.27764	3.60181	29
32	.22231	4.49832	.24069	4.15465	.25924	3.85745	.27795	3.59775	28
33	.22261	4.49215	.24100	4.14934	.25955	3.85284	.27826	3.59370	27
34	.22292	4.48600	.24131	4.14405	.25986	3.84824	.27858	3.58966	26
35	.22322	4.47986	.24162	4.13877	.26017	3.84364	.27889	3.58562	25
36	.22353	4.47374	.24193	4.13350	.26048	3.83906	.27921	3.58160	24
37	.22383	4.46764	.24223	4.12825	.26079	3.83449	.27952	3.57758	23
38	.22414	4.46155	.24254	4.12301	.26110	3.82992	.27983	3.57357	22
39	.22444	4.45548	.24285	4.11778	.26141	3.82537	.28015	3.56957	21
40	.22475	4.44942	.24316	4.11256	.26172	3.82083	.28046	3.56557	20
41	.22505	4.44338	.24347	4.10736	.26203	3.81630	.28077	3.56159	19
42	.22536	4.43735	.24377	4.10216	.26235	3.81177	.28109	3.55761	18
43	.22567	4.43134	.24408	4.09699	.26266	3.80726	.28140	3.55364	17
44	.22597	4.42534	.24439	4.09182	.26297	3.80276	.28172	3.54968	16
45	.22628	4.41936	.24470	4.08666	.26328	3.79827	.28203	3.54573	15
46	.22658	4.41340	.24501	4.08152	.26359	3.79378	.28234	3.54179	14
47	.22689	4.40745	.24532	4.07639	.26390	3.78931	.28266	3.53785	13
48	.22719	4.40152	.24562	4.07127	.26421	3.78485	.28297	3.53393	12
49	.22750	4.39560	.24593	4.06616	.26452	3.78040	.28329	3.53001	11
50	.22781	4.38969	.24624	4.06107	.26483	3.77595	.28360	3.52609	10
51	.22811	4.38381	.24655	4.05599	.26515	3.77152	.28391	3.52219	9
52	.22842	4.37793	.24686	4.05092	.26546	3.76709	.28423	3.51829	8
53	.22872	4.37207	.24717	4.04586	.26577	3.76268	.28454	3.51441	7
54	.22903	4.36623	.24747	4.04081	.26608	3.75828	.28486	3.51053	6
55	.22934	4.36040	.24778	4.03578	.26639	3.75388	.28517	3.50666	5
56	.22964	4.35459	.24809	4.03076	.26670	3.74950	.28549	3.50279	4
57	.22995	4.34879	.24840	4.02574	.26701	3.74512	.28580	3.49894	3
58	.23026	4.34300	.24871	4.02074	.26733	3.74075	.28612	3.49509	2
59	.23056	4.33723	.24902	4.01576	.26764	3.73640	.28643	3.49125	1
60	.23087	4.33148	.24933	4.01078	.26795	3.73205	.28675	3.48741	0
′	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	′
	77°		76°		75°		74°		

′	16° Tang	16° Cotang	17° Tang	17° Cotang	18° Tang	18° Cotang	19° Tang	19° Cotang	′
0	.28675	3.48741	.30573	3.27085	.32492	3.07768	.34433	2.90421	60
1	.28706	3.48359	.30605	3.26745	.32524	3.07464	.34465	2.90147	59
2	.28738	3.47977	.30637	3.26406	.32556	3.07160	.34498	2.89873	58
3	.28769	3.47596	.30669	3.26067	.32588	3.06857	.34530	2.89600	57
4	.28800	3.47216	.30700	3.25729	.32621	3.06554	.34563	2.89327	56
5	.28832	3.46837	.30732	3.25392	.32653	3.06252	.34596	2.89055	55
6	.28864	3.46458	.30764	3.25055	.32685	3.05950	.34628	2.88783	54
7	.28895	3.46080	.30796	3.24719	.32717	3.05649	.34661	2.88511	53
8	.28927	3.45703	.30828	3.24383	.32749	3.05349	.34693	2.88240	52
9	.28958	3.45327	.30860	3.24049	.32782	3.05049	.34726	2.87970	51
10	.28990	3.44951	.30891	3.23714	.32814	3.04749	.34758	2.87700	50
11	.29021	3.44576	.30923	3.23381	.32846	3.04450	.34791	2.87430	49
12	.29053	3.44202	.30955	3.23048	.32878	3.04152	.34824	2.87161	48
13	.29084	3.43829	.30987	3.22715	.32911	3.03854	.34856	2.86892	47
14	.29116	3.43456	.31019	3.22384	.32943	3.03556	.34889	2.86624	46
15	.29147	3.43084	.31051	3.22053	.32975	3.03260	.34922	2.86356	45
16	.29179	3.42713	.31083	3.21722	.33007	3.02963	.34954	2.86089	44
17	.29210	3.42343	.31115	3.21392	.33040	3.02667	.34987	2.85822	43
18	.29242	3.41973	.31147	3.21063	.33072	3.02372	.35020	2.85555	42
19	.29274	3.41604	.31178	3.20734	.33104	3.02077	.35052	2.85289	41
20	.29305	3.41236	.31210	3.20406	.33136	3.01783	.35085	2.85023	40
21	.29337	3.40869	.31242	3.20079	.33169	3.01489	.35118	2.84758	39
22	.29368	3.40502	.31274	3.19752	.33201	3.01196	.35150	2.84494	38
23	.29400	3.40136	.31306	3.19426	.33233	3.00903	.35183	2.84229	37
24	.29432	3.39771	.31338	3.19100	.33266	3.00611	.35216	2.83965	36
25	.29463	3.39406	.31370	3.18775	.33298	3.00319	.35248	2.83702	35
26	.29495	3.39042	.31402	3.18451	.33330	3.00028	.35281	2.83439	34
27	.29526	3.38679	.31434	3.18127	.33363	2.99738	.35314	2.83176	33
28	.29558	3.38317	.31466	3.17804	.33395	2.99447	.35346	2.82914	32
29	.29590	3.37955	.31498	3.17481	.33427	2.99158	.35379	2.82653	31
30	.29621	3.37594	.31530	3.17159	.33460	2.98868	.35412	2.82391	30
31	.29653	3.37234	.31562	3.16838	.33492	2.98580	.35445	2.82130	29
32	.29685	3.36875	.31594	3.16517	.33524	2.98292	.35477	2.81870	28
33	.29716	3.36516	.31626	3.16197	.33557	2.98004	.35510	2.81610	27
34	.29748	3.36158	.31658	3.15877	.33589	2.97717	.35543	2.81350	26
35	.29780	3.35800	.31690	3.15558	.33621	2.97430	.35576	2.81091	25
36	.29811	3.35443	.31722	3.15240	.33654	2.97144	.35608	2.80833	24
37	.29843	3.35087	.31754	3.14922	.33686	2.96858	.35641	2.80574	23
38	.29875	3.34732	.31786	3.14605	.33718	2.96573	.35674	2.80316	22
39	.29906	3.34377	.31818	3.14288	.33751	2.96288	.35707	2.80059	21
40	.29938	3.34023	.31850	3.13972	.33783	2.96004	.35740	2.79802	20
41	.29970	3.33670	.31882	3.13656	.33816	2.95721	.35772	2.79545	19
42	.30001	3.33317	.31914	3.13341	.33848	2.95437	.35805	2.79289	18
43	.30033	3.32965	.31946	3.13027	.33881	2.95155	.35838	2.79033	17
44	.30065	3.32614	.31978	3.12713	.33913	2.94872	.35871	2.78778	16
45	.30097	3.32264	.32010	3.12400	.33945	2.94591	.35904	2.78523	15
46	.30128	3.31914	.32042	3.12087	.33978	2.94309	.35937	2.78269	14
47	.30160	3.31565	.32074	3.11775	.34010	2.94028	.35969	2.78014	13
48	.30192	3.31216	.32106	3.11464	.34043	2.93748	.36002	2.77761	12
49	.30224	3.30868	.32139	3.11153	.34075	2.93468	.36035	2.77507	11
50	.30255	3.30521	.32171	3.10842	.34108	2.93189	.36068	2.77254	10
51	.30287	3.30174	.32203	3.10532	.34140	2.92910	.36101	2.77002	9
52	.30319	3.29829	.32235	3.10223	.34173	2.92632	.36134	2.76750	8
53	.30351	3.29483	.32267	3.09914	.34205	2.92354	.36167	2.76498	7
54	.30382	3.29139	.32299	3.09606	.34238	2.92076	.36199	2.76247	6
55	.30414	3.28795	.32331	3.09298	.34270	2.91799	.36232	2.75996	5
56	.30446	3.28452	.32363	3.08991	.34303	2.91523	.36265	2.75746	4
57	.30478	3.28109	.32396	3.08685	.34335	2.91246	.36298	2.75496	3
58	.30509	3.27767	.32428	3.08379	.34368	2.90971	.36331	2.75246	2
59	.30541	3.27426	.32460	3.08073	.34400	2.90696	.36364	2.74997	1
60	.30573	3.27085	.32492	3.07768	.34433	2.90421	.36397	2.74748	0
′	73° Cotang	73° Tang	72° Cotang	72° Tang	71° Cotang	71° Tang	70° Cotang	70° Tang	′

′	20° Tang	20° Cotang	21° Tang	21° Cotang	22° Tang	22° Cotang	23° Tang	23° Cotang	
0	.36397	2.74748	.38386	2.60509	.40403	2.47509	.42447	2.35585	60
1	.36430	2.74499	.38420	2.60283	.40436	2.47302	.42482	2.35395	59
2	.36463	2.74251	.38453	2.60057	.40470	2.47095	.42516	2.35205	58
3	.36496	2.74004	.38487	2.59831	.40504	2.46888	.42551	2.35015	57
4	.36529	2.73756	.38520	2.59606	.40538	2.46682	.42585	2.34825	56
5	.36562	2.73509	.38553	2.59381	.40572	2.46476	.42619	2.34636	55
6	.36595	2.73263	.38587	2.59156	.40606	2.46270	.42654	2.34447	54
7	.36628	2.73017	.38620	2.58932	.40640	2.46065	.42688	2.34258	53
8	.36661	2.72771	.38654	2.58708	.40674	2.45860	.42722	2.34069	52
9	.36694	2.72526	.38687	2.58484	.40707	2.45655	.42757	2.33881	51
10	.36727	2.72281	.38721	2.58261	.40741	2.45451	.42791	2.33693	50
11	.36760	2.72036	.38754	2.58038	.40775	2.45246	.42826	2.33505	49
12	.36793	2.71792	.38787	2.57815	.40809	2.45043	.42860	2.33317	48
13	.36826	2.71548	.38821	2.57593	.40843	2.44839	.42894	2.33130	47
14	.36859	2.71305	.38854	2.57371	.40877	2.44636	.42929	2.32943	46
15	.36892	2.71062	.38888	2.57150	.40911	2.44433	.42963	2.32756	45
16	.36925	2.70819	.38921	2.56928	.40945	2.44230	.42998	2.32570	44
17	.36958	2.70577	.38955	2.56707	.40979	2.44027	.43032	2.32383	43
18	.36991	2.70335	.38988	2.56487	.41013	2.43825	.43067	2.32197	42
19	.37024	2.70094	.39022	2.56266	.41047	2.43623	.43101	2.32012	41
20	.37057	2.69853	.39055	2.56046	.41081	2.43422	.43136	2.31826	40
21	.37090	2.69612	.39089	2.55827	.41115	2.43220	.43170	2.31641	39
22	.37123	2.69371	.39122	2.55608	.41149	2.43019	.43205	2.31456	38
23	.37157	2.69131	.39156	2.55389	.41183	2.42819	.43239	2.31271	37
24	.37190	2.68892	.39190	2.55170	.41217	2.42618	.43274	2.31086	36
25	.37223	2.68653	.39223	2.54952	.41251	2.42418	.43308	2.30902	35
26	.37256	2.68414	.39257	2.54734	.41285	2.42218	.43343	2.30718	34
27	.37289	2.68175	.39290	2.54516	.41319	2.42019	.43378	2.30534	33
28	.37322	2 67937	.39324	2.54299	.41353	2.41819	.43412	2.30351	32
29	.37355	2.67700	.39357	2.54082	.41387	2.41620	.43447	2.30167	31
30	.37388	2.67462	.39291	2.53865	.41421	2.41421	.43481	2.29984	30
31	.37422	2.67225	.39425	2.53648	.41455	2.41223	.43516	2.29801	29
32	.37455	2.66989	.39458	2.53432	.41490	2.41025	.43550	2.29619	28
33	.37488	2.66752	.39492	2.53217	.41524	2.40827	.43585	2.29437	27
34	.37521	2.66516	.39526	2.53001	.41558	2.40629	.43620	2.29254	26
35	.37554	2.66281	.39559	2.52786	.41592	2.40432	.43654	2.29073	25
36	.37588	2.66046	.39593	2.52571	.41626	2.40235	.43689	2.28891	24
37	.37621	2.65811	.39626	2.52357	.41660	2.40038	.43724	2.28710	23
38	.37654	2.65576	.39660	2.52142	.41694	2.39841	.43758	2.28528	22
39	.37687	2.65342	.39694	2.51929	.41728	2.39645	.43793	2.28348	21
40	.37720	2.65109	.39727	2.51715	.41763	2.39449	.43828	2.28167	20
41	.37754	2.64875	.39761	2.51502	.41797	2.39253	.43862	2.27987	19
42	.37787	2.64642	.39795	2.51289	.41831	2.39058	.43897	2.27806	18
43	.37820	2.64410	.39829	2.51076	.41865	2.38863	.43932	2.27626	17
44	.37853	2.64177	.39862	2.50864	41899	2.38668	.43966	2.27447	16
45	.37887	2.63945	.39896	2.50652	.41933	2.38473	.44001	2.27267	15
46	.37920	2.63714	.39930	2.50440	.41968	2.38279	.44036	2.27088	14
47	.37953	2.63483	.39963	2.50229	.42002	2.38084	.44071	2.26909	13
48	.37986	2.63252	.39997	2.50018	.42036	2.37891	.44105	2.26730	12
49	.38020	2.63021	.40031	2.49807	.42070	2.37697	.44140	2.26552	11
50	.38053	2.62791	.40065	2.49597	.42105	2.37504	.44175	2.26374	10
51	.38086	2.62561	.40098	2.49386	.42139	2.37311	.44210	2.26196	9
52	.38120	2.62332	.40132	2.49177	.42173	2.37118	.44244	2.26018	8
53	.38153	2.62103	.40166	2.48967	.42207	2.36925	.44279	2.25840	7
54	.38186	2.61874	.40200	2.48758	.42242	2.36733	.44314	2.25663	6
55	.38220	2.61646	.40234	2.48549	.42276	2.36541	.44349	2.25486	5
56	.38253	2.61418	.40267	2 48340	.42310	2.36349	.44384	2.25309	4
57	.38286	2.61190	.40301	2.48132	.42345	2.36158	.44418	2.25132	3
58	.38320	2.60963	.40335	2.47924	.42379	2.35967	.44453	2.24956	2
59	.38353	2.60736	.40369	2.47716	.42413	2.35776	.44488	2.24780	1
60	.38386	2.60509	.40403	2.47509	.42447	2.35585	.44523	2.24604	0
′	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	′
	69°		68°		67°		66°		

′	24°		25°		26°		27°		′
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.44523	2.24604	.46631	2.14451	.48773	2.05030	.50953	1.96261	60
1	.44558	2.24428	.46666	2.14288	.48809	2.04879	.50989	1.96120	59
2	.44593	2.24252	.46702	2.14125	.48845	2.04728	.51026	1.95979	58
3	.44627	2.24077	.46737	2.13963	.48881	2.04577	.51063	1.95838	57
4	.44662	2.23902	.46772	2.13801	.48917	2.04426	.51099	1.95698	56
5	.44697	2.23727	.46808	2.13639	.48953	2.04276	.51136	1.95557	55
6	.44732	2.23553	.46843	2.13477	.48989	2.04125	.51173	1.95417	54
7	.44767	2.23378	.46879	2.13316	.49026	2.03975	.51209	1.95277	53
8	.44802	2.23204	.46914	2.13154	.49062	2.03825	.51246	1.95137	52
9	.44837	2.23030	.46950	2.12993	.49098	2.03675	.51283	1.94997	51
10	.44872	2.22857	.46985	2.12832	.49134	2.03526	.51319	1.94858	50
11	.44907	2.22683	.47021	2.12671	.49170	2.03376	.51356	1.94718	49
12	.44942	2.22510	.47056	2.12511	.49206	2.03227	.51393	1.94579	48
13	.44977	2.22337	.47092	2.12350	.49242	2.03078	.51430	1.94440	47
14	.45012	2.22164	.47128	2.12190	.49278	2.02929	.51467	1.94301	46
15	.45047	2.21992	.47163	2.12030	.49315	2.02780	.51503	1.94162	45
16	.45082	2.21819	.47199	2.11871	.49351	2.02631	.51540	1.94023	44
17	.45117	2.21647	.47234	2.11711	.49387	2.02483	.51577	1.93885	43
18	.45152	2.21475	.47270	2.11552	.49423	2.02335	.51614	1.93746	42
19	.45187	2.21304	.47305	2.11392	.49459	2.02187	.51651	1.93608	41
20	.45222	2.21132	.47341	2.11233	.49495	2.02039	.51688	1.93470	40
21	.45257	2.20961	.47377	2.11075	.49532	2.01891	.51724	1.93332	39
22	.45292	2.20790	.47412	2.10916	.49568	2.01743	.51761	1.93195	38
23	.45327	2.20619	.47448	2.10758	.49604	2.01596	.51798	1.93057	37
24	.45362	2.20449	.47483	2.10600	.49640	2.01449	.51835	1.92920	36
25	.45397	2.20278	.47519	2.10442	.49677	2.01302	.51872	1.92782	35
26	.45432	2.20108	.47555	2.10284	.49713	2.01155	.51909	1.92645	34
27	.45467	2.19938	.47590	2.10126	.49749	2.01008	.51946	1.92508	33
28	.45502	2.19769	.47626	2.09969	.49786	2.00862	.51983	1.92371	32
29	.45538	2.19599	.47662	2.09811	.49822	2.00715	.52020	1.92235	31
30	.45573	2.19430	.47698	2.09654	.49858	2.00569	.52057	1.92098	30
31	.45608	2.19261	.47733	2.09498	.49894	2.00423	.52094	1.91962	29
32	.45643	2.19092	.47769	2.09341	.49931	2.00277	.52131	1.91826	28
33	.45678	2.18923	.47805	2.09184	.49967	2.00131	.52168	1.91690	27
34	.45713	2.18755	.47840	2.09028	.50004	1.99986	.52205	1.91554	26
35	.45748	2.18587	.47876	2.08872	.50040	1.99841	.52242	1.91418	25
36	.45784	2.18419	.47912	2.08716	.50076	1.99695	.52279	1.91282	24
37	.45819	2.18251	.47948	2.08560	.50113	1.99550	.52316	1.91147	23
38	.45854	2.18084	.47984	2.08405	.50149	1.99406	.52353	1.91012	22
39	.45889	2.17916	.48019	2.08250	.50185	1.99261	.52390	1.90876	21
40	.45924	2.17749	.48055	2.08094	.50222	1.99116	.52427	1.90741	20
41	.45960	2.17582	.48091	2.07939	.50258	1.98972	.52464	1.90607	19
42	.45995	2.17416	.48127	2.07785	.50295	1.98828	.52501	1.90472	18
43	.46030	2.17249	.48163	2.07630	.50331	1.98684	.52538	1.90337	17
44	.46065	2.17083	.48198	2.07476	.50368	1.98540	.52575	1.90203	16
45	.46101	2.16917	.48234	2.07321	.50404	1.98396	.52613	1.90069	15
46	.46136	2.16751	.48270	2.07167	.50441	1.98253	.52650	1.89935	14
47	.46171	2.16585	.48306	2.07014	.50477	1.98110	.52687	1.89801	13
48	.46206	2.16420	.48342	2.06860	.50514	1.97966	.52724	1.89667	12
49	.46242	2.16255	.48378	2.06706	.50550	1.97823	.52761	1.89533	11
50	.46277	2.16090	.48414	2.06553	.50587	1.97681	.52798	1.89400	10
51	.46312	2.15925	.48450	2.06400	.50623	1.97538	.52836	1.89266	9
52	.46348	2.15760	.48486	2.06247	.50660	1.97395	.52873	1.89133	8
53	.46383	2.15596	.48521	2.06094	.50696	1.97253	.52910	1.89000	7
54	.46418	2.15432	.48557	2.05942	.50733	1.97111	.52947	1.88867	6
55	.46454	2.15268	.48593	2.05790	.50769	1.96969	.52985	1.88734	5
56	.46489	2.15104	.48629	2.05637	.50806	1.96827	.53022	1.88602	4
57	.46525	2.14940	.48665	2.05485	.50843	1.96685	.53059	1.88469	3
58	.46560	2.14777	.48701	2.05333	.50879	1.96544	.53096	1.88337	2
59	.46595	2.14614	.48737	2.05182	.50916	1.96402	.53134	1.88205	1
60	.46631	2.14451	.48773	2.05030	.50953	1.96261	.53171	1.88073	0
′	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	′
	65°		64°		63°		62°		

′	28°		29°		30°		31°	
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang
0	.53171	1.88073	.55431	1.80405	.57735	1.73205	.60086	1.66428
1	.53208	1.87941	.55469	1.80281	.57774	1.73089	.60126	1.66318
2	.53246	1.87809	.55507	1.80158	.57813	1.72973	.60165	1.66209
3	.53283	1.87677	.55545	1.80034	.57851	1.72857	.60205	1.66099
4	.53320	1.87546	.55583	1.79911	.57890	1.72741	.60245	1.65990
5	.53358	1.87415	.55621	1.79788	.57929	1.72625	.60284	1.65881
6	.53395	1.87283	.55659	1.79665	.57968	1.72509	.60324	1.65772
7	.53432	1.87152	.55697	1.79542	.58007	1.72393	.60364	1.65663
8	.53470	1.87021	.55736	1.79419	.58046	1.72278	.60403	1.65554
9	.53507	1.86891	.55774	1.79296	.58085	1.72163	.60443	1.65445
10	.53545	1.86760	.55812	1.79174	.58124	1.72047	.60483	1.65337
11	.53582	1.86630	.55850	1.79051	.58162	1.71932	.60522	1.65228
12	.53620	1.86499	.55888	1.78929	.58201	1.71817	.60562	1.65120
13	.53657	1.86369	.55926	1.78807	.58240	1.71702	.60602	1.65011
14	.53694	1.86239	.55964	1.78685	.58279	1.71588	.60642	1.64903
15	.53732	1.86109	.56003	1.78563	.58318	1.71473	.60681	1.64795
16	.53769	1.85979	.56041	1.78441	.58357	1.71358	.60721	1.64687
17	.53807	1.85850	.56079	1.78319	.58396	1.71244	.60761	1.64579
18	.53844	1.85720	.56117	1.78198	.58435	1.71129	.60801	1.64471
19	.53882	1.85591	.56156	1.78077	.58474	1.71015	.60841	1.64363
20	.53920	1.85462	.56194	1.77955	.58513	1.70901	.60881	1.64256
21	.53957	1.85333	.56232	1.77834	.58552	1.70787	.60921	1.64148
22	.53995	1.85204	.56270	1.77713	.58591	1.70673	.60960	1.64041
23	.54032	1.85075	.56309	1.77592	.58631	1.70560	.61000	1.63934
24	.54070	1.84946	.56347	1.77471	.58670	1.70446	.61040	1.63826
25	.54107	1.84818	.56385	1.77351	.58709	1.70332	.61080	1.63719
26	.54145	1.84689	.56424	1.77230	.58748	1.70219	.61120	1.63612
27	.54183	1.84561	.56462	1.77110	.58787	1.70106	.61160	1.63505
28	.54220	1.84433	.56501	1.76990	.58826	1.69992	.61200	1.63398
29	.54258	1.84305	.56539	1.76869	.58865	1.69879	.61240	1.63292
30	.54296	1.84177	.56577	1.76749	.58905	1.69766	.61280	1.63185
31	.54333	1.84049	.56616	1.76629	.58944	1.69653	.61320	1.63079
32	.54371	1.83922	.56654	1.76510	.58983	1.69541	.61360	1.62972
33	.54409	1.83794	.56693	1.76390	.59022	1.69428	.61400	1.62866
34	.54446	1.83667	.56731	1.76271	.59061	1.69316	.61440	1.62760
35	.54484	1.83540	.56769	1.76151	.59101	1.69203	.61480	1.62654
36	.54522	1.83413	.56808	1.76032	.59140	1.69091	.61520	1.62548
37	.54560	1.83286	.56846	1.75913	.59179	1.68979	.61561	1.62442
38	.54597	1.83159	.56885	1.75794	.59218	1.68866	.61601	1.62336
39	.54635	1.83033	.56923	1.75675	.59258	1.68754	.61641	1.62230
40	.54673	1.82906	.56962	1.75556	.59297	1.68643	.61681	1.62125
41	.54711	1.82780	.57000	1.75437	.59336	1.68531	.61721	1.62019
42	.54748	1.82654	.57039	1.75319	.59376	1.68419	.61761	1.61914
43	.54786	1.82528	.57078	1.75200	.59415	1.68308	.61801	1.61808
44	.54824	1.82402	.57116	1.75082	.59454	1.68196	.61842	1.61703
45	.54862	1.82276	.57155	1.74964	.59494	1.68085	.61882	1.61598
46	.54900	1.82150	.57193	1.74846	.59533	1.67974	.61922	1.61493
47	.54938	1.82025	.57232	1.74728	.59573	1.67863	.61962	1.61388
48	.54975	1.81899	.57271	1.74610	.59612	1.67752	.62003	1.61283
49	.55013	1.81774	.57309	1.74492	.59651	1.67641	.62043	1.61179
50	.55051	1.81649	.57348	1.74375	.59691	1.67530	.62083	1.61074
51	.55089	1.81524	.57386	1.74257	.59730	1.67419	.62124	1.60970
52	.55127	1.81399	.57425	1.74140	.59770	1.67309	.62164	1.60865
53	.55165	1.81274	.57464	1.74022	.59809	1.67198	.62204	1.60761
54	.55203	1.81150	.57503	1.73905	.59849	1.67088	.62245	1.60657
55	.55241	1.81025	.57541	1.73788	.59888	1.66978	.62285	1.60553
56	.55279	1.80901	.57580	1.73671	.59928	1.66867	.62325	1.60449
57	.55317	1.80777	.57619	1.73555	.59967	1.66757	.62366	1.60345
58	.55355	1.80653	.57657	1.73438	.60007	1.66647	.62406	1.60241
59	.55393	1.80529	.57696	1.73321	.60046	1.66538	.62446	1.60137
60	.55431	1.80405	.57735	1.73205	.60086	1.66428	.62487	1.60033
	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang
′	61°		60°		59°		58°	

′	32°		33°		34°		35°		′
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.62487	1.60033	.64941	1.53986	.67451	1.48256	.70021	1.42815	60
1	.62527	1.59930	.64982	1.53888	.67493	1.48163	.70064	1.42726	59
2	.62568	1.59826	.65024	1.53791	.67536	1.48070	.70107	1.42638	58
3	.62608	1.59723	.65065	1.53693	.67578	1.47977	.70151	1.42550	57
4	.62649	1.59620	.65106	1.53595	.67620	1.47885	.70194	1.42462	56
5	.62689	1.59517	.65148	1.53497	.67663	1.47792	.70238	1.42374	55
6	.62730	1.59414	.65189	1.53400	.67705	1.47699	.70281	1.42286	54
7	.62770	1.59311	.65231	1.53302	.67748	1.47607	.70325	1 42198	53
8	.62811	1.59208	.65272	1.53205	.67790	1.47514	.70368	1.42110	52
9	.62852	1.59105	.65314	1.53107	.67832	1.47422	.70412	1.42022	51
10	.62892	1.59002	.65355	1.53010	.67875	1.47330	.70455	1.41934	50
11	.62933	1.58900	.65397	1.52913	.67917	1.47238	.70499	1.41847	49
12	.62973	1.58797	.65438	1.52816	.67960	1.47146	.70542	1.41759	48
13	.63014	1.58695	.65480	1.52719	.68002	1.47053	.70586	1.41672	47
14	.63055	1.58593	.65521	1.52622	.68045	1.46962	.70629	1.41584	46
15	.63095	1.58490	.65563	1.52525	.68088	1.46870	.70673	1.41497	45
16	.63136	1.58388	.65604	1.52429	.68130	1.46778	.70717	1.41409	44
17	.63177	1.58286	.65646	1.52332	.68173	1.46686	.70760	1.41322	43
18	.63217	1.58184	.65688	1.52235	.68215	1.46595	.70804	1.41235	42
19	.63258	1.58083	.65729	1.52139	.68258	1.46503	.70848	1.41148	41
20	.63299	1.57981	.65771	1.52043	.68301	1.46411	.70891	1.41061	40
21	.63340	1.57879	.65813	1.51946	.68343	1.46320	.70935	1.40974	39
22	.63380	1.57778	.65854	1.51850	.68386	1.46229	.70979	1.40887	38
23	.63421	1.57676	.65896	1.51754	.68429	1.46137	.71023	1.40800	37
24	.63462	1.57575	.65938	1.51658	.68471	1.46046	.71066	1.40714	36
25	.63503	1.57474	.65980	1.51562	.68514	1.45955	.71110	1.40627	35
26	.63544	1.57372	.66021	1.51466	.68557	1.45864	.71154	1.40540	34
27	.63584	1.57271	.66063	1.51370	.68600	1.45773	.71198	1.40454	33
28	.63625	1.57170	.66105	1.51275	.68642	1.45682	.71242	1.40367	32
29	.63666	1.57069	.66147	1.51179	.68685	1.45592	.71285	1.40281	31
30	.63707	1.56969	.66189	1.51084	.68728	1.45501	.71329	1.40195	30
31	.63748	1.56868	.66230	1.50988	.68771	1.45410	.71373	1.40109	29
32	.63789	1.56767	.66272	1.50893	.68814	1.45320	.71417	1.40022	28
33	.63830	1.56667	.66314	1.50797	.68857	1.45229	.71461	1.39936	27
34	.63871	1.56566	.66356	1.50702	.68900	1.45139	.71505	1.39850	26
35	.63912	1.56466	.66398	1.50607	.68942	1.45049	.71549	1.39764	25
36	.63953	1.56366	.66440	1.50512	.68985	1.44958	.71593	1.39679	24
37	.63994	1.56265	.66482	1.50417	.69028	1.44868	.71637	1.39593	23
38	.64035	1.56165	.66524	1.50322	.69071	1.44778	.71681	1.39507	22
39	.64076	1.56065	.66566	1.50228	.69114	1.44688	.71725	1.39421	21
40	.64117	1.55966	.66608	1.50133	.69157	1.44598	.71769	1.39336	20
41	.64158	1.55866	.66650	1.50038	.69200	1.44508	.71813	1.39250	19
42	.64199	1.55766	.66692	1.49944	.69243	1.44418	.71857	1.39165	18
43	.64240	1.55666	.66734	1.49849	.69286	1.44329	.71901	1.39079	17
44	.64281	1.55567	.66776	1.49755	.69329	1.44239	.71946	1.38994	16
45	.64322	1.55467	.66818	1.49661	.69372	1.44149	.71990	1.38909	15
46	.64363	1.55368	.66860	1.49566	.69416	1.44060	.72034	1.38824	14
47	.64404	1.55269	.66902	1.49472	.69459	1.43970	.72078	1.38738	13
48	.64446	1.55170	.66944	1.49378	.69502	1.43881	.72122	1.38653	12
49	.64487	1.55071	.66986	1.49284	.69545	1.43792	.72167	1.38568	11
50	.64528	1.54972	.67028	1.49190	.69588	1.43703	.72211	1.38484	10
51	.64569	1.54873	.67071	1.49097	.69631	1.43614	.72255	1.38399	9
52	.64610	1.54774	.67113	1.49003	.69675	1.43525	.72299	1.38314	8
53	.64652	1.54675	.67155	1.48909	.69718	1.43436	.72344	1.38229	7
54	.64693	1.54576	.67197	1.48816	.69761	1.43347	.72388	1.38145	6
55	.64734	1.54478	.67239	1.48722	.69804	1.43258	.72432	1.38060	5
56	.64775	1.54379	.67282	1.48629	.69847	1.43169	.72477	1.37976	4
57	.64817	1.54281	.67324	1.48536	.69891	1.43080	.72521	1.37891	3
58	.64858	1.54183	.67366	1.48442	.69934	1.42992	.72565	1.37807	2
59	.64899	1.54085	.67409	1.48349	.69977	1.42903	.72610	1.37722	1
60	.64941	1.53986	.67451	1.48256	.70021	1.42815	.72654	1.37638	0
′	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	′
	57°		56°		55°		54°		

′	36° Tang	36° Cotang	37° Tang	37° Cotang	38° Tang	38° Cotang	39° Tang	39° Cotang	′
0	.72654	1.37638	.75355	1.32704	.78129	1.27994	.80978	1.23490	60
1	.72699	1.37554	.75401	1.32624	.78175	1.27917	.81027	1.23416	59
2	.72743	1.37470	.75447	1.32544	.78222	1.27841	.81075	1.23343	58
3	.72788	1.37386	.75492	1.32464	.78269	1.27764	.81123	1.23270	57
4	.72832	1.37302	.75538	1.32384	.78316	1.27688	.81171	1.23196	56
5	.72877	1.37218	.75584	1.32304	.78363	1.27611	.81220	1.23123	55
6	.72921	1.37134	.75629	1.32224	.78410	1.27535	.81268	1.23050	54
7	.72966	1.37050	.75675	1.32144	.78457	1.27458	.81316	1.22977	53
8	.73010	1.36967	.75721	1.32064	.78504	1.27382	.81364	1.22904	52
9	.73055	1.36883	.75767	1.31984	.78551	1.27306	.81413	1.22831	51
10	.73100	1.36800	.75812	1.31904	.78598	1.27230	.81461	1.22758	50
11	.73144	1.36716	.75858	1.31825	.78645	1.27153	.81510	1.22685	49
12	.73189	1.36633	.75904	1.31745	.78692	1.27077	.81558	1.22612	48
13	.73234	1.36549	.75950	1.31666	.78739	1.27001	.81606	1.22539	47
14	.73278	1.36466	.75996	1.31586	.78786	1.26925	.81655	1.22467	46
15	.73323	1.36383	.76042	1.31507	.78834	1.26849	.81703	1.22394	45
16	.73368	1.36300	.76088	1.31427	.78881	1.26774	.81752	1.22321	44
17	.73413	1.36217	.76134	1.31348	.78928	1.26698	.81800	1.22249	43
18	.73457	1.36134	.76180	1.31269	.78975	1.26622	.81849	1.22176	42
19	.73502	1.36051	.76226	1.31190	.79022	1.26546	.81898	1.22104	41
20	.73547	1.35968	.76272	1.31110	.79070	1.26471	.81946	1.22031	40
21	.73592	1.35885	.76318	1.31031	.79117	1.26395	.81905	1.21959	39
22	.73637	1.35802	.76364	1.30952	.79164	1.26319	.82044	1.21886	38
23	.73681	1.35719	.76410	1.30873	.79212	1.26244	.82092	1.21814	37
24	.73726	1.35637	.76456	1.30795	.79259	1.26169	.82141	1.21742	36
25	.73771	1.35554	.76502	1.30716	.79306	1.26093	.82190	1.21670	35
26	.73816	1.35472	.76548	1.30637	.79354	1.26018	.82238	1.21598	34
27	.73861	1.35389	.76594	1.30558	.79401	1.25943	.82287	1.21526	33
28	.73906	1.35307	.76640	1.30480	.79449	1.25867	.82336	1.21454	32
29	.73951	1.35224	.76686	1.30401	.79496	1.25792	.82385	1.21382	31
30	.73996	1.35142	.76733	1.30323	.79544	1.25717	.82434	1.21310	30
31	.74041	1.35060	.76779	1.30244	.79591	1.25642	.82483	1.21238	29
32	.74086	1.34978	.76825	1.30166	.79639	1.25567	.82531	1.21166	28
33	.74131	1.34896	.76871	1.30087	.79686	1.25492	.82580	1.21094	27
34	.74176	1.34814	.76918	1.30009	.79734	1.25417	.82629	1.21023	26
35	.74221	1.34732	.76964	1.29931	.79781	1.25343	.82678	1.20951	25
36	.74267	1.34650	.77010	1.29853	.79829	1.25268	.82727	1.20879	24
37	.74312	1.34568	.77057	1.29775	.79877	1.25193	.82776	1.20808	23
38	.74357	1.34487	.77103	1.29696	.79924	1.25118	82825	1.20736	22
39	.74402	1.34405	.77149	1.29618	.79972	1.25044	.82874	1.20665	21
40	.74447	1.34323	.77196	1.29541	.80020	1.24969	.82923	1.20593	20
41	.74492	1.34242	.77242	1.29463	.80067	1.24895	.82972	1.20522	19
42	.74538	1.34160	.77289	1.29385	.80115	1.24820	.83022	1.20451	18
43	.74583	1.34079	.77335	1.29307	.80163	1.24746	.83071	1.20379	17
44	.74628	1.33998	.77382	1.29229	.80211	1.24672	.83120	1.20308	16
45	.74674	1.33916	.77428	1.29152	.80258	1.24597	.83169	1.20237	15
46	.74719	1.33835	.77475	1.29074	.80306	1.24523	.83218	1.20166	14
47	.74764	1.33754	.77521	1.28997	.80354	1.24449	.83268	1.20095	13
48	.74810	1.33673	.77568	1.28919	.80402	1.24375	.83317	1.20024	12
49	.74855	1.33592	.77615	1.28842	.80450	1.24301	.83366	1.19953	11
50	.74900	1.33511	.77661	1.28764	.80498	1.24227	.83415	1.19882	10
51	.74946	1.33430	.77708	1.28687	.80546	1.24153	.83465	1.19811	9
52	.74991	1.33349	.77754	1.28610	.80594	1.24079	.83514	1.19740	8
53	.75037	1.33268	.77801	1.28533	.80642	1.24005	.83564	1.19669	7
54	.75082	1.33187	.77848	1.28456	.80690	1.23931	.83613	1.19599	6
55	.75128	1.33107	.77895	1.28379	.80738	1.23858	.83662	1.19528	5
56	.75173	1.33026	.77941	1.28302	.80786	1.23784	.83712	1.19457	4
57	.75219	1.32946	.77988	1.28225	.80834	1.23710	.83761	1.19387	3
58	.75264	1.32865	.78035	1.28148	.80882	1.23637	.83811	1.19316	2
59	.75310	1.32785	.78082	1.28071	.80930	1.23563	.83860	1.19246	1
60	.75355	1.32704	.78129	1.27994	.80978	1.23490	.83910	1.19175	0
′	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	′
	53°		52°		51°		50°		

′	40° Tang	40° Cotang	41° Tang	41° Cotang	42° Tang	42° Cotang	43° Tang	43° Cotang	′
0	.83910	1.19175	.86929	1.15037	.90040	1.11061	.93252	1.07237	60
1	.83960	1.19105	.86980	1.14969	.90093	1.10996	.93306	1.07174	59
2	.84009	1.19035	.87031	1.14902	.90146	1.10931	.93360	1.07112	58
3	.84059	1.18964	.87082	1.14834	.90199	1.10867	.93415	1.07049	57
4	.84108	1.18894	.87133	1.14767	.90251	1.10802	.93469	1.06987	56
5	.84158	1.18824	.87184	1.14699	.90304	1.10737	.93524	1.06925	55
6	.84208	1.18754	.87236	1.14632	.90357	1.10672	.93578	1.06862	54
7	.84258	1.18684	.87287	1.14565	.90410	1.10607	.93633	1.06800	53
8	.84307	1.18614	.87338	1.14498	.90463	1.10543	.93688	1.06738	52
9	.84357	1.18544	.87389	1.14430	.90516	1.10478	.93742	1.06676	51
10	.84407	1.18474	.87441	1.14363	.90569	1.10414	.93797	1.06613	50
11	.84457	1.18404	.87492	1.14296	.90621	1.10349	.93852	1.06551	49
12	.84507	1.18334	.87543	1.14229	.90674	1.10285	.93906	1.06489	48
13	.84556	1.18264	.87595	1.14162	.90727	1.10220	.93961	1.06427	47
14	.84606	1.18194	.87646	1.14095	.90781	1.10156	.94016	1.06365	46
15	.84656	1.18125	.87698	1.14028	.90834	1.10091	.94071	1.06303	45
16	.84706	1.18055	.87749	1.13961	.90887	1.10027	.94125	1.06241	44
17	.84756	1.17986	.87801	1.13894	.90940	1.09963	.94180	1.06179	43
18	.84806	1.17916	.87852	1.13828	.90993	1.09899	.94235	1.06117	42
19	.84856	1.17846	.87904	1.13761	.91046	1.09834	.94290	1.06056	41
20	.84906	1.17777	.87955	1.13694	.91099	1.09770	.94345	1.05994	40
21	.84956	1.17708	.88007	1.13627	.91153	1.09706	.94400	1.05932	39
22	.85006	1.17638	.88059	1.13561	.91206	1.09642	.94455	1.05870	38
23	.85057	1.17569	.88110	1.13494	.91259	1.09578	.94510	1.05809	37
24	.85107	1.17500	.88162	1.13428	.91313	1.09514	.94565	1.05747	36
25	.85157	1.17430	.88214	1.13361	.91366	1.09450	.94620	1.05685	35
26	.85207	1.17361	.88265	1.13295	.91419	1.09386	.94676	1.05624	34
27	.85257	1.17292	.88317	1.13228	.91473	1.09322	.94731	1.05562	33
28	.85308	1.17223	.88369	1.13162	.91526	1.09258	.94786	1.05501	32
29	.85358	1.17154	.88421	1.13096	.91580	1.09195	.94841	1.05439	31
30	.85408	1.17085	.88473	1.13029	.91633	1.09131	.94896	1.05378	30
31	.85458	1.17016	.88524	1.12963	.91687	1.09067	.94952	1.05317	29
32	.85509	1.16947	.88576	1.12897	.91740	1.09003	.95007	1.05255	28
33	.85559	1.16878	.88628	1.12831	.91794	1.08940	.95062	1.05194	27
34	.85609	1.16809	.88680	1.12765	.91847	1.08876	.95118	1.05133	26
35	.85660	1.16741	.88732	1.12699	.91901	1.08813	.95173	1.05072	25
36	.85710	1.16672	.88784	1.12633	.91955	1.08749	.95229	1.05010	24
37	.85761	1.16603	.88836	1.12567	.92008	1.08686	.95284	1.04949	23
38	.85811	1.16535	.88888	1.12501	.92062	1.08622	.95340	1.04888	22
39	.85862	1.16466	.88940	1.12435	.92116	1.08559	.95395	1.04827	21
40	.85912	1.16398	.88992	1.12369	.92170	1.08496	.95451	1.04766	20
41	.85963	1.16329	.89045	1.12303	.92224	1.08432	.95506	1.04705	19
42	.86014	1.16261	.89097	1.12238	.92277	1.08369	.95562	1.04644	18
43	.86064	1.16192	.89149	1.12172	.92331	1.08306	.95618	1.04583	17
44	.86115	1.16124	.89201	1.12106	.92385	1.08243	.95673	1.04522	16
45	.86166	1.16056	.89253	1.12041	.92439	1.08179	.95729	1.04461	15
46	.86216	1.15987	.89306	1.11975	.92493	1.08116	.95785	1.04401	14
47	.86267	1.15919	.89358	1.11909	.92547	1.08053	.95841	1.04340	13
48	.86318	1.15851	.89410	1.11844	.92601	1.07990	.95897	1.04279	12
49	.86368	1.15783	.89463	1 11778	.92655	1.07927	.95952	1.04218	11
50	.86419	1.15715	.89515	1.11713	.92709	1.07864	.96008	1.04158	10
51	.86470	1.15647	.89567	1.11648	.92763	1.07801	.96064	1.04097	9
52	.86521	1.15579	.89620	1.11582	.92817	1.07738	.96120	1.04036	8
53	.86572	1.15511	.89672	1.11517	.92872	1.07676	.96176	1.03976	7
54	.86623	1.15443	.89725	1.11452	.92926	1.07613	.96232	1.03915	6
55	.86674	1.15375	.89777	1.11387	.92980	1.07550	.96288	1.03855	5
56	.86725	1.15308	.89830	1.11321	.93034	1.07487	.96344	1.03794	4
57	.86776	1.15240	.89883	1.11256	.93088	1.07425	.96400	1.03734	3
58	.86827	1.15172	.89935	1.11191	.93143	1.07362	.96457	1.03674	2
59	.86878	1.15104	.89988	1.11126	.93197	1.07299	.96513	1.03613	1
60	.86929	1.15037	.90040	1.11061	.93252	1.07237	.96569	1.03553	0
′	Cotang 49°	Tang 49°	Cotang 48°	Tang 48°	Cotang 47°	Tang 47°	Cotang 46°	Tang 46°	′

′	44° Tang	44° Cotang	′	′	44° Tang	44° Cotang	′	′	44° Tang	44° Cotang	′
0	.96569	1.03553	60	20	.97700	1.02355	40	40	.98843	1.01170	20
1	.96625	1.03493	59	21	.97756	1.02295	39	41	.98901	1.01112	19
2	.96681	1.03433	58	22	.97813	1.02236	38	42	.98958	1.01053	18
3	.96738	1.03372	57	23	.97870	1.02176	37	43	.99016	1.00994	17
4	.96794	1.03312	56	24	.97927	1.02117	36	44	.99073	1.00935	16
5	.96850	1.03252	55	25	.97984	1.02057	35	45	.99131	1.00876	15
6	.96907	1.03192	54	26	.98041	1.01998	34	46	.99189	1.00818	14
7	.96963	1.03132	53	27	.98098	1.01939	33	47	.99247	1.00759	13
8	.97020	1.03072	52	28	.98155	1.01879	32	48	.99304	1.00701	12
9	.97076	1.03012	51	29	.98213	1.01820	31	49	.99362	1.00642	11
10	.97133	1.02952	50	30	.98270	1.01761	30	50	.99420	1.00583	10
11	.97189	1.02892	49	31	.98327	1.01702	29	51	.99478	1.00525	9
12	.97246	1.02832	48	32	.98384	1.01642	28	52	.99536	1.00467	8
13	.97302	1.02772	47	33	.98441	1.01583	27	53	.99594	1.00408	7
14	.97359	1.02713	46	34	.98499	1.01524	26	54	.99652	1.00350	6
15	.97416	1.02653	45	35	.98556	1.01465	25	55	.99710	1.00291	5
16	.97472	1.02593	44	36	.98613	1.01406	24	56	.99768	1.00233	4
17	.97529	1.02533	43	37	.98671	1.01347	23	57	.99826	1.00175	3
18	.97586	1.02474	42	38	.98728	1.01288	22	58	.99884	1.00116	2
19	.97643	1.02414	41	39	.98786	1.01229	21	59	.99942	1.00058	1
20	.97700	1.02355	40	40	.98843	1.01170	20	60	1.00000	1.00000	0
′	Cotang 45°	Tang 45°	′	′	Cotang 45°	Tang 45°	′	′	Cotang 45°	Tang 45°	′

LENGTHS OF CIRCULAR ARCS.

Radius = 1.

	Degrees.	Minutes.	Seconds.
1	0.017 453 293	0.000 290 888	0.000 004 848
2	.034 906 585	.000 581 776	.000 009 696
3	.052 359 878	.000 872 664	.000 014 544
4	.069 813 170	.001 163 553	.000 019 393
5	.087 266 463	.001 454 440	.000 024 241
6	.104 719 755	.001 745 329	.000 029 089
7	.122 173 048	.002 036 217	.000 033 937
8	.139 626 340	.002 327 106	.000 038 785
9	.157 079 633	.002 617 994	.000 043 633
10	.174 532 925	.002 908 882	.000 048 481

TABLE III.

DAILY VARIATION OF THE MAGNETIC NEEDLE AT PHILADELPHIA, PA.

	Jan.	Feb.	Mar.	Apr.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.
	′	′	′	′	′	′	′	′				
6 A.M.	+0.6	+1.2	+1.8	+2.6	+3.7	+3.9	+4.2	+4.7	+3.5	+1.3	+1.2	+0.7
7	+1.2	+1.9	+2.9	+3.5	+4.7	+5.0	+5.4	+5.7	+4.5	+1.7	+1.7	+1.0
8	+2.1	+2.5	+3.7	+4.0	+4.7	+5.1	+5.4	+5.5	+4.5	+2.2	+1.9	+1.4
9	+2.5	+2.5	+3.4	+3.4	+3.2	+3.8	+4.0	+3.7	+2.8	+1.9	+1.5	+1.6
10	+1.6	+1.5	+1.8	+1.5	+0.8	+1.2	+1.5	+0.6	−0.1	+0.8	+0.4	+1.1
11	−0.3	−0.2	−0.6	−1.1	−1.9	−1.7	−1.5	−2.9	−3.2	−0.8	−1.1	−0.3
Noon	−2.3	−2.0	−2.7	−3.6	−4.1	−4.0	−3.9	−5.4	−5.2	−2.6	−2.2	−1.9
1	−3.4	−3.0	−3.9	−5.1	−5.1	−5.0	−5.3	−6.3	−5.5	−3.2	−2.8	−3.0
2	−3.3	−3.0	−3.9	−5.2	−4.9	−4.8	−5.4	−5.5	−4.5	−3.0	−2.6	−3.0
3	−2.5	−2.4	−3.2	−4.3	−3.9	−3.8	−4.5	−3.8	−3.0	−2.2	−1.9	−2.3
4	−1.5	−1.7	−2.3	−3.0	−2.5	−2.6	−3.3	−2.0	−1.7	−1.1	−1.2	−1.3
5	−0.9	−1.2	−1.6	−1.8	−1.2	−1.6	−2.0	−0.9	−0.8	−0.3	−0.6	−0.6
6	−0.6	−0.8	−1.0	−0.9	−0.4	−0.9	−1.2	−0.5	−0.3	+0.4	−0.1	−0.1

The above table, which is taken from the U. S. Coast and Géodetic Survey Report for 1881, gives the mean results of five years' observations of the daily variation of the magnetic needle at Philadelphia. A plus sign indicates a deviation of the north end of the needle to the eastward of the magnetic meridian, a minus sign indicates a deviation to the westward.

For other places in the United States the daily variation may be approximately ascertained by multiplying the values for Philadelphia by the numbers taken from the following supplementary table. For example, at a place in latitude 45 degrees

Lat.	Long. 70°.	Long. 80°.	Long. 90°.	Long. 100°.	Long. 110°.	Long. 120°.
25°	....	0.64	0.64	0.63	0.60	....
30	....	0.71	0.70	0.68	0.66	0.65
35	0.93	0.86	0.80	0.77	0.76	0.74
40	1.05	1.00	0.93	0.90	0.82	0.80
45	1.31	1.35	1.20	1.05	0.95	0.93
50	....	....	1.50	1.67	1.24	1.14

and longitude 95 degrees the multiplier is 1.13. In southern latitudes, moreover, the maximum deviations occur about an hour later than in northern, and in any particular case the table cannot be depended upon within one hour on account of minor irregularities and disturbances.

TO REDUCE DEGREES TO TIME.

° / ′ / ″	H. M. / M. S. / S. T.	° / ′ / ″	H. M. / M. S. / S. T.	Degrees.	Hours. Minutes.
1	0 4	51	3 24	101	6 44
2	0 8	52	3 28	102	6 48
3	0 12	53	3 32	103	6 52
4	0 16	54	3 36	104	6 56
5	0 20	55	3 40	105	7 0
6	0 24	56	3 44	106	7 4
7	0 28	57	3 48	107	7 8
8	0 32	58	3 52	108	7 12
9	0 36	59	3 56	109	7 16
10	0 40	60	4 0	110	7 20
11	0 44	61	4 4	115	7 40
12	0 48	62	4 8	120	8 0
13	0 52	63	4 12	125	8 20
14	0 56	64	4 16	130	8 40
15	1 0	65	4 20	135	9 0
16	1 4	66	4 24	140	9 20
17	1 8	67	4 28	145	9 40
18	1 12	68	4 32	150	10 0
19	1 16	69	4 36	155	10 20
20	1 20	70	4 40	160	10 40
21	1 24	71	4 44	165	11 0
22	1 28	72	4 48	170	11 20
23	1 32	73	4 52	175	11 40
24	1 36	74	4 56	180	12 0
25	1 40	75	5 0	185	12 20
26	1 44	76	5 4	190	12 40
27	1 48	77	5 8	195	13 0
28	1 52	78	5 12	200	13 20
29	1 56	79	5 16	205	13 40
30	2 0	80	5 20	210	14 0
31	2 4	81	5 24	215	14 20
32	2 8	82	5 28	220	14 40
33	2 12	83	5 32	225	15 0
34	2 16	84	5 36	230	15 20
35	2 20	85	5 40	235	15 40
36	2 24	86	5 44	240	16 0
37	2 28	87	5 48	245	16 20
38	2 32	88	5 52	250	16 40
39	2 36	89	5 56	255	17 0
40	2 40	90	6 0	260	17 20
41	2 44	91	6 4	270	18 0
42	2 48	92	6 8	280	18 40
43	2 52	93	6 12	290	19 20
44	2 56	94	6 16	300	20 0
45	3 0	95	6 20	310	20 40
46	3 4	96	6 24	320	21 20
47	3 8	97	6 28	330	22 0
48	3 12	98	6 32	340	22 40
49	3 16	99	6 36	350	23 20
50	3 20	100	6 40	360	24 0

TO REDUCE TIME TO DEGREES.

Hours.	Degrees.	M. / S. / T.	° ′ / ′ ″ / ″ ‴	M. / S. / T.	° ′ / ′ ″ / ″ ‴
1	15	1	0 15	51	12 45
1½	22½	2	0 30	52	13 0
2	30	3	0 45	53	13 15
2½	37½	4	1 0	54	13 30
3	45	5	1 15	55	13 45
3½	52½	6	1 30	56	14 0
4	60	7	1 45	57	14 15
4½	67½	8	2 0	58	14 30
5	75	9	2 15	59	14 45
5½	82½	10	2 30	60	15 0
6	90	11	2 45	61	15 15
6½	97½	12	3 0	62	15 30
7	105	13	3 15	63	15 45
7½	112½	14	3 30	64	16 0
8	120	15	3 45	65	16 15
8½	127½	16	4 0	66	16 30
9	135	17	4 15	67	16 45
9½	142½	18	4 30	68	17 0
10	150	19	4 45	69	17 15
10½	157½	20	5 0	70	17 30
11	165	21	5 15	71	17 45
11½	172½	22	5 30	72	18 0
12	180	23	5 45	73	18 15
12½	187½	24	6 0	74	18 30
13	195	25	6 15	75	18 45
13½	202½	26	6 30	76	19 0
14	210	27	6 45	77	19 15
14½	217½	28	7 0	78	19 30
15	225	29	7 15	79	19 45
15½	232½	30	7 30	80	20 0
16	240	31	7 45	81	20 15
16½	247½	32	8 0	82	20 30
17	255	33	8 15	83	20 45
17½	262½	34	8 30	84	21 0
18	270	35	8 45	85	21 15
18½	277½	36	9 0	86	21 30
19	285	37	9 15	87	21 45
19½	292½	38	9 30	88	22 0
20	300	39	9 45	89	22 15
20½	307½	40	10 0	90	22 30
21	315	41	10 15	91	22 45
21½	322½	42	10 30	92	23 0
22	330	43	10 45	93	23 15
22½	337½	44	11 0	94	23 30
23	345	45	11 15	95	23 45
23½	352½	46	11 30	96	24 0
24	360	47	11 45	97	24 15
		48	12 0	98	24 30
		49	12 15	99	24 45
		50	12 30	100	25 0

TABLE V.

LOCAL TIMES OF ELONGATIONS OF POLARIS IN 1915.

For 40° North Latitude and 90° West Longitude.

Date in 1915.		Eastern Elongation.		Western Elongation.	
		h.	m.	h.	m.
January	1	12	51.7 P.M.	12	42.1 A.M.
	15	11	52.5 A.M.	11	46.8 P.M.
February	1	10	45.3 A.M.	10	39.7 P.M.
	15	9	50.1 A.M.	9	44.4 P.M.
March	1	8	54.8 A.M.	8	49.2 P.M.
	15	7	59.6 A.M.	7	54.0 P.M.
April	1	6	52.7 A.M.	6	47.1 P.M.
	15	5	57.7 A.M.	5	52.0 P.M.
May	1	4	54.8 A.M.	4	49.2 P.M.
	15	3	59.9 A.M.	3	54.2 P.M.
June	1	2	53.3 A.M.	2	47.6 P.M.
	15	1	58.5 A.M.	1	52.8 A.M.
July	1	12	55.9 A.M.	12	50.2 A.M.
	15	12	01.1 P.M.	11	51.5 A.M.
August	1	10	54.5 P.M.	10	44.9 A.M.
	15	9	59.8 P.M.	9	50.2 A.M.
September	1	8	53.2 P.M.	8	43.6 A.M.
	15	7	58.3 P.M.	7	48.7 A.M.
October	1	6	55.5 P.M.	6	45.9 A.M.
	15	6	00.6 P.M.	5	51.0 A.M.
November	1	4	53.7 P.M.	4	44.1 A.M.
	15	3	58.6 P.M.	3	49.0 A.M.
December	1	2	55.6 P.M.	2	46.0 A.M.
	15	2	00.4 P.M.	1	50.8 A.M.

For other years than 1915, the following quantities should be added or subtracted to the above tabular values:

For 1913	subtract	2.9 minutes
1914	subtract	1.5
1916, before March 1,	add	1.6
1916, after Feb. 29,	subtract	2.3
1917	subtract	0.7
1918	add	0.9
1919	add	2.5
1920, before March 1,	add	4.0
1920, after Feb. 29,	add	0.1
1921	add	1.6
1922	add	3.1
1923	add	4.5
1924, before March 1,	add	5.9
1924, after Feb. 29,	add	2.0
1925	add	3.3
1926	add	4.6
1927	add	5.9

To obtain the time of elongation for any day not given in the table, add 3.93 minutes for every day from it to the day of the next following tabular value. For example, the eastern elongation on Nov. 12, 1915, occurred at $4^h\ 10^m.4$ P.M. in latitude 40° and longitude 90°.

For any latitude other than 40°, between 25° and 50° north, there should be added to the time of western elongation 0.10 minutes for every degree south of 40° and 0.16 minutes be subtracted for every degree north of 40°. For eastern elongations 0.10 minutes should be subtracted for every degree south of 40° and 0.16 minutes be added for every degree north of 40°. For any longitude other than 90° west of Greenwich, add 0.16 minutes for each 15 degrees east of the ninetieth meridian and subtract 0.16 minutes for each 15 degrees west of that meridian.

The time in Table V is local time, which is the same as mean solar time. Local time can be reduced to standard time by adding or subtracting 4.0 minutes for each degree of longitude west or east of the meridian of the standard.

As an example involving all these corrections, let it be required to find, for an observer in north latitude 42° 06′ and west longitude 78° 45′, the standard time of the eastern elongation of Polaris on Aug. 28, 1920. From the Table the local time $8^h\ 35^m.2$ P.M. is found for Sept. 1, 1915, and to this is added the correction for 1920, making $8^h\ 53^m.3$ P.M. for Sept. 1, 1920. To this $15^m.7$ are added for the four days from Aug. 28 to Sept. 1, giving $9^h\ 09^m.0$ P.M. for Aug. 24, 1920. The corrections for latitude and longitude of the given station are $-0^m.34$ and $+0^m.12$; hence the eastern elongation will occur at that station on Aug. 28, 1920, at $9^h\ 08^m.8$ P.M. On a watch indicating eastern standard time the time of the eastern elongation for the given day and station will be $9^h\ 23^m.8$ P.M. A result deduced in this manner will usually be correct within about $0^m.3$.

Table V has been taken from "Principal Facts of the Earth's Magnetism," issued in 1914 by the U. S. Coast and Geodetic Survey.

Table VI.

AZIMUTHS OF POLARIS AT ELONGATION.

Lat.	1911	1912	1913	1914	1915	1916	1917	1918
25°	1° 17′.4	1° 17′.0	1° 16′.7	1° 16′.4	1° 16′.0	1° 15′.7	1° 15′.3	1° 15′.0
26	18 .0	17 .7	17 .3	17 .0	16 .6	16 .3	16 .0	15 .6
27	18 .7	18 .4	18 .0	17 .7	17 .3	17 .0	16 .6	16 .3
28	19 .4	19 .1	18 .7	18 .4	18 .0	17 .7	17 .3	17 .0
29	20 .2	19 .8	19 .5	19 .1	18 .8	18 .4	18 .1	17 .7
30	21 .0	20 .6	20 .3	19 .9	19 .6	19 .2	18 .8	18 .5
31	21 .8	21 .5	21 .1	20 .7	20 .4	20 .0	19 .7	19 .3
32	22 .7	22 .3	22 .0	21 .6	21 .2	20 .9	20 .5	20 .1
33	23 .6	23 .3	22 .9	22 .5	22 .1	21 .8	21 .4	21 .0
34	24 .6	24 .2	23 .8	23 .5	23 .1	22 .7	22 .4	22 .0
35	25 .6	25 .2	24 .9	24 .5	24 .1	23 .7	23 .3	23 .0
36	26 .7	26 .3	26 .9	25 .5	25 .2	24 .8	24 .4	24 .0
37	27 .8	27 .4	27 .0	26 .7	26 .3	25 .9	25 .5	25 .1
38	29 .0	28 .6	28 .2	27 .8	27 .4	27 .0	26 .6	26 .2
39	30 .2	29 .8	29 .4	29 .0	28 .6	28 .2	27 .8	27 .5
40	31 .6	31 .1	30 .7	30 .3	29 .9	29 .5	29 .1	28 .7
41	32 .9	32 .5	32 .1	31 .7	31 .3	30 .9	30 .4	30 .0
42	34 .4	34 .0	33 .5	33 .1	32 .7	32 .3	31 .9	31 .5
43	35 .9	35 .5	35 .0	34 .6	34 .2	33 .8	33 .4	32 .9
44	37 .5	37 .1	36 .6	36 .2	35 .8	35 .3	34 .9	34 .5
45	39 .2	38 .7	38 .3	37 .8	37 .4	37 .0	36 .6	36 .1
46	41 .0	40 .5	40 .1	39 .6	39 .2	38 .7	38 .3	37 .8
47	42 .8	42 .4	41 .9	41 .5	41 .0	40 .6	40 .1	39 .7
48	44 .8	44 .4	43 .9	43 .4	43 .0	42 .5	42 .0	41 .6
49	46 .9	46 .4	46 .0	45 .5	45 .0	44 .5	44 .1	43 .6
50	49 .1	1 48 .6	1 48 .2	1 47 .7	1 47 .2	1 46 .7	1 46 .2	1 45 .7

The azimuths in Table VI are reckoned from the true north toward the east for eastern elongation and from the true north toward the west for western elongation. For intermediate latitudes values may be obtained by interpolation; for example, in latitude 41° 30′ the mean azimuth during 1913 is 1° 32′.8, and for July 1, 1913, the azimuth is 1° 33′.2. An azimuth deduced in this manner will in general be correct within 0′.3

This table has been taken from "Principal Facts of the Earth's Magnetism," issued in 1914 by the U. S. Coast and Geodetic Survey.

AZIMUTHS OF POLARIS AT ELONGATION.

Lat.	1919	1920	1921	1922	1923	1924	1925	1926
25°	1° 14′.7	1° 14′.7	1° 14′.0	1° 13′.6	1° 13′.3	1° 13′.0	1° 12′.6	1° 12′.3
26	15 .3	14 .9	14 .7	14 .2	13 .9	13 .6	13 .2	12 .9
27	15 .9	15 .6	15 .2	14 .9	14 .6	14 .2	13 .9	13 .5
28	16 .6	16 .3	15 .9	15 .6	15 .2	14 .9	14 .6	14 .2
29	17 .4	17 .0	16 .6	16 .3	16 .0	15 .6	15 .2	14 .9
30	19 .1	18 .8	17 .4	17 .0	16 .7	16 .4	16 .0	15 .6
31	19 .9	18 .6	18 .2	17 .9	17 .5	17 .2	16 .8	16 .4
32	19 .8	18 .4	19 .1	18 .7	18 .3	18 .0	17 .6	17 .2
33	20 .7	20 .3	19 .9	19 .6	19 .2	18 .8	18 .5	18 .1
34	21. 6	21 .2	20 .9	20 .5	20 .1	19 .8	19 .4	19 .0
35	22 .6	22. 2	21. 8	21 .5	21 .1	20 .7	20 .4	20 .0
36	23 .6	23 .3	22. 9	22 .5	22 .1	21 .7	21 .4	21 .0
37	24 .7	24 .3	24 .0	23 .6	23 .2	22 .8	22 .4	22 .0
38	25 .9	25 .5	25 .1	24 .7	24 .3	23 .9	23 .5	23 .2
39	27 .1	26 .7	26 .3	25 .8	25 .5	25 .1	24 .7	24 .3
40	28 .3	27 .9	27 .5	27 .1	26 .7	26 .3	25 .9	25 .5
41	29 .6	29 .1	28 .8	28 .4	28 .0	27 .6	27 .2	26 .8
42	31 .0	30 .6	30 .2	29 .8	29 .4	29 .0	28 .6	28 .2
43	32. 5	32 .1	31 .8	31 .2	30 .8	30 .4	30 .0	29 .6
44	34 .1	33. 6	33 .2	32 .8	32 .4	31 .9	31 .5	31 .1
45	35 .7	35 .3	34 .8	34 .4	34 .0	33. 5	33 .1	32 .6
46	37 .4	37 .0	36 .5	36 .1	35 .6	35 .2	34 .8	34 .3
47	39 .2	38 .8	38 .3	37 .9	37 .4	36 .5	36 .5	36 .1
48	41 .1	40 .7	40 .2	39 .8	39 .3	38 .8	38 .4	37 .9
49	43 .1	42 .7	42 .2	41 .7	41 .3	40 .8	40 .3	39 .9
50°	1° 45′.3	1° 44′.8	1° 44′.3	1° 43′.8	1° 43′.4	1° 42′.9	1° 42′.4	1° 41′.9

When an azimuth is required with a precision less than one minute, a correction taken from the following supplementary table should be applied. For example, the azimuth as seen in latitude 42° on Dec. 1, 1920, is 1° 29′.9. An azimuth deduced in this manner will generally be correct within 0′.3.

For middle of	Correction.	For middle of	Correction.
January............	−0 .5	July..............	+0 .2
February..........	−0 .4	August............	+0 .1
March.............	−0 .3	September.........	−0 .1
April...............	0 .0	October...........	−0 .4
May...............	+0 .1	November.........	−0 .6
June..............	+0 .2	December..........	−0 .8

CONVERSION OF ENGLISH INCHES INTO CENTIMETRES.

Ins.	0	1	2	3	4	5	6	7	8	9
	Cm.	Cm.	Cm.	Cm.	Cm.	Cm.	Cm.	Cm.	Cm.	Cm.
0	0.000	2.540	5.080	7.620	10.16	12.70	15.24	17.78	20.32	22.86
10	25.40	27.94	30.48	33.02	35.56	38.10	40.64	43.18	45.72	48.26
20	50.80	53.34	55.88	58.42	60.96	63.50	66.04	68.58	71.12	73.66
30	76.20	78.74	81.28	83.82	86.36	88.90	91.44	93.98	96.52	99.06
40	101.60	104.14	106.68	109.22	111.76	114.30	116.84	119.38	121.92	124.46
50	127.00	129.54	132.08	134.62	137.16	139.70	142.24	144.78	147.32	149.86
60	152.40	154.94	157.48	160.02	162.56	165.10	167.64	170.18	172.72	175.26
70	177.80	180.34	182.88	185.42	187.96	190.50	193.04	195.58	198.12	200.96
80	203.20	205.74	208.28	210.82	213.36	215.90	218.44	220.98	223.52	226.06
90	228.60	231.14	233.68	236.22	238.76	241.30	243.84	246.38	248.92	251.46
100	254.00	256.54	259.08	261.62	264.16	266.70	269.24	271.78	274.32	276.86

CONVERSION OF CENTIMETRES INTO ENGLISH INCHES.

Cm.	0	1	2	3	4	5	6	7	8	9
	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.
0	0.000	0.394	0.787	1.181	1.575	1.969	2.362	2.756	3.150	3.543
10	3.937	4.331	4.742	5.118	5.512	5.906	6.299	6.693	7.087	7.480
20	7.874	8.268	8.662	9.055	9.449	9.843	10.236	10.630	11.024	11.418
30	11.811	12.205	12.599	12.992	13.386	13.780	14.173	14.567	14.961	15.355
40	15.748	16.142	16.536	16.929	17.323	17.717	18.111	18.504	18.898	19.292
50	19.685	20.079	20.473	20.867	21.260	21.654	22.048	22.441	22.835	23.229
60	23.622	24.016	24.410	24.804	25.197	25.591	25.985	26.378	26.772	27.166
70	27.560	27.953	28.347	28.741	29.134	29.528	29.922	30.316	30.709	31.103
80	31.497	31.890	32.284	32.678	33.071	33.465	33.859	34.253	34.646	35.040
90	35.434	35.827	36.221	36.615	37.009	37.402	37.796	38.190	38.583	38.977
100	39.370	39.764	40.158	40.552	40.945	41.339	41.733	42.126	42.520	42.914

CONVERSION OF ENGLISH FEET INTO METRES.

Feet.	0	1	2	3	4	5	6	7	8	9
	Met.	Met.	Met.	Met.	Met.	Met.	Met.	Met.	Met.	Met.
0	0.000	0.3048	0.6096	0.9144	1.2192	1.5239	1.8287	2.1335	2.4383	2.7431
10	3.0479	3.3527	3.6575	3.9623	4.2671	4.5719	4.8767	5.1815	5.4863	5.7911
20	6.0959	6.4006	6.7055	7.0102	7.3150	7.6198	7.9246	8.2294	8.5342	8.8390
30	9.1438	9.4486	9.7534	10.058	10.363	10.668	10.972	11.277	11.582	11.887
40	12.192	12.496	12.801	13.106	13.411	13.716	14.020	14.325	14.630	14.935
50	15.239	15.544	15.849	16.154	16.459	16.763	17.068	17.373	17.678	17.983
60	18.287	18.592	18.897	19.202	19.507	19.811	20.116	20.421	20.726	21.031
70	21.335	21.640	21.945	22.250	22.555	22.859	23.164	23.469	23.774	24.079
80	24.383	24.688	24.993	25.298	25.602	25.907	26.212	26.517	26.822	27.126
90	27.431	27.736	28.041	28.346	28.651	28.955	29.260	29.565	29.870	30.174
100	30.479	30.784	31.089	31.394	31.698	32.003	32.308	32.613	32.918	33.[illegible]

CONVERSION OF METRES INTO ENGLISH FEET.

Met.	0	1	2	3	4	5	6	7	8	9
	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
0	0.000	3.2809	6.5618	9.8427	13.123	16.404	19.685	22.966	26.247	29.528
10	32.809	36.090	39.371	42.651	45.932	49.213	52.494	55.775	59.056	62.337
20	65.618	68.899	72.179	75.461	78.741	82.022	85.303	88.584	91.865	95.146
30	98.427	101.71	104.99	108.27	111.55	114.83	118.11	121.39	124.67	127.96
40	131.24	134.52	137.80	141.08	144.36	147.64	150.92	154.20	157.48	160.76
50	164.04	167.33	170.61	173.89	177.17	180.45	183.73	187.01	190.29	193.57
60	196.85	200.13	203.42	206.70	209.98	213.26	216.54	219.82	223.10	226.38
70	229.66	232.94	236.22	239.51	242.79	246.07	249.35	252.63	255.91	259.19
80	262.47	265.75	269.03	272.31	275.60	278.88	282.16	285.44	288.72	292.00
90	295.28	298.56	301.84	305.12	308.40	311.69	314.97	318.25	321.53	324.81
100	328.09	331.37	334.65	337.93	341.21	344.49	347.78	351.06	354.34	357.[illegible]

CONVERSION OF ENGLISH STATUTE-MILES INTO KILOMETRES.

Miles.	0	1	2	3	4	5	6	7	8	9
	Kilo.	Kilo.	Kilo.	Kilo.	Kilo.	Kilo.	Kilo.	Kilo.	Kilo.	Kilo.
0	0.0000	1.6093	3.2186	4.8279	6.4372	8.0465	9.6558	11.2652	12.8745	14.4848
10	16.093	17.702	19.312	20.921	22.530	24.139	25.749	27.358	28.967	30.577
20	32.186	33.795	35.405	37.014	38.623	40.232	41.842	43.451	45.060	46.670
30	48.279	49.888	51.498	53.107	54.716	56.325	57.935	59.544	61.153	62.763
40	64.372	65.981	67.591	69.200	70.809	72.418	74.028	75.637	77.246	78.856
50	80.465	82.074	83.684	85.293	86.902	88.511	90.121	91.730	93.339	94.949
60	96.558	98.167	99.777	101.39	102.99	104.60	106 21	107.82	109.43	111.04
70	112.65	114.26	115.87	117.48	119.08	120.69	122.30	123.91	125.52	127.13
80	128.74	130.35	131.96	133.57	135.17	136.78	138.39	140.00	141.61	143.22
90	144.85	146.44	148.05	149.66	151.26	152.87	154.48	156.09	157.70	159.31
100	160.93	162.53	164 14	165 75	167.35	168.96	170.57	172.18	173.79	175.40

CONVERSION OF KILOMETRES INTO ENGLISH STATUTE-MILES.

Kilom.	0	1	2	3	4	5	6	7	8	9
	Miles.	Miles.	Miles.	Miles.	Miles.	Miles.	Miles.	Miles.	Miles.	Miles.
0	0.0000	0.6214	1.2427	1.8641	2.4855	3.1069	3.7282	4.3497	4.9711	5.5924
10	6.2138	6.8352	7.4565	8.0780	8.6994	9.3208	9.9421	10.562	11.185	11.805
20	12.427	13.049	13 670	14.292	14.913	15.534	16.156	16.776	17.399	18.019
30	18.641	19.263	19.884	20.506	21.127	21.748	23.370	22.990	23.613	24.233
40	24.855	25.477	26.098	26.720	27.341	27.962	28.584	29.204	29.827	30.447
50	31.069	31.690	32.311	32.933	33.554	34.175	34.797	35.417	36.040	36.660
60	37.282	37.904	38.525	39.147	39.768	40.389	41.011	41.631	42.254	42.874
70	43.497	44.118	44.739	45.361	45.982	46.603	47.225	47.845	48.468	49.088
80	49.711	50.332	50.953	51.575	52.196	52.817	53.439	54.059	54.682	55.302
90	55.924	56.545	57.166	57.788	58.409	59.030	59.652	60.272	60.895	61.515
100	62.138	62.759	63.380	64.002	64.623	65.244	65.866	66.486	67.109	67.729

TABLE VIII.
LENGTH IN FEET OF 1′ ARCS OF LATITUDE AND LONGITUDE.

Lat.	1′ Lat.	1′ Long.	Lat.	1′ Lat.	1′ Long.
1°	6045	6085	31°	6061	5222
2°	6045	6083	32°	6062	5166
3°	6045	6078	33°	6063	5109
4°	6045	6071	34°	6064	5051
5°	6045	6063	35°	6065	4991
6°	6045	6053	36°	6066	4930
7°	6046	6041	37°	6067	4867
8°	6046	6027	38°	6068	4802
9°	6046	6012	39°	6070	4736
10°	6047	5994	40°	6071	4668
11°	6047	5975	41°	6072	4600
12°	6048	5954	42°	6073	4530
13°	6048	5931	43°	6074	4458
14°	6049	5907	44°	6075	4385
15°	6049	5880	45°	6076	4311
16°	6050	5852	46°	6077	4235
17°	6050	5822	47°	6078	4158
18°	6051	5790	48°	6079	4080
19°	6052	5757	49°	6080	4001
20°	6052	5721	50°	6081	3920
21°	6053	5684	51°	6082	3838
22°	6054	5646	52°	6084	3755
23°	6054	5605	53°	6085	3671
24°	6055	5563	54°	6086	3586
25°	6056	5519	55°	6087	3499
26°	6057	5474	56°	6088	3413
27°	6058	5427	57°	6089	3323
28°	6059	5378	58°	6090	3233
29°	6060	5327	59°	6091	3142
30°	6061	5275	60°	6092	3051

TABLE IX.

REDUCTION OF INCLINED DISTANCES TO THE HORIZONTAL.

Inclined Distance = 100 feet.

Slope.	Correction.	Horizontal Distance.	Slope.	Correction.	Horizontal Distance.
0° 00′	....	100.000	8° 00′	0.973	99.027
30	0.004	99.996	30	1.098	98.902
1 00	0.015	99.985	9 00	1.231	98.769
30	0.034	99.966	30	1.371	98.629
2 00	0.061	99.939	10 00	1.519	98.481
30	0.095	99.905	30	1.675	98.325
3 00	0.137	99.863	11 00	1.837	98.163
30	0.187	99.813	30	2.008	97.992
4 00	0.244	99.756	12 00	2.185	97.814
30	0.308	99.692	30	2.370	97.630
5 00	0.381	99.619	13 00	2.563	97.437
30	0.460	99.540	30	2.763	97.237
6 00	0.548	99.452	14 00	2.970	97.030
30	0.643	99.357	30	3.185	96.815
7 00	0.745	99.255	15 00	3.407	96.593
30	0.856	99.144	30	3.637	96.363

ANSWERS TO PROBLEMS.

Prob. 1: $A = 24° 39'$, $B = 17° 56'$. Prob. 2: azimuth of $DE = 106° 45'$. Prob. 3: latitude = + 2458.2 feet, longitude = + 5379.4 feet. Prob. 4: area = 5 acres, 104 rods, 84 square feet. Prob. 5: for BC, + 382.1 feet, and + 823.3 feet. Prob. 6: Area = 11 acres, 116 rods, 126 square feet. Prob. 8: distance = 10340 feet. Prob. 9: M is 226.6 feet above N. Prob. 10: $AOD = 117° 52\frac{1}{2}'$, $COD = 22° 01\frac{1}{2}'$. Prob. 11: true area = 7 acres, 146 rods, 222 square feet. Prob. 13: maximum declination 8° 03′ in January, 1916. Prob. 14: area = 3 acres, 0 roods, 4.7 square rods. Prob. 18: N 78° 06′ W, 26 links, for A; S 74° 35′ W, 56 links for C. Prob. 20: 476.954 and 477.715 chains. Prob. 23: error = 0.025 feet. Prob. 28: pull = 17.1 pounds. Prob. 30: latitude = 2000.000 feet, longitude = 4000.000 feet. Prob. 31: $83\frac{1}{3}$ feet, 398.6 acres. Prob. 34: 902.6 and 417.1 for the first point.

TABLE X.

REDUCTION OF STADIA READINGS

TO

HORIZONTAL DISTANCES

AND TO

DIFFERENCES OF ELEVATION.

This table was computed by Professor Arthur Winslow, State Geologist of Missouri.

TABLE X.

STADIA REDUCTIONS FOR READING 100.

Minutes.	0° Hor. Dist.	0° Diff. Elev.	1° Hor. Dist.	1° Diff. Elev.	2° Hor. Dist.	2° Diff. Elev.	3° Hor. Dist.	3° Diff. Elev.
0′	100.00	.00	99.97	1.74	99.88	3.49	99.73	5.23
2	"	.06	"	1.80	99.87	3.55	99.72	5.28
4	"	.12	"	1.86	"	3.60	99.71	5.34
6	"	.17	99.96	1.92	"	3.66	"	5.40
8	"	.23	"	1.98	99.86	3.72	99.70	5.46
10	"	.29	"	2.04	"	3.78	99.69	5.52
12	"	.35	"	2.09	99.85	3.84	"	5.57
14	"	.41	99.95	2.15	"	3.90	99.68	5.63
16	"	.47	"	2.21	99.84	3.95	"	5.69
18	"	.52	"	2.27	"	4.01	99.67	5.75
20	"	.58	"	2.33	99.83	4.07	99.66	5.80
22	"	.64	99.94	2.38	"	4.13	"	5.86
24	"	.70	"	2.44	99.82	4.18	99.65	5.92
26	99.99	.76	"	2.50	"	4.24	99.64	5.98
28	"	.81	99.93	2.56	99.81	4.30	99.63	6.04
30	"	.87	"	2.62	"	4.36	"	6.09
32	"	.93	"	2.67	99.80	4.42	99.62	6.15
34	"	.99	"	2.73	"	4.48	"	6.21
36	"	1.05	99.92	2.79	99.79	4.53	99.61	6.27
38	"	1.11	"	2.85	"	4.59	99.60	6.33
40	"	1.16	"	2.91	99.78	4.65	99.59	6.38
42	"	1.22	99.91	2.97	"	4.71	"	6.44
44	99.98	1.28	"	3.02	99.77	4.76	99.58	6.50
46	"	1.34	99.90	3.08	"	4.82	99.57	6.56
48	"	1.40	"	3.14	99.76	4.88	99.56	6.61
50	"	1.45	"	3.20	"	4.94	"	6.67
52	"	1.51	99.89	3.26	99.75	4.99	99.55	6.73
54	"	1.57	"	3.31	99.74	5.05	99.54	6.78
56	99.97	1.63	"	3.37	"	5.11	99.53	6.84
58	"	1.69	99.88	3.43	99.73	5.17	99.52	6.90
60	"	1.74	"	3.49	"	5.23	99 51	6.96
$c+f=$ .75	.75	.01	.75	.02	.75	.03	.75	.05
$c+f=$ 1.00	1.00	.01	1.00	.03	1.00	.04	1.00	.06
$c+f=$ 1.25	1.25	.02	1.25	.03	1.25	.05	1.25	.08

TABLE X.

STADIA REDUCTIONS FOR READING 100.

Minutes.	4° Hor. Dist.	4° Diff. Elev.	5° Hor. Dist.	5° Diff. Elev.	6° Hor. Dist.	6° Diff. Elev.	7° Hor. Dist.	7° Diff. Elev.
0′	99.51	6.96	99.24	8.68	98.91	10.40	98.51	12.10
2	"	7.02	99.23	8.74	98.90	10.45	98.50	12.15
4	99.50	7.07	99.22	8.80	98.88	10.51	98.48	12.21
6	99.49	7.13	99.21	8.85	98.87	10.57	98.47	12.26
8	99.48	7.19	99.20	8.91	98.86	10 62	98.46	12.32
10	99.47	7.25	99.19	8.97	98.85	10.68	98.44	12.38
12	99.46	7.30	99.18	9.03	98.83	10.74	98.43	12.43
14	"	7.36	99.17	9.08	98.82	10.79	98.41	12.49
16	99.45	7.42	99.16	9.14	98.81	10.85	98.40	12.55
18	99.44	7.48	99.15	9.20	98.80	10.91	98.39	12.60
20	99.43	7.53	99.14	9.25	98.78	10.96	98.37	12.66
22	99.42	7.59	99.13	9.31	98.77	11.02	98.36	12.72
24	99.41	7.65	99.11	9.37	98.76	11.08	98.34	12.77
26	99.40	7.71	99.10	9.43	98.74	11.13	98.33	12.83
28	99.39	7.76	99.09	9.48	98.73	11.19	98.31	12.88
30	99.38	7.82	99.08	9.54	98.72	11.25	98.29	12.94
32	99.38	7.88	99.07	9.60	98.71	11.30	98.28	13.00
34	99.37	7.94	99.06	9.65	98 69	11.36	98.27	13.05
36	99.36	7.99	99.05	9.71	98.68	11.42	98.25	13.11
38	99.35	8.05	99.04	9.77	98.67	11.47	98.24	13.17
40	99.34	8.11	99.03	9.83	98.65	11.53	98.22	13.22
42	99.33	8.17	99.01	9.88	98.64	11.59	98.20	13.28
44	99.32	8.22	99.00	9.94	98.63	11.64	98.19	13.33
46	99.31	8.28	98.99	10.00	98.61	11.70	98.17	13 39
48	99.30	8.34	98.98	10.05	98.60	11.76	98.16	13.45
50	99.29	8.40	98.97	10.11	98.58	11.81	98.14	13.50
52	99.28	8.45	98.96	10.17	98.57	11.87	98.13	13.56
54	99.27	8.51	98.94	10.22	98.56	11.93	98.11	13.61
56	99.26	8.57	98.93	10.28	98.54	11.98	98.10	13.67
58	99.25	8.63	98.92	10.34	98.53	12.04	98.08	13.73
60	99.24	8.68	98.91	10.40	98.51	12.10	98.06	13.78
$c+f=$ .75	.75	.06	.75	.07	.75	.08	.74	.10
$c+f=$ 1.00	1.00	.08	.99	.09	.99	.11	.99	.13
$c+f=$ 1.25	1.25	.10	1.24	.11	1.24	.14	1.24	.16

TABLE X.

STADIA REDUCTIONS FOR READING 100.

Minutes.	8°		9°		10°		11°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.
0′	98.06	13.78	97.55	15.45	96.98	17.10	96.36	18.73
2	98.05	13.84	97.53	15.51	96.96	17.16	96.34	18.78
4	98.03	13.89	97.52	15.56	96.94	17.21	96.32	18.84
6	98.01	13.95	97.50	15.62	96.92	17.26	96.29	18.89
8	98.00	14.01	97.48	15.67	96.90	17.32	96.27	18.95
10	97.98	14.06	97.46	15.73	96.88	17.37	96.25	19.00
12	97.97	14.12	97.44	15.78	96.86	17.43	96.23	19.05
14	97.95	14.17	97.43	15.84	96.84	17.48	96.21	19.11
16	97.93	14.23	97.41	15.89	96.82	17.54	96.18	19.16
18	97.92	14.28	97.39	15.95	96.80	17.59	96.16	19.21
20	97.90	14.34	97.37	16.00	96.78	17.65	96.14	19.27
22	97.88	14.40	97.35	16.06	96.76	17.70	96.12	19.32
24	97.87	14.45	97.33	16.11	96.74	17.76	96.09	19.38
26	97.85	14.51	97.31	16.17	96.72	17.81	96.07	19.43
28	97.83	14.56	97.29	16.22	96.70	17.86	96.05	19.48
30	97.82	14.62	97.28	16.28	96.68	17.92	96.03	19.54
32	97.80	14.67	97.26	16.33	96.66	17.97	96.00	19.59
34	97.78	14.73	97.24	16.39	96.64	18.03	95.98	19.64
36	97.76	14.79	97.22	16.44	96.62	18.08	95.96	19.70
38	97.75	14.84	97.20	16.50	96.60	18.14	95.93	19.75
40	97.73	14.90	97.18	16.55	96.57	18.19	95.91	19.80
42	97.71	14.95	97.16	16.61	96.55	18.24	95.89	19.86
44	97.69	15.01	97.14	16.66	96.53	18.30	95.86	19.91
46	97.68	15.06	97.12	16.72	96.51	18.35	95.84	19.96
48	97.66	15.12	97.10	16.77	96.49	18.41	95.82	20.02
50	97.64	15.17	97.08	16.83	96.47	18.46	95.79	20.07
52	97.62	15.23	97.06	16.88	96.45	18.51	95.77	20.12
54	97.61	15.28	97.04	16.94	96.42	18.57	95.75	20.18
56	97.59	15.34	97.02	16.99	96.40	18.62	95.72	20.23
58	97.57	15.40	97.00	17.05	96.38	18.68	95.70	20.28
60	97.55	15.45	96.98	17.10	96.36	18.73	95.68	20.34
$c+f=.75$	.74	.11	.74	.12	.74	.14	.73	.15
$c+f=1.00$	.99	.15	.99	.16	.98	.18	.98	.20
$c+f=1.25$	1.23	.18	1.23	.21	1.23	.23	1.22	.25

TABLE X.

STADIA REDUCTIONS FOR READING 100.

Minutes.	12°		13°		14°		15°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.
0′	95.68	20.34	94.94	21.92	94.15	23.47	93.30	25.00
2	95.65	20.39	94.91	21.97	94.12	23.52	93.27	25.05
4	95.63	20.44	94.89	22.02	94.09	23.58	93.24	25.10
6	95.61	20.50	94.86	22.08	94.07	23.63	93.21	25.15
8	95.58	20.55	94.84	22.13	94.04	23.68	93.18	25.20
10	95.56	20.60	94.81	22.18	94.01	23.73	93.16	25.25
12	95.53	20.66	94.79	22.23	93.98	23.78	93.13	25.30
14	95.51	20.71	94.76	22.28	93.95	23.83	93.10	25.35
16	95.49	20.76	94.73	22.34	93.93	23.88	93.07	25.40
18	95.46	20.81	94.71	22.39	93.90	23.93	93.04	25.45
20	95.44	20.87	94.68	22.44	93.87	23.99	93.01	25.50
22	95.41	20.92	94.66	22.49	93.84	24.04	92.98	25.55
24	95.39	20.97	94.63	22.54	93.81	24.09	92.95	25.60
26	95.36	21.03	94.60	22.60	93.79	24.14	92.92	25.65
28	95.34	21.08	94.58	22.65	93.76	24.19	92.89	25.70
30	95.32	21.13	94.55	22.70	93.73	24.24	92.86	25.75
32	95.29	21.18	94.52	22.75	93.70	24.29	92.83	25.80
34	95.27	21.24	94.50	22.80	93.67	24.34	92.80	25.85
36	95.24	21.29	94.47	22.85	93.65	24.39	92.77	25.90
38	95.22	21.34	94.44	22.91	93.62	24.44	92.74	25.95
40	95.19	21.39	94.42	22.96	93.59	24.49	92.71	26.00
42	95.17	21.45	94.39	23.01	93.56	24.55	92.68	26.05
44	95.14	21.50	94.36	23.06	93.53	24.60	92.65	26.10
46	95.12	21.55	94.34	23.11	93.50	24.65	92.62	26.15
48	95.09	21.60	94.31	23.16	93.47	24.70	92.59	26.20
50	95.07	21.66	94.28	23.22	93.45	24.75	92.56	26.25
52	95.04	21.71	94.26	23.27	93.42	24.80	92.53	26.30
54	95.02	21.76	94.23	23.32	93.39	24.85	92.49	26.35
56	94.99	21.81	94.20	23.37	93.36	24.90	92.46	26.40
58	94.97	21.87	94.17	23.42	93.33	24.95	92.43	26.45
60	94.94	21.92	94.15	23.47	93.30	25.00	92.40	26.50
$c+f=$ .75	.73	.16	.73	.17	.73	.19	.72	.20
$c+f=$ 1.00	.98	.22	.97	.23	.97	.25	.96	.27
$c+f=$ 1.25	1.23	.27	1.21	.29	1.21	.31	1.20	.34

Table X.

STADIA REDUCTIONS FOR READING 100.

Minutes.	16°		17°		18°		19°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.
0′	92.40	26.50	91.45	27.96	90.45	29.39	89.40	30.78
2	92.37	26.55	91.42	28.01	90.42	29.44	89.36	30.83
4	92.34	26.59	91.39	28.06	90.38	29.48	89.33	30.87
6	92.31	26.64	91.35	28.10	90.35	29.53	89.29	30.92
8	92.28	26.69	91.32	28.15	90.31	29.58	89.26	30.97
10	92.25	26.74	91.29	28.20	90.28	29.62	89.22	31.01
12	92.22	26.79	91.26	28.25	90.24	29.67	89.18	31.06
14	92.19	26.84	91.22	28.30	90.21	29.72	89.15	31.10
16	92.15	26.89	91.19	28.34	90.18	29.76	89.11	31.15
18	92.12	26.94	91.16	28.39	90.14	29.81	89.08	31.19
20	92.09	26.99	91.12	28.44	90.11	29.86	89.04	31.24
22	92.06	27.04	91.09	28.49	90.07	29.90	89.00	31.28
24	92.03	27.09	91.06	28.54	90.04	29.95	88.96	31.33
26	92.00	27.13	91.02	28.58	90.00	30.00	88.93	31.38
28	91.97	27.18	90.99	28.63	89.97	30.04	88.89	31.42
30	91.93	27.23	90.96	28.68	89.93	30.09	88.86	31.47
32	91.90	27.28	90.92	28.73	89.90	30.14	88.82	31.51
34	91.87	27.33	90.89	28.77	89.86	30.19	88.78	31.56
36	91.84	27.38	90.86	28.82	89.83	30.23	88.75	31.60
38	91.81	27.43	90.82	28.87	89.79	30.28	88.71	31.65
40	91.77	27.48	90.79	28.92	89.76	30.32	88.67	31.69
42	91.74	27.52	90.76	28.96	89.72	30.37	88.64	31.74
44	91.71	27.57	90.72	29.01	89.69	30.41	88.60	31.78
46	91.68	27.62	90.69	29.06	89.65	30.46	88.56	31.83
48	91.65	27.67	90.66	29.11	89.61	30.51	88.53	31.87
50	91.61	27.72	90.62	29.15	89.58	30.55	88.49	31.92
52	91.58	27.77	90.59	29.20	89.54	30.60	88.45	31.96
54	91.55	27.81	90.55	29.25	89.51	30.65	88.41	32.01
56	91.52	27.86	90.52	29.30	89.47	30.69	88.38	32.05
58	91.48	27.91	90.48	29.34	89.44	30.74	88.34	32.09
60	91.45	27.96	90.45	29.39	89.40	30.78	88.30	32.14
$c+f=$ .75	.72	.21	.72	.23	.71	.24	.71	.25
$c+f=$ 1.00	.96	.28	.95	.30	.95	.32	.94	.33
$c+f=$ 1.25	1.20	.36	1.19	.38	1.19	.40	1.18	.42

TABLE X.

STADIA REDUCTIONS FOR READING 100.

Minutes.	20°		21°		22°		23°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.
0′	88.30	32.14	87.16	33.46	85.97	34.73	84.73	35.97
2	88.26	32.18	87.12	33.50	85.93	34.77	84.69	36.01
4	88.23	32.23	87.08	33.54	85.89	34.82	84.65	36.05
6	88.19	32.27	87.04	33.59	85.85	34.86	84.61	36.09
8	88.15	32.32	87.00	33.63	85.80	34 90	84.57	36.13
10	88.11	32.36	86.96	33.67	85.76	34.94	84.52	36.17
12	88.08	32.41	86.92	33.72	85.72	34.98	84.48	36.21
14	88.04	32.45	86.88	33.76	85.68	35.02	84.44	36.25
16	88.00	32.49	86.84	33.80	85.64	35.07	84.40	36.29
18	87.96	32.54	86.80	33.84	85.60	35.11	84.35	36.33
20	87.93	32.58	86.77	33.89	85.56	35.15	84.31	36.37
22	87.89	32.63	86.73	33.93	85.52	35.19	84.27	36.41
24	87.85	32.67	86.69	33.97	85.48	35.23	84.23	36.45
26	87.81	32.72	86.65	34.01	85.44	35.27	84.18	36.49
28	87.77	32.76	86.61	34.06	85.40	35.31	84.14	36.53
30	87.74	32.80	86.57	34.10	85.36	35 36	84.10	36.57
32	87.70	32.85	86.53	34.14	85.31	35.40	84.06	36.61
34	87.66	32.89	86.49	34.18	85.27	35.44	84.01	36.65
36	87.62	32.93	86.45	34.23	85.23	35.48	83.97	36.69
38	87.58	32.98	86.41	34.27	85.19	35.52	83.93	36.73
40	87.54	33.02	86.37	34.31	85.15	35.56	83.89	36.77
42	87.51	33.07	86.33	34.35	85.11	35.60	83.84	36.80
44	87.47	33.11	86.29	34.40	85.07	35.64	83.80	36.84
46	87.43	33.15	86.25	34.44	85.02	35.68	83.76	36.88
48	87.39	33.20	86 21	34.48	84.98	35.72	83.72	36.92
50	87.35	33.24	86.17	34.52	84.94	35.76	83.67	36.96
52	87.31	33.28	86.13	34.57	84.90	35.80	83.63	37.00
54	87.27	33.33	86.09	34.61	84.86	35.85	83.59	37.04
56	87.24	33.37	86.05	34.65	84.82	35.89	83.54	37.08
58	87.20	33.41	86.01	34.69	84.77	35.93	83.50	37.12
60	87.16	33.46	85.97	34.73	84.73	35.97	83.46	37.16
$c+f=$ .75	.70	.26	.70	.27	.69	.29	.69	.30
$c+f=$ 1.00	.94	.35	.93	.37	.92	.38	.92	.40
$c+f=$ 1.25	1.17	.44	1.16	.46	1.15	.48	1.15	.50

TABLE X.

STADIA REDUCTIONS FOR READING 100.

Minutes.	24°		25°		26°		27°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.
0′	83.46	37.16	82.14	38.30	80.78	39.40	79.39	40.45
2	83.41	37.20	82.09	38.34	80.74	39.44	79.34	40.49
4	83.37	37.23	82.05	38.38	80.69	39.47	79.30	40.52
6	83.33	37.27	82.01	38.41	80.65	39.51	79.25	40.55
8	83.28	37.31	81.96	38.45	80.60	39.54	79.20	40.59
10	83.24	37.35	81.92	38.49	80.55	39.58	79.15	40.62
12	83.20	37.39	81.87	38.53	80.51	39.61	79.11	40.66
14	83.15	37.43	81.83	38.56	80.46	39.65	79.06	40.69
16	83.11	37.47	81.78	38.60	80.41	39.69	79.01	40.72
18	83.07	37.51	81.74	38.64	80.37	39.72	78.96	40.76
20	83.02	37.54	81.69	38.67	80.32	39.76	78.92	40.79
22	82.98	37.58	81.65	38.71	80.28	39.79	78.87	40.82
24	82.93	37.62	81.60	38.75	80.23	39.83	78.82	40.86
26	82.89	37.66	81.56	38.78	80.18	39.86	78.77	40.89
28	82.85	37.70	81.51	38.82	80.14	39.90	78.73	40.92
30	82.80	37.74	81.47	38.86	80.09	39.93	78.68	40.96
32	82.76	37.77	81.42	38.89	80.04	39.97	78.63	40.99
34	82.72	37.81	81.38	38.93	80.00	40.00	78.58	41.02
36	82.67	37.85	81.33	38.97	79.95	40.04	78.54	41.06
38	82.63	37.89	81.28	39.00	79.90	40.07	78.49	41.09
40	82.58	37.93	81.24	39.04	79.86	40.11	78.44	41.12
42	82.54	37.96	81.19	39.08	79.81	40.14	78.39	41.16
44	82.49	38.00	81.15	39.11	79.76	40.18	78.34	41.19
46	82.45	38.04	81.10	39.15	79.72	40.21	78.30	41.22
48	82.41	38.08	81.06	39.18	79.67	40.24	78.25	41.26
50	82.36	38.11	81.01	39.22	79.62	40.28	78.20	41.29
52	82.32	38.15	80.97	39.26	79.58	40.31	78.15	41.32
54	82.27	38.19	80.92	39.29	79.53	40.35	78.10	41.35
56	82.23	38.23	80.87	39.33	79.48	40.38	78.06	41.39
58	82.18	38.26	80.83	39.36	79.44	40.42	78.01	41.42
60	82.14	38.30	80.78	39.40	79.39	40.45	77.96	41.45
$c+f=$ .75	.68	.31	.68	.32	.67	.33	.66	.35
$c+f=$ 1.00	.91	.41	.90	.43	.89	.45	.89	.46
$c+f=$ 1.25	1.14	.52	1.13	.54	1.12	.56	1.11	.58

TABLE XI.

LOGARITHMS OF NUMBERS

FROM

1 to 10 000

TO SIX DECIMAL PLACES.

N.	Log.	N.	Log.	N.	Log.	N.	Log.	N.	Log.
1	0.000000	21	1.322219	41	1.612784	61	1.785330	81	1.908485
2	0.301030	22	1.342423	42	1.623249	62	1.792392	82	1.913814
3	0.477121	23	1.361728	43	1.633468	63	1.799341	83	1.919078
4	0.602060	24	1.380211	44	1.643453	64	1.806180	84	1.924279
5	0.698970	25	1.397940	45	1.653213	65	1.812913	85	1.929419
6	0.778151	26	1.414973	46	1.662758	66	1.819544	86	1.934498
7	0.845098	27	1.431364	47	1.672098	67	1.826075	87	1.939519
8	0.903090	28	1.447158	48	1.681241	68	1.832509	88	1.944483
9	0.954243	29	1.462398	49	1.690196	69	1.838849	89	1.949390
10	1.000000	30	1.477121	50	1.698970	70	1.845098	90	1.954243
11	1.041393	31	1.491362	51	1.707570	71	1.851258	91	1.959041
12	1.079181	32	1.505150	52	1.716003	72	1.857332	92	1.963788
13	1.113943	33	1.518514	53	1.724276	73	1.863323	93	1.968483
14	1.146128	34	1.531479	54	1.732394	74	1.869232	94	1.973128
15	1.176091	35	1.544068	55	1.740363	75	1.875061	95	1.977724
16	1.204120	36	1.556303	56	1.748188	76	1.880814	96	1.982271
17	1.230449	37	1.568202	57	1.755875	77	1.886491	97	1.986772
18	1.255273	38	1.579784	58	1.763428	78	1.892095	98	1.991226
19	1.278754	39	1.591065	59	1.770852	79	1.897627	99	1.995635
20	1.301030	40	1.602060	60	1.778151	80	1.903090	100	2.000000

No. 100 L. 000.] [No. 109 L. 040.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
100	000000	0434	0868	1301	1734	2166	2598	3029	3461	3891	432
1	4321	4751	5181	5609	6038	6466	6894	7321	7748	8174	428
2	8600	9026	9451	9876	0300	0724	1147	1570	1993	2415	424
3	012837	3259	3680	4100	4521	4940	5360	5779	6197	6616	420
4	7033	7451	7868	8284	8700	9116	9532	9947	0361	0775	416
5	021189	1603	2016	2428	2841	3252	3664	4075	4486	4896	412
6	5306	5715	6125	6533	6942	7350	7757	8164	8571	8978	408
7	9384	9789	0195	0600	1004	1408	1812	2216	2619	3021	404
8	033424	3826	4227	4628	5029	5430	5830	6230	6629	7028	400
9	7426	7825	8223	8620	9017	9414	9811	0207	0602	0998	397
	04										

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
434	43.4	86.8	130.2	173.6	217.0	260.4	303.8	347.2	390.6
433	43.3	86.6	129.9	173.2	216.5	259.8	303.1	346.4	389.7
432	43.2	86.4	129.6	172.8	216.0	259.2	302.4	345.6	388.8
431	43.1	86.2	129.3	172.4	215.5	258.6	301.7	344.8	387.9
430	43.0	86.0	129.0	172.0	215.0	258.0	301.0	344.0	387.0
429	42.9	85.8	128.7	171.6	214.5	257.4	300.3	343.2	386.1
428	42.8	85.6	128.4	171.2	214.0	256.8	299.6	342.4	385.2
427	42.7	85.4	128.1	170.8	213.5	256.2	298.9	341.6	384.3
426	42.6	85.2	127.8	170.4	213.0	255.6	298.2	340.8	383.4
425	42.5	85.0	127.5	170.0	212.5	255.0	297.5	340.0	382.5
424	42.4	84.8	127.2	169.6	212.0	254.4	296.8	339.2	381.6
423	42.3	84.6	126.9	169.2	211.5	253.8	296.1	338.4	380.7
422	42.2	84.4	126.6	168.8	211.0	253.2	295.4	337.6	379.8
421	42.1	84.2	126.3	168.4	210.5	252.6	294.7	336.8	378.9
420	42.0	84.0	126.0	168.0	210.0	252.0	294.0	336.0	378.0
419	41.9	83.8	125.7	167.6	209.5	251.4	293.3	335.2	377.1
418	41.8	83.6	125.4	167.2	209.0	250.8	292.6	334.4	376.2
417	41.7	83.4	125.1	166.8	208.5	250.2	291.9	333.6	375.3
416	41.6	83.2	124.8	166.4	208.0	249.6	291.2	332.8	374.4
415	41.5	83.0	124.5	166.0	207.5	249.0	290.5	332.0	373.5
414	41.4	82.8	124.2	165.6	207.0	248.4	289.8	331.2	372.6
413	41.3	82.6	123.9	165.2	206.5	247.8	289.1	330.4	371.7
412	41.2	82.4	123.6	164.8	206.0	247.2	288.4	329.6	370.8
411	41.1	82.2	123.3	164.4	205.5	246.6	287.7	328.8	369.9
410	41.0	82.0	123.0	164.0	205.0	246.0	287.0	328.0	369.0
409	40.9	81.8	122.7	163.6	204.5	245.4	286.3	327.2	368.1
408	40.8	81.6	122.4	163.2	204.0	244.8	285.6	326.4	367.2
407	40.7	81.4	122.1	162.8	203.5	244.2	284.9	325.6	366.3
406	40.6	81.2	121.8	162.4	203.0	243 6	284.2	324.8	365.4
405	40.5	81.0	121.5	162.0	202.5	243.0	283.5	324.0	364.5
404	40.4	80.8	121.2	161.6	202.0	242.4	282.8	323.2	363.6
403	40.3	80.6	120.9	161.2	201.5	241.8	282.1	322.4	362.7
402	40.2	80.4	120.6	160.8	201.0	241 2	281.4	321.6	361.8
401	40.1	80.2	120.3	160.4	200.5	240.6	280.7	320.8	360.9
400	40.0	80·0	120.0	160.0	200.0	240.0	280.0	320.0	360.0
399	39.9	79.8	119.7	159.6	199.5	239.4	279.3	319.2	359.1
398	39.8	79.6	119.4	159.2	199.0	238.8	278.6	318.4	358.2
397	39.7	79.4	119.1	158.8	198.5	238.2	277.9	317.6	357.3
396	39.6	79.2	118.8	158.4	198.0	237.6	277.2	316.8	356.4
395	39.5	79.0	118.5	158.0	197.5	237.0	276.5	316.0	355.5

No. 110 L. 041.] [No. 119 L. 078.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
110	041393	1787	2182	2576	2969	3362	3755	4148	4540	4932	393
1	5323	5714	6105	6495	6885	7275	7664	8053	8442	8830	390
2	9218	9606	9993	0380	0766	1153	1538	1924	2309	2694	386
3	053078	3463	3846	4230	4613	4996	5378	5760	6142	6524	383
4	6905	7286	7666	8046	8426	8805	9185	9563	9942	0320	379
5	060698	1075	1452	1829	2206	2582	2958	3333	3709	4083	376
6	4458	4832	5206	5580	5953	6326	6699	7071	7443	7815	373
7	8186	8557	8928	9298	9668	0038	0407	0776	1145	1514	370
8	071882	2250	2617	2985	3352	3718	4085	4451	4816	5182	366
9	5547	5912	6276	6640	7004	7368	7731	8094	8457	8819	363

Proportional Parts.

Diff.	1	2	3	4	5	6	7	8	9
395	39.5	79.0	118.5	158.0	197.5	237.0	276.5	316.0	355.5
394	39.4	78.8	118.2	157.6	197.0	236.4	275.8	315.2	354.6
393	39.3	78.6	117.9	157.2	196.5	235.8	275.1	314.4	353.7
392	39.2	78.4	117.6	156.8	196.0	235.2	274.4	313.6	352.8
391	39.1	78.2	117.3	156.4	195.5	234.6	273.7	312.8	351.9
390	39.0	78.0	117.0	156.0	195.0	234.0	273.0	312.0	351.0
389	38.9	77.8	116.7	155.6	194.5	233.4	272.3	311.2	350.1
388	38.8	77.6	116.4	155.2	194.0	232.8	271.6	310.4	349.2
387	38.7	77.4	116.1	154.8	193.5	232.2	270.9	309.6	348.3
386	38.6	77.2	115.8	154.4	193.0	231.6	270.2	308.8	347.4
385	38.5	77.0	115.5	154.0	192.5	231.0	269.5	308.0	346.5
384	38.4	76.8	115.2	153.6	192.0	230.4	268.8	307.2	345.6
383	38.3	76.6	114.9	153.2	191.5	229.8	268.1	306.4	344.7
382	38.2	76.4	114.6	152.8	191.0	229.2	267.4	305.6	343.8
381	38.1	76.2	114.3	152.4	190.5	228.6	266.7	304.8	342.9
380	38.0	76.0	114.0	152.0	190.0	228.0	266.0	304.0	342.0
379	37.9	75.8	113.7	151.6	189.5	227.4	265.3	303.2	341.1
378	37.8	75.6	113.4	151.2	189.0	226.8	264.6	302.4	340.2
377	37.7	75.4	113.1	150.8	188.5	226.2	263.9	301.6	339.3
376	37.6	75.2	112.8	150.4	188.0	225.6	263.2	300.8	338.4
375	37.5	75.0	112.5	150.0	187.5	225.0	262.5	300.0	337.5
374	37.4	74.8	112.2	149.6	187.0	224.4	261.8	299.2	336.6
373	37.3	74.6	111.9	149.2	186.5	223.8	261.1	298.4	335.7
372	37.2	74.4	111.6	148.8	186.0	223.2	260.4	297.6	334.8
371	37.1	74.2	111.3	148.4	185.5	222.6	259.7	296.8	333.9
370	37.0	74.0	111.0	148.0	185.0	222.0	259.0	296.0	333.0
369	36.9	73.8	110.7	147.6	184.5	221.4	258.3	295.2	332.1
368	36.8	73.6	110.4	147.2	184.0	220.8	257.6	294.4	331.2
367	36.7	73.4	110.1	146.8	183.5	220.2	256.9	293.6	330.3
366	36.6	73.2	109.8	146.4	183.0	219.6	256.2	292.8	329.4
365	36.5	73.0	109.5	146.0	182.5	219.0	255.7	292.0	328.5
364	36.4	72.8	109.2	145.6	182.0	218.4	254.8	291.2	327.6
363	36.3	72.6	108.9	145.2	181.5	217.8	254.1	290.4	326.7
362	36.2	72.4	108.6	144.8	181.0	217.2	253.4	289.6	325.8
361	36.1	72.2	108.3	144.4	180.5	216.6	252.7	288.8	324.9
360	36.0	72.0	108.0	144.0	180.0	216.0	252.0	288.0	324.0
359	35.9	71.8	107.7	143.6	179.5	215.4	251.3	287.2	323.1
358	35.8	71.6	107.4	143.2	179.0	214.8	250.6	286.4	322.2
357	35.7	71.4	107.1	142.8	178.5	214.2	249.9	285.6	321.3
356	35.6	71.2	106.8	142.4	178.0	213.6	249.2	284.8	320.4

No. 120 L. 079.] [No. 134 L. 130.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
120	079181	9543	9904	0266	0626	0987	1347	1707	2067	2426	360
1	082785	3144	3503	3861	4219	4576	4934	5291	5647	6004	357
2	6360	6716	7071	7426	7781	8136	8490	8845	9198	9552	355
3	9905	0258	0611	0963	1315	1667	2018	2370	2721	3071	352
4	093422	3772	4122	4471	4820	5169	5518	5866	6215	6562	349
5	6910	7257	7604	7951	8298	8644	8990	9335	9681	0026	346
6	100371	0715	1059	1403	1747	2091	2434	2777	3119	3462	343
7	3804	4146	4487	4828	5169	5510	5851	6191	6531	6871	341
8	7210	7549	7888	8227	8565	8903	9241	9579	9916	0253	338
9	110590	0926	1263	1599	1934	2270	2605	2940	3275	3609	335
130	3943	4277	4611	4944	5278	5611	5943	6276	6608	6940	333
1	7271	7603	7934	8265	8595	8926	9256	9586	9915	0245	330
2	120574	0903	1231	1560	1888	2216	2544	2871	3198	3525	328
3	3852	4178	4504	4830	5156	5481	5806	6131	6456	6781	325
4	7105	7429	7753	8076	8399	8722	9045	9368	9690	0012	323
	13										

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
355	35.5	71.0	106.5	142.0	177.5	213.0	248.5	284.0	319.5
354	35.4	70.8	106.2	141.6	177.0	212.4	247.8	283.2	318.6
353	35.3	70.6	105.9	141.2	176.5	211.8	247.1	282.4	317.7
352	35.2	70.4	105.6	140.8	176.0	211.2	246.4	281.6	316.8
351	35.1	70.2	105.3	140.4	175.5	210.6	245.7	280.8	315.9
350	35.0	70.0	105.0	140.0	175.0	210.0	245.0	280.0	315.0
349	34.9	69.8	104.7	139.6	174.5	209.4	244.3	279.2	314.1
348	34.8	69.6	104.4	139.2	174.0	208.8	243.6	278.4	313.2
347	34.7	69.4	104.1	138.8	173.5	208.2	242.9	277.6	312.3
346	34.6	69.2	103.8	138.4	173.0	207.6	242.2	276.8	311.4
345	34.5	69.0	103.5	138.0	172.5	207.0	241.5	276.0	310.5
344	34.4	68.8	103.2	137.6	172.0	206.4	240.8	275.2	309.6
343	34.3	68.6	102.9	137.2	171.5	205.8	240.1	274.4	308.7
342	34.2	68.4	102.6	136.8	171.0	205.2	239.4	273.6	307.8
341	34.1	68.2	102.3	136.4	170.5	204.6	238.7	272.8	306.9
340	34.0	68.0	102.0	136.0	170.0	204.0	238.0	272.0	306.0
339	33.9	67.8	101.7	135.6	169.5	203.4	237.3	271.2	305.1
338	33.8	67.6	101.4	135.2	169.0	202.8	236.6	270.4	304.2
337	33.7	67.4	101.1	134.8	168.5	202.2	235.9	269.6	303.3
336	33.6	67.2	100.8	134.4	168.0	201.6	235.2	268.8	302.4
335	33.5	67.0	100.5	134.0	167.5	201.0	234.5	268.0	301.5
334	33.4	66.8	100.2	133.6	167.0	200.4	233.8	267.2	300.6
333	33.3	66.6	99.9	133.2	166.5	199.8	233.1	266.4	299.7
332	33.2	66.4	99.6	132.8	166.0	199.2	232.4	265.6	298.8
331	33.1	66.2	99.3	132.4	165.5	198.6	231.7	264.8	297.9
330	33.0	66.0	99.0	132.0	165.0	198.0	231.0	264.0	297.0
329	32.9	65.8	98.7	131.6	164.5	197.4	230.3	263.2	296.1
328	32.8	65.6	98.4	131.2	164.0	196.8	229.6	262.4	295.2
327	32.7	65.4	98.1	130.8	163.5	196.2	228.9	261.6	294.3
326	32.6	65.2	97.8	130.4	163.0	195.6	228.2	260.8	293.4
325	32.5	65.0	97.5	130.0	162.5	195.0	227.5	260.0	292.5
324	32.4	64.8	97.2	129.6	162.0	194.4	226.8	259.2	291.6
323	32.3	64.6	96.9	129.2	161.5	193.8	226.1	258.4	290.7
322	32.2	64.4	96.6	128.8	161.0	193.2	225.4	257.6	289.8

N.	0	1	2	3	4	5	6	7	8	9	Diff.
135	130334	0655	0977	1298	1619	1939	2260	2580	2900	3219	321
6	3539	3858	4177	4496	4814	5133	5451	5769	6086	6403	318
7	6721	7037	7354	7671	7987	8303	8618	8934	9249	9564	316
8	9879	0194	0508	0822	1136	1450	1763	2076	2389	2702	314
9	143015	3327	3639	3951	4263	4574	4885	5196	5507	5818	311
140	6128	6438	6748	7058	7367	7676	7985	8294	8603	8911	309
1	9219	9527	9835	0142	0449	0756	1063	1370	1676	1982	307
2	152288	2594	2900	3205	3510	3815	4120	4424	4728	5032	305
3	5336	5640	5943	6246	6549	6852	7154	7457	7759	8061	303
4	8362	8664	8965	9266	9567	9868	0168	0469	0769	1068	301
5	161368	1667	1967	2266	2564	2863	3161	3460	3758	4055	299
6	4353	4650	4947	5244	5541	5838	6134	6430	6726	7022	297
7	7317	7613	7908	8203	8497	8792	9086	9380	9674	9968	295
8	170262	0555	0848	1141	1434	1726	2019	2311	2603	2895	293
9	3186	3478	3769	4060	4351	4641	4932	5222	5512	5802	291

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
321	32.1	64.2	96.3	128.4	160.5	192.6	224.7	256.8	288.9
320	32.0	64.0	96.0	128.0	160.0	192.0	224.0	256.0	288.0
319	31.9	63.8	95.7	127.6	159.5	191.4	223.3	255.2	287.1
318	31.8	63.6	95.4	127.2	159.0	190.8	222.6	254.4	286.2
317	31.7	63.4	95.1	126.8	158.5	190.2	221.9	253.6	285.3
316	31.6	63.2	94.8	126.4	158.0	189.6	221.2	252.8	284.4
315	31.5	63.0	94.5	126.0	157.5	189.0	220.5	252.0	283.5
314	31.4	62.8	94.2	125.6	157.0	188.4	219.8	251.2	282.6
313	31.3	62.6	93.9	125.2	156.5	187.8	219.1	250.4	281.7
312	31.2	62.4	93.6	124.8	156.0	187.2	218.4	249.6	280.8
311	31.1	62.2	93.3	124.4	155.5	186.6	217.7	248.8	279.9
310	31.0	62.0	93.0	124.0	155.0	186.0	217.0	248.0	279.0
309	30.9	61.8	92.7	123.6	154.5	185.4	216.3	247.2	278.1
308	30.8	61.6	92.4	123.2	154.0	184.8	215.6	246.4	277.2
307	30.7	61.4	92.1	122.8	153.5	184.2	214.9	245.6	276.3
306	30.6	61.2	91.8	122.4	153.0	183.6	214.2	244.8	275.4
305	30.5	61.0	91.5	122.0	152.5	183.0	213.5	244.0	274.5
304	30.4	60.8	91.2	121.6	152.0	182.4	212.8	243.2	273.6
303	30.3	60.6	90.9	121.2	151.5	181.8	212.1	242.4	272.7
302	30.2	60.4	90.6	120.8	151.0	181.2	211.4	241.6	271.8
301	30.1	60.2	90.3	120.4	150.5	180.6	210.7	240.8	270.9
300	30.0	60.0	90.0	120.0	150.0	180.0	210.0	240.0	270.0
299	29.9	59.8	89.7	119.6	149.5	179.4	209.3	239.2	269.1
298	29.8	59.6	89.4	119.2	149.0	178.8	208.6	238.4	268.2
297	29.7	59.4	89.1	118.8	148.5	178.2	207.9	237.6	267.3
296	29.6	59.2	88.8	118.4	148.0	177.6	207.2	236.8	266.4
295	29.5	59.0	88.5	118.0	147.5	177.0	206.5	236.0	265.5
294	29.4	58.8	88.2	117.6	147.0	176.4	205.8	235.2	264.6
293	29.3	58.6	87.9	117.2	146.5	175.8	205.1	234.4	263.7
292	29.2	58.4	87.6	116.8	146.0	175.2	204.4	233.6	262.8
291	29.1	58.2	87.3	116.4	145.5	174.6	203.7	232.8	261.9
290	29.0	58.0	87.0	116.0	145.0	174.0	203.0	232.0	261.0
289	28.9	57.8	86.7	115.6	144.5	173.4	202.3	231.2	260.1
288	28.8	57.6	86.4	115.2	144.0	172.8	201.6	230.4	259.2
287	28.7	57.4	86.1	114.8	143.5	172.2	200.9	229.6	258.3
286	28.6	57.2	85.8	114.4	143.0	171.6	200.2	228.8	257.4

No. 150 L. 176.] [No. 169 L. 230.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
150	176091	6381	6670	6959	7248	7536	7825	8113	8401	8689	289
1	8977	9264	9552	9839	0126	0413	0699	0986	1272	1558	287
2	181844	2129	2415	2700	2985	3270	3555	3839	4123	4407	285
3	4691	4975	5259	5542	5825	6108	6391	6674	6956	7239	283
4	7521	7803	8084	8366	8647	8928	9209	9490	9771	0051	281
5	190332	0612	0892	1171	1451	1730	2010	2289	2567	2846	279
6	3125	3403	3681	3959	4237	4514	4792	5069	5346	5623	278
7	5900	6176	6453	6729	7005	7281	7556	7832	8107	8382	276
8	8657	8932	9206	9481	9755	0029	0303	0577	0850	1124	274
9	201397	1670	1943	2216	2488	2761	3033	3305	3577	3848	272
160	4120	4391	4663	4934	5204	5475	5746	6016	6286	6556	271
1	6826	7096	7365	7634	7904	8173	8441	8710	8979	9247	269
2	9515	9783	0051	0319	0586	0853	1121	1388	1654	1921	267
3	212188	2454	2720	2986	3252	3518	3783	4049	4314	4579	266
4	4844	5109	5373	5638	5902	6166	6430	6694	6957	7221	264
5	7484	7747	8010	8273	8536	8798	9060	9323	9585	9846	262
6	220108	0370	0631	0892	1153	1414	1675	1936	2196	2456	261
7	2716	2976	3236	3496	3755	4015	4274	4533	4792	5051	259
8	5309	5568	5826	6084	6342	6600	6858	7115	7372	7630	258
9	7887	8144	8400	8657	8913	9170	9426	9682	9938	0193	256
	23										

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
285	28.5	57.0	85.5	114.0	142.5	171.0	199.5	228.0	256.5
284	28.4	56.8	85.2	113.6	142.0	170.4	198.8	227.2	255.6
283	28.3	56.6	84.9	113.2	141.5	169.8	198.1	226.4	254.7
282	28.2	56.4	84.6	112.8	141.0	169.2	197.4	225.6	253.8
281	28.1	56.2	84.3	112.4	140.5	168.6	196.7	224.8	252.9
280	28.0	56.0	84.0	112.0	140.0	168.0	196.0	224.0	252.0
279	27.9	55.8	83.7	111.6	139.5	167.4	195.3	223.2	251.1
278	27.8	55.6	83.4	111.2	139.0	166.8	194.6	222.4	250.2
277	27.7	55.4	83.1	110.8	138.5	166.2	193.9	221.6	249.3
276	27.6	55.2	82.8	110.4	138.0	165.6	193.2	220.8	248.4
275	27.5	55.0	82.5	110.0	137.5	165.0	192.5	220.0	247.5
274	27.4	54.8	82.2	109.6	137.0	164.4	191.8	219.2	246.6
273	27.3	54.6	81.9	109.2	136.5	163.8	191.1	218.4	245.7
272	27.2	54.4	81.6	108.8	136.0	163.2	190.4	217.6	244.8
271	27.1	54.2	81.3	108.4	135.5	162.6	189.7	216.8	243.9
270	27.0	54.0	81.0	108.0	135.0	162.0	189.0	216.0	243.0
269	26.9	53.8	80.7	107.6	134.5	161.4	188.3	215.2	242.1
268	26.8	53.6	80.4	107.2	134.0	160.8	187.6	214.4	241.2
267	26.7	53.4	80.1	106.8	133.5	160.2	186.9	213.6	240.3
266	26.6	53.2	79.8	106.4	133.0	159.6	186.2	212.8	239.4
265	26.5	53.0	79.5	106.0	132.5	159.0	185.5	212.0	238.5
264	26.4	52.8	79.2	105.6	132.0	158.4	184.8	211.2	237.6
263	26.3	52.6	78.9	105.2	131.5	157.8	184.1	210.4	236.7
262	26.2	52.4	78.6	104.8	131.0	157.2	183.4	209.6	235.8
261	26.1	52.2	78.3	104.4	130.5	156.6	182.7	208.8	234.9
260	26.0	52.0	78.0	104.0	130.0	156.0	182.0	208.0	234.0
259	25.9	51.8	77.7	103.6	129.5	155.4	181.3	207.2	233.1
258	25.8	51.6	77.4	103.2	129.0	154.8	180.6	206.4	232.2
257	25.7	51.4	77.1	102.8	128.5	154.2	179.9	205.6	231.3
256	25.6	51.2	76.8	102.4	128.0	153.6	179.2	204.8	230.4
255	25.5	51.0	76.5	102.0	127.5	153.0	178.5	204.0	229.5

No. 170 L. 230.] [No. 189 L. 278.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
170	230449	0704	0960	1215	1470	1724	1979	2234	2488	2742	255
1	2996	3250	3504	3757	4011	4264	4517	4770	5023	5276	253
2	5528	5781	6033	6285	6537	6789	7041	7292	7544	7795	252
3	8046	8297	8548	8799	9049	9299	9550	9800			
									0050	0300	250
4	240549	0799	1048	1297	1546	1795	2044	2293	2541	2790	249
5	3038	3286	3534	3782	4030	4277	4525	4772	5019	5266	248
6	5513	5759	6006	6252	6499	6745	6991	7237	7482	7728	246
7	7973	8219	8464	8709	8954	9198	9443	9687	9932		
										0176	245
8	250420	0664	0908	1151	1395	1638	1881	2125	2368	2610	243
9	2853	3096	3338	3580	3822	4064	4306	4548	4790	5031	242
180	5273	5514	5755	5996	6237	6477	6718	6958	7198	7439	241
1	7679	7918	8158	8398	8637	8877	9116	9355	9594	9833	239
2	260071	0310	0548	0787	1025	1263	1501	1739	1976	2214	238
3	2451	2688	2925	3162	3399	3636	3873	4109	4346	4582	237
4	4818	5054	5290	5525	5761	5996	6232	6467	6702	6937	235
5	7172	7406	7641	7875	8110	8344	8578	8812	9046	9279	234
6	9513	9746	9980								
				0213	0446	0679	0912	1144	1377	1609	233
7	271842	2074	2306	2538	2770	3001	3233	3464	3696	3927	232
8	4158	4389	4620	4850	5081	5311	5542	5772	6002	6232	230
9	6462	6692	6921	7151	7380	7609	7838	8067	8296	8525	229

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
255	25.5	51.0	76.5	102.0	127.5	153.0	178.5	204.0	229.5
254	25.4	50.8	76.2	101.6	127.0	152.4	177.8	203.2	228.6
253	25.3	50.6	75.9	101.2	126.5	151.8	177.1	202.4	227.7
252	25.2	50.4	75.6	100.8	126.0	151.2	176.4	201.6	226.8
251	25.1	50.2	75.3	100.4	125.5	150.6	175.7	200.8	225.9
250	25 0	50.0	75.0	100.0	125.0	150.0	175.0	200.0	225.0
249	24.9	49.8	74.7	99.6	124.5	149.4	174.3	199.2	224.1
248	24.8	49.6	74.4	99.2	124.0	148.8	173.6	198.4	223.2
247	24.7	49.4	74.1	98.8	123.5	148.2	172.9	197.6	222.3
246	24.6	49.2	73.8	98.4	123.0	147.6	172.2	196.8	221.4
245	24.5	49.0	73.5	98.0	122.5	147.0	171.5	196.0	220.5
244	24.4	48.8	73.2	97.6	122.0	146.4	170.8	195.2	219.6
243	24.3	48.6	72.9	97.2	121.5	145.8	170.1	194.4	218.7
242	24.2	48.4	72.6	96.8	121.0	145.2	169.4	193.6	217.8
241	24.1	48.2	72.3	96.4	120.5	144.6	168.7	192.8	216.9
240	24.0	48.0	72.0	96.0	120.0	144.0	168.0	192.0	216.0
239	23.9	47.8	71.7	95.6	119.5	143.4	167.3	191.2	215.1
238	23.8	47.6	71.4	95.2	119.0	142.8	166.6	190.4	214.2
237	23.7	47.4	71.1	94.8	118.5	142.2	165.9	189.6	213.3
236	23.6	47.2	70.8	94.4	118.0	141.6	165.2	188.8	212.4
235	23.5	47.0	70.5	94.0	117.5	141.0	164.5	188.0	211.5
234	23.4	46.8	70.2	93.6	117.0	140.4	163.8	187.2	210.6
233	23.3	46.6	69.9	93.2	116.5	139.8	163.1	186.4	209.7
232	23.2	46.4	69.6	92.8	116.0	139.2	162.4	185.6	208.8
231	23.1	46.2	69.3	92.4	115.5	138.6	161.7	184.8	207.9
230	23.0	46.0	69.0	92.0	115.0	138.0	161.0	184.0	207.0
229	22.9	45.8	68.7	91.6	114.5	137.4	160.3	183.2	206.1
228	22.8	45.6	68.4	91.2	114.0	136.8	159.6	182.4	205.
227	22.7	45.4	68.1	90.8	113.5	136.2	158.9	181.6	204.
226	22.6	45.2	67.8	90.4	113.0	135.6	158.2	180.8	203

No. 190 L. 278.] [No. 214 L. 332.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
190	278754	8982	9211	9439	9667	9895	0123	0351	0578	0806	228
1	281033	1261	1488	1715	1942	2169	2396	2622	2849	3075	227
2	3301	3527	3753	3979	4205	4431	4656	4882	5107	5332	226
3	5557	5782	6007	6232	6456	6681	6905	7130	7354	7578	225
4	7802	8026	8249	8473	8696	8920	9143	9366	9589	9812	223
5	290035	0257	0480	0702	0925	1147	1369	1591	1813	2034	222
6	2256	2478	2699	2920	3141	3363	3584	3804	4025	4246	221
7	4466	4687	4907	5127	5347	5567	5787	6007	6226	6446	220
8	6665	6884	7104	7323	7542	7761	7979	8198	8416	8635	219
9	8853	9071	9289	9507	9725	9943	0161	0378	0595	0813	218
200	301030	1247	1464	1681	1898	2114	2331	2547	2764	2980	217
1	3196	3412	3628	3844	4059	4275	4491	4706	4921	5136	216
2	5351	5566	5781	5996	6211	6425	6639	6854	7068	7282	215
3	7496	7710	7924	8137	8351	8564	8778	8991	9204	9417	213
4	9630	9843	0056	0268	0481	0693	0906	1118	1330	1542	212
5	311754	1966	2177	2389	2600	2812	3023	3234	3445	3656	211
6	3867	4078	4289	4499	4710	4920	5130	5340	5551	5760	210
7	5970	6180	6390	6599	6809	7018	7227	7436	7646	7854	209
8	8063	8272	8481	8689	8898	9106	9314	9522	9730	9938	208
9	320146	0354	0562	0769	0977	1184	1391	1598	1805	2012	207
210	2219	2426	2633	2839	3046	3252	3458	3665	3871	4077	206
1	4282	4488	4694	4899	5105	5310	5516	5721	5926	6131	205
2	6336	6541	6745	6950	7155	7359	7563	7767	7972	8176	204
3	8380	8583	8787	8991	9194	9398	9601	9805	0008	0211	203
4	330414	0617	0819	1022	1225	1427	1630	1832	2034	2236	202

Proportional Parts.

Diff.	1	2	3	4	5	6	7	8	9
225	22.5	45.0	67.5	90.0	112.5	135.0	157.5	180.0	202.5
224	22.4	44.8	67.2	89.6	112.0	134.4	156.8	179.2	201.6
223	22.3	44.6	66.9	89.2	111.5	133.8	156.1	178.4	200.7
222	22.2	44.4	66.6	88.8	111.0	133.2	155.4	177.6	199.8
221	22.1	44.2	66.3	88.4	110.5	132.6	154.7	176.8	198.9
220	22.0	44.0	66.0	88.0	110.0	132.0	154.0	176.0	198.0
219	21.9	43.8	65.7	87.6	109.5	131.4	153.3	175.2	197.1
218	21.8	43.6	65.4	87.2	109.0	130.8	152.6	174.4	196.2
217	21.7	43.4	65.1	86.8	108.5	130.2	151.9	173.6	195.3
216	21.6	43.2	64.8	86.4	108.0	129.6	151.2	172.8	194.4
215	21.5	43.0	64.5	86.0	107.5	129.0	150.5	172.0	193.5
214	21.4	42.8	64.2	85.6	107.0	128.4	149.8	171.2	192.6
213	21.3	42.6	63.9	85.2	106.5	127.8	149.1	170.4	191.7
212	21.2	42.4	63.6	84.8	106.0	127.2	148.4	169.6	190.8
211	21.1	42.2	63.3	84.4	105.5	126.6	147.7	168.8	189.9
210	21.0	42.0	63.0	84.0	105.0	126.0	147.0	168.0	189.0
209	20.9	41.8	62.7	83.6	104.5	125.4	146.3	167.2	188.1
208	20.8	41.6	62.4	83.2	104.0	124.8	145.6	166.4	187.2
207	20.7	41.4	62.1	82.8	103.5	124.2	144.9	165.6	186.3
206	20.6	41.2	61.8	82.4	103.0	123.6	144.2	164.8	185.4
205	20.5	41.0	61.5	82.0	102.5	123.0	143.5	164.0	184.5
204	20.4	40.8	61.2	81.6	102.0	122.4	142.8	163.2	183.6
203	20.3	40.6	60.9	81.2	101.5	121.8	142.1	162.4	182.7
202	20.2	40.4	60.6	80.8	101.0	121.2	141.4	161.6	181.8

No. 215 L. 332.] [No. 239 L. 380.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
215	332438	2640	2842	3044	3246	3447	3649	3850	4051	4253	202
6	4454	4655	4856	5057	5257	5458	5658	5859	6059	6260	201
7	6460	6660	6860	7060	7260	7459	7659	7858	8058	8257	200
8	8456	8656	8855	9054	9253	9451	9650	9849			
									0047	0246	199
9	340444	0642	0841	1039	1237	1435	1632	1830	2028	2225	198
220	2423	2620	2817	3014	3212	3409	3606	3802	3999	4196	197
1	4392	4589	4785	4981	5178	5374	5570	5766	5962	6157	196
2	6353	6549	6744	6939	7135	7330	7525	7720	7915	8110	195
3	8305	8500	8694	8889	9083	9278	9472	9666	9860		
										0054	194
4	350248	0442	0636	0829	1023	1216	1410	1603	1796	1989	193
5	2183	2375	2568	2761	2954	3147	3339	3532	3724	3916	193
6	4108	4301	4493	4685	4876	5068	5260	5452	5643	5834	192
7	6026	6217	6408	6599	6790	6981	7172	7363	7554	7744	191
8	7935	8125	8316	8506	8696	8886	9076	9266	9456	9646	190
9	9835										
		0025	0215	0404	0593	0783	0972	1161	1350	1539	189
230	361728	1917	2105	2294	2482	2671	2859	3048	3236	3424	188
1	3612	3800	3988	4176	4363	4551	4739	4926	5113	5301	188
2	5488	5675	5862	6049	6236	6423	6610	6796	6983	7169	187
3	7356	7542	7729	7915	8101	8287	8473	8659	8845	9030	186
4	9216	9401	9587	9772	9958						
						0143	0328	0513	0698	0883	185
5	371068	1253	1437	1622	1806	1991	2175	2360	2544	2728	184
6	2912	3096	3280	3464	3647	3831	4015	4198	4382	4565	184
7	4748	4932	5115	5298	5481	5664	5846	6029	6212	6394	183
8	6577	6759	6942	7124	7306	7488	7670	7852	8034	8216	182
9	8398	8580	8761	8943	9124	9306	9487	9668	9849		
	38									0030	181

Proportional Parts.

Diff.	1	2	3	4	5	6	7	8	9
202	20.2	40.4	60.6	80.8	101.0	121.2	141.4	161.6	181.8
201	20.1	40.2	60.3	80.4	100.5	120.6	140.7	160.8	180.9
200	20.0	40.0	60.0	80.0	100.0	120.0	140.0	160.0	180.0
199	19.9	39.8	59.7	79.6	99.5	119.4	139.3	159.2	179.1
198	19.8	39.6	59.4	79.2	99.0	118.8	138.6	158.4	178.2
197	19.7	39.4	59.1	78.8	98.5	118.2	137.9	157.6	177.3
196	19.6	39.2	58.8	78.4	98.0	117.6	137.2	156.8	176.4
195	19.5	39.0	58.5	78.0	97.5	117.0	136.5	156.0	175.5
194	19.4	38.8	58.2	77.6	97.0	116.4	135.8	155.2	174.6
193	19.3	38.6	57.9	77.2	96.5	115.8	135.1	154.4	173.7
192	19.2	38.4	57.6	76.8	96.0	115.2	134.4	153.6	172.8
191	19.1	38.2	57.3	76.4	95.5	114.6	133.7	152.8	171.9
190	19.0	38.0	57.0	76.0	95.0	114.0	133.0	152.0	171.0
189	18.9	37.8	56.7	75.6	94.5	113.4	132.3	151.2	170.1
188	18.8	37.6	56.4	75.2	94.0	112.8	131.6	150.4	169.2
187	18.7	37.4	56.1	74.8	93.5	112.2	130.9	149.6	168.3
186	18.6	37.2	55.8	74.4	93.0	111.6	130.2	148.8	167.4
185	18.5	37.0	55.5	74.0	92.5	111.0	129.5	148.0	166.5
184	18.4	36.8	55.2	73.6	92.0	110.4	128.8	147.2	165.6
183	18.3	36.6	54.9	73.2	91.5	109.8	128.1	146.4	164.7
182	18.2	36.4	54.6	72.8	91.0	109.2	127.4	145.6	163.8
181	18.1	36.2	54.3	72.4	90.5	108.6	126.7	144.8	162.9
180	18.0	36.0	54.0	72.0	90.0	108.0	126.0	144.0	162.0
179	17.9	35.8	53.7	71.6	89.5	107.4	125.3	143.2	161.1

No. 240 L. 380.] [No. 269 L. 431.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
240	380211	0392	0573	0754	0934	1115	1296	1476	1656	1837	181
1	2017	2197	2377	2557	2737	2917	3097	3277	3456	3636	180
2	3815	3995	4174	4353	4533	4712	4891	5070	5249	5428	179
3	5606	5785	5964	6142	6321	6499	6677	6856	7034	7212	178
4	7390	7568	7746	7924	8101	8279	8456	8634	8811	8989	178
5	9166	9343	9520	9698	9875						
						0051	0228	0405	0582	0759	177
6	390935	1112	1288	1464	1641	1817	1993	2169	2345	2521	176
7	2697	2873	3048	3224	3400	3575	3751	3926	4101	4277	176
8	4452	4627	4802	4977	5152	5326	5501	5676	5850	6025	175
9	6199	6374	6548	6722	6896	7071	7245	7419	7592	7766	174
250	7940	8114	8287	8461	8634	8808	8981	9154	9328	9501	173
1	9674	9847									
			0020	0192	0365	0538	0711	0883	1056	1228	173
2	401401	1573	1745	1917	2089	2261	2433	2605	2777	2949	172
3	3121	3292	3464	3635	.3807	3978	4149	4320	4492	4663	171
4	4834	5005	5176	5346	5517	5688	5858	6029	6199	6370	171
5	6540	6710	6881	7051	7221	7391	7561	7731	7901	8070	170
6	8240	8410	8579	8749	8918	9087	9257	9426	9595	9764	169
7	9933										
		0102	0271	0440	0609	0777	0946	1114	1283	1451	169
8	411620	1788	1956	2124	2293	2461	2629	2796	2964	3132	168
9	3300	3467	3635	3803	3970	4137	4305	4472	4639	4806	167
260	4973	5140	5307	5474	5641	5808	5974	6141	6308	6474	167
1	6641	6807	6973	7139	7306	7472	7638	7804	7970	8135	166
2	8301	8467	8633	8798	8964	9129	9295	9460	9625	9791	165
3	9956										
		0121	0286	0451	0616	0781	0945	1110	1275	1439	165
4	421604	1768	1933	2097	2261	2426	2590	2754	2918	3082	164
5	3246	3410	3574	3737	3901	4065	4228	4392	4555	4718	164
6	4882	5045	5208	5371	5534	5697	5860	6023	6186	6349	163
7	6511	6674	6836	6999	7161	7324	7486	7648	7811	7973	162
8	8135	8297	8459	8621	8783	8944	9106	9268	9429	9591	162
9	9752	9914									
	43		0075	0236	0398	0559	0720	0881	1042	1203	161

Proportional Parts.

Diff.	1	2	3	4	5	6	7	8	9
178	17.8	35.6	53.4	71.2	89.0	106.8	124.6	142.4	160.2
177	17.7	35.4	53.1	70.8	88.5	106.2	123.9	141.6	159.3
176	17.6	35.2	52.8	70.4	88.0	105.6	123.2	140.8	158.4
175	17.5	35.0	52.5	70.0	87.5	105.0	122.5	140.0	157.5
174	17.4	34.8	52.2	69.6	87.0	104.4	121.8	139.2	156.6
173	17.3	34.6	51.9	69.2	86.5	103.8	121.1	138.4	155.7
172	17.2	34.4	51.6	68.8	86.0	103.2	120.4	137.6	154.8
171	17.1	34.2	51.3	68.4	85.5	102.6	119.7	136.8	153.9
170	17.0	34.0	51.0	68.0	85.0	102.0	119.0	136.0	153.0
169	16.9	33.8	50.7	67.6	84.5	101.4	118.3	135.2	152.1
168	16.8	33.6	50.4	67.2	84.0	100.8	117.6	134.4	151.2
167	16.7	33.4	50.1	66.8	83.5	100.2	116.9	133.6	150.3
166	16.6	33.2	49.8	66.4	83.0	99.6	116.2	132.8	149.4
165	16.5	33.0	49.5	66.0	82.5	99.0	115.5	132.0	148.5
164	16.4	32.8	49.2	65.6	82.0	98.4	114.8	131.2	147.6
163	16.3	32.6	48.9	65.2	81.5	97.8	114.1	130.4	146.7
162	16.2	32.4	48.5	64.8	81.0	97.2	113.4	129.6	145.8
161	16.1	32.2	48.3	64.4	80.5	96.6	112.7	128.8	144.9

No. 270 L 431.] [No. 299 L. 476.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
270	431364	1525	1685	1846	2007	2167	2328	2488	2649	2809	161
1	2969	3130	3290	3450	3610	3770	3930	4090	4249	4409	160
2	4569	4729	4888	5048	5207	5367	5526	5685	5844	6004	159
3	6163	6322	6481	6640	6799	6957	7116	7275	7433	7592	159
4	7751	7909	8067	8226	8384	8542	8701	8859	9017	9175	158
5	9333	9491	9648	9806	9964	0122	0279	0437	0594	0752	158
6	440909	1066	1224	1381	1538	1695	1852	2009	2166	2323	157
7	2480	2637	2793	2950	3106	3263	3419	3576	3732	3889	157
8	4045	4201	4357	4513	4669	4825	4981	5137	5293	5449	156
9	5604	5760	5915	6071	6226	6382	6537	6692	6848	7003	155
280	7158	7313	7468	7623	7778	7933	8088	8242	8397	8552	155
1	8706	8861	9015	9170	9324	9478	9633	9787	9941	0095	154
2	450249	0403	0557	0711	0865	1018	1172	1326	1479	1633	154
3	1786	1940	2093	2247	2400	2553	2706	2859	3012	3165	153
4	3318	3471	3624	3777	3930	4082	4235	4387	4540	4692	153
5	4845	4997	5150	5302	5454	5606	5758	5910	6062	6214	152
6	6366	6518	6670	6821	6973	7125	7276	7428	7579	7731	152
7	7882	8033	8184	8336	8487	8638	8789	8940	9091	9242	151
8	9392	9543	9694	9845	9995	0146	0296	0447	0597	0748	151
9	460898	1048	1198	1348	1499	1649	1799	1948	2098	2248	150
290	2398	2548	2697	2847	2997	3146	3296	3445	3594	3744	150
1	3893	4042	4191	4340	4490	4639	4788	4936	5085	5234	149
2	5383	5532	5680	5829	5977	6126	6274	6423	6571	6719	149
3	6868	7016	7164	7312	7460	7608	7756	7904	8052	8200	148
4	8347	8495	8643	8790	8938	9085	9233	9380	9527	9675	148
5	9822	9969	0116	0263	0410	0557	0704	0851	0998	1145	147
6	471292	1438	1585	1732	1878	2025	2171	2318	2464	2610	146
7	2756	2903	3049	3195	3341	3487	3633	3779	3925	4071	146
8	4216	4362	4508	4653	4799	4944	5090	5235	5381	5526	146
9	5671	5816	5962	6107	6252	6397	6542	6687	6832	6976	145

Proportional Parts.

Diff.	1	2	3	4	5	6	7	8	9
161	16.1	32.2	48.3	64.4	80.5	96.6	112.7	128.8	144.9
160	16.0	32.0	48.0	64.0	80.0	96.0	112.0	128.0	144.0
159	15.9	31.8	47.7	63.6	79.5	95.4	111.3	127.2	143.1
158	15.8	31.6	47.4	63.2	79.0	94.8	110.6	126.4	142.2
157	15.7	31.4	47.1	62.8	78.5	94.2	109.9	125.6	141.3
156	15.6	31.2	46.8	62.4	78.0	93.6	109.2	124.8	140.4
155	15.5	31.0	46.5	62.0	77.5	93.0	108.5	124.0	139.5
154	15.4	30.8	46.2	61.6	77.0	92.4	107.8	123.2	138.6
153	15.3	30.6	45.9	61.2	76.5	91.8	107.1	122.4	137.7
152	15.2	30.4	45.6	60.8	76.0	91.2	106.4	121.6	136.8
151	15.1	30.2	45.3	60.4	75.5	90.6	105.7	120.8	135.9
150	15.0	30.0	45.0	60.0	75.0	90.0	105.0	120.0	135.0
149	14.9	29.8	44.7	59.6	74.5	89.4	104.3	119.2	134.1
148	14.8	29.6	44.4	59.2	74.0	88.8	103.6	118.4	133.2
147	14.7	29.4	44.1	58.8	73.5	88.2	102.9	117.6	132.3
146	14.6	29.2	43.8	58.4	73.0	87.6	102.2	116.8	131.4
145	14.5	29.0	43.5	58.0	72.5	87.0	101.5	116.0	130.5
144	14.4	28.8	43.2	57.6	72.0	86.4	100.8	115.2	129.6
143	14.3	28.6	42.9	57.2	71.5	85.8	100.1	114.4	128.7
142	14.2	28.4	42.6	56.8	71.0	85.2	99.4	113.6	127.8
141	14.1	28.2	42.3	56.4	70.5	84.6	98.7	112.8	126.9
140	14.0	28.0	42.0	56.0	70.0	84.0	98.0	112.0	126.0

N.	0	1	2	3	4	5	6	7	8	9	Diff.
300	477121	7266	7411	7555	7700	7844	7989	8133	8278	8422	145
1	8566	8711	8855	8999	9143	9287	9431	9575	9719	9863	144
2	480007	0151	0294	0438	0582	0725	0869	1012	1156	1299	144
3	1443	1586	1729	1872	2016	2159	2302	2445	2588	2731	143
4	2874	3016	3159	3302	3445	3587	3730	3872	4015	4157	143
5	4300	4442	4585	4727	4869	5011	5153	5295	5437	5579	142
6	5721	5863	6005	6147	6289	6430	6572	6714	6855	6997	142
7	7138	7280	7421	7563	7704	7845	7986	8127	8269	8410	141
8	8551	8692	8833	8974	9114	9255	9396	9537	9677	9818	141
9	9958	0099	0239	0380	0520	0661	0801	0941	1081	1222	140
310	491362	1502	1642	1782	1922	2062	2201	2341	2481	2621	140
1	2760	2900	3040	3179	3319	3458	3597	3737	3876	4015	139
2	4155	4294	4433	4572	4711	4850	4989	5128	5267	5406	139
3	5544	5683	5822	5960	6099	6238	6376	6515	6653	6791	139
4	6930	7068	7206	7344	7483	7621	7759	7897	8035	8173	138
5	8311	8448	8586	8724	8862	8999	9137	9275	9412	9550	138
6	9687	9824	9962	0099	0236	0374	0511	0648	0785	0922	137
7	501059	1196	1333	1470	1607	1744	1880	2017	2154	2291	137
8	2427	2564	2700	2837	2973	3109	3246	3382	3518	3655	136
9	3791	3927	4063	4199	4335	4471	4607	4743	4878	5014	136
320	5150	5286	5421	5557	5693	5828	5964	6099	6234	6370	136
1	6505	6640	6776	6911	7046	7181	7316	7451	7586	7721	135
2	7856	7991	8126	8260	8395	8530	8664	8799	8934	9068	135
3	9203	9337	9471	9606	9740	9874	0009	0143	0277	0411	134
4	510545	0679	0813	0947	1081	1215	1349	1482	1616	1750	134
5	1883	2017	2151	2284	2418	2551	2684	2818	2951	3084	133
6	3218	3351	3484	3617	3750	3883	4016	4149	4282	4415	133
7	4548	4681	4813	4946	5079	5211	5344	5476	5609	5741	133
8	5874	6006	6139	6271	6403	6535	6668	6800	6932	7064	132
9	7196	7328	7460	7592	7724	7855	7987	8119	8251	8382	132
330	8514	8646	8777	8909	9040	9171	9303	9434	9566	9697	131
1	9828	9959	0090	0221	0353	0484	0615	0745	0876	1007	131
2	521138	1269	1400	1530	1661	1792	1922	2053	2183	2314	131
3	2444	2575	2705	2835	2966	3096	3226	3356	3486	3616	130
4	3746	3876	4006	4136	4266	4396	4526	4656	4785	4915	130
5	5045	5174	5304	5434	5563	5693	5822	5951	6081	6210	129
6	6339	6469	6598	6727	6856	6985	7114	7243	7372	7501	129
7	7630	7759	7888	8016	8145	8274	8402	8531	8660	8788	129
8	8917	9045	9174	9302	9430	9559	9687	9815	9943	0072	128
9	530200	0328	0456	0584	0712	0840	0968	1096	1223	1351	128

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
139	13.9	27.8	41.7	55.6	69.5	83.4	97.3	111.2	125.1
138	13.8	27.6	41.4	55.2	69.0	82.8	96.6	110.4	124.2
137	13.7	27.4	41.1	54.8	68.5	82.2	95.9	109.6	123.3
136	13.6	27.2	40.8	54.4	68.0	81.6	95.2	108.8	122.4
135	13.5	27.0	40.5	54.0	67.5	81.0	94.5	108.0	121.5
134	13.4	26.8	40.2	53.6	67.0	80.4	93.8	107.2	120.6
133	13.3	26.6	39.9	53.2	66.5	79.8	93.1	106.4	119.7
132	13.2	26.4	39.6	52.8	66.0	79.2	92.4	105.6	118.8
131	13.1	26.2	39.3	52.4	65.5	78.6	91.7	104.8	117.9
130	13.0	26.0	39.0	52.0	65.0	78.0	91.0	104.0	117.0
129	12.9	25.8	38.7	51.6	64.5	77.4	90.3	103.2	116.1
128	12.8	25.6	38.4	51.2	64.0	76.8	89.6	102.4	115.2
127	12.7	25.4	38.1	50.8	63.5	76.2	88.9	101.6	114.3

No. 340 L. 531.] [No. 379 L. 579.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
340	531479	1607	1734	1862	1990	2117	2245	2372	2500	2627	128
1	2754	2882	3009	3136	3264	3391	3518	3645	3772	3899	127
2	4026	4153	4280	4407	4534	4661	4787	4914	5041	5167	127
3	5294	5421	5547	5674	5800	5927	6053	6180	6306	6432	126
4	6558	6685	6811	6937	7063	7189	7315	7441	7567	7693	126
5	7819	7945	8071	8197	8322	8448	8574	8699	8825	8951	126
6	9076	9202	9327	9452	9578	9703	9829	9954	0079	0204	125
7	540329	0455	0580	0705	0830	0955	1080	1205	1330	1454	125
8	1579	1704	1829	1953	2078	2203	2327	2452	2576	2701	125
9	2825	2950	3074	3199	3323	3447	3571	3696	3820	3944	124
350	4068	4192	4316	4440	4564	4688	4812	4936	5060	5183	124
1	5307	5431	5555	5678	5802	5925	6049	6172	6296	6419	124
2	6543	6666	6789	6913	7036	7159	7282	7405	7529	7652	123
3	7775	7898	8021	8144	8267	8389	8512	8635	8758	8881	123
4	9003	9126	9249	9371	9494	9616	9739	9861	9984	0106	123
5	550228	0351	0473	0595	0717	0840	0962	1084	1206	1328	122
6	1450	1572	1694	1816	1938	2060	2181	2303	2425	2547	122
7	2668	2790	2911	3033	3155	3276	3398	3519	3640	3762	121
8	3883	4004	4126	4247	4368	4489	4610	4731	4852	4973	121
9	5094	5215	5336	5457	5578	5699	5820	5940	6061	6182	121
360	6303	6423	6544	6664	6785	6905	7026	7146	7267	7387	120
1	7507	7627	7748	7868	7988	8108	8228	8349	8469	8589	120
2	8709	8829	8948	9068	9188	9308	9428	9548	9667	9787	120
3	9907	0026	0146	0265	0385	0504	0624	0743	0863	0982	119
4	561101	1221	1340	1459	1578	1698	1817	1936	2055	2174	119
5	2293	2412	2531	2650	2769	2887	3006	3125	3244	3362	119
6	3481	3600	3718	3837	3955	4074	4192	4311	4429	4548	119
7	4666	4784	4903	5021	5139	5257	5376	5494	5612	5730	118
8	5848	5966	6084	6202	6320	6437	6555	6673	6791	6909	118
9	7026	7144	7262	7379	7497	7614	7732	7849	7967	8084	118
370	8202	8319	8436	8554	8671	8788	8905	9023	9140	9257	117
1	9374	9491	9608	9725	9842	9959	0076	0193	0309	0426	117
2	570543	0660	0776	0893	1010	1126	1243	1359	1476	1592	117
3	1709	1825	1942	2058	2174	2291	2407	2523	2639	2755	116
4	2872	2988	3104	3220	3336	3452	3568	3684	3800	3915	116
5	4031	4147	4263	4379	4494	4610	4726	4841	4957	5072	116
6	5188	5303	5419	5534	5650	5765	5880	5996	6111	6226	115
7	6341	6457	6572	6687	6802	6917	7032	7147	7262	7377	115
8	7492	7607	7722	7836	7951	8066	8181	8295	8410	8525	115
9	8639	8754	8868	8983	9097	9212	9326	9441	9555	9669	114

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
128	12.8	25.6	38.4	51.2	64.0	76.8	89.6	102.4	115.2
127	12.7	25.4	38.1	50.8	63.5	76.2	88.9	101.6	114.3
126	12.6	25.2	37.8	50.4	63.0	75.6	88.2	100.8	113.4
125	12.5	25.0	37.5	50.0	62.5	75.0	87.5	100.0	112.5
124	12.4	24.8	37.2	49.6	62.0	74.4	86.8	99.2	111.6
123	12.3	24.6	36.9	49.2	61.5	73.8	86.1	98.4	110.7
122	12.2	24.4	36.6	48.8	61.0	73.2	85.4	97.6	109.8
121	12.1	24.2	36.3	48.4	60.5	72.6	84.7	96.8	108.9
120	12.0	24.0	36.0	48.0	60.0	72.0	84.0	96.0	108.0
119	11.9	23.8	35.7	47.6	59.5	71.4	83.3	95.2	107.1

No. 380. L. 579.] [No. 414 L. 617.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
380	579784	9898	0012	0126	0241	0355	0469	0583	0697	0811	114
1	580925	1039	1153	1267	1381	1495	1608	1722	1836	1950	
2	2063	2177	2291	2404	2518	2631	2745	2858	2972	3085	
3	3199	3312	3426	3539	3652	3765	3879	3992	4105	4218	
4	4331	4444	4557	4670	4783	4896	5009	5122	5235	5348	113
5	5461	5574	5686	5799	5912	6024	6137	6250	6362	6475	
6	6587	6700	6812	6925	7037	7149	7262	7374	7486	7599	
7	7711	7823	7935	8047	8160	8272	8384	8496	8608	8720	112
8	8832	8944	9056	9167	9279	9391	9503	9615	9726	9838	
9	9950	0061	0173	0284	0396	0507	0619	0730	0842	0953	
390	591065	1176	1287	1399	1510	1621	1732	1843	1955	2066	
1	2177	2288	2399	2510	2621	2732	2843	2954	3064	3175	111
2	3286	3397	3508	3618	3729	3840	3950	4061	4171	4282	
3	4393	4503	4614	4724	4834	4945	5055	5165	5276	5386	
4	5496	5606	5717	5827	5937	6047	6157	6267	6377	6487	
5	6597	6707	6817	6927	7037	7146	7256	7366	7476	7586	110
6	7695	7805	7914	8024	8134	8243	8353	8462	8572	8681	
7	8791	8900	9009	9119	9228	9337	9446	9556	9665	9774	
8	9883	9992	0101	0210	0319	0428	0537	0646	0755	0864	109
9	600973	1082	1191	1299	1408	1517	1625	1734	1843	1951	
400	2060	2169	2277	2386	2494	2603	2711	2819	2928	3036	
1	3144	3253	3361	3469	3577	3686	3794	3902	4010	4118	108
2	4226	4334	4442	4550	4658	4766	4874	4982	5089	5197	
3	5305	5413	5521	5628	5736	5844	5951	6059	6166	6274	
4	6381	6489	6596	6704	6811	6919	7026	7133	7241	7348	
5	7455	7562	7669	7777	7884	7991	8098	8205	8312	8419	107
6	8526	8633	8740	8847	8954	9061	9167	9274	9381	9488	
7	9594	9701	9808	9914	0021	0128	0234	0341	0447	0554	
8	610660	0767	0873	0979	1086	1192	1298	1405	1511	1617	
9	1723	1829	1936	2042	2148	2254	2360	2466	2572	2678	106
410	2784	2890	2996	3102	3207	3313	3419	3525	3630	3736	
1	3842	3947	4053	4159	4264	4370	4475	4581	4686	4792	
2	4897	5003	5108	5213	5319	5424	5529	5634	5740	5845	
3	5950	6055	6160	6265	6370	6476	6581	6686	6790	6895	105
4	7000	7105	7210	7315	7420	7525	7629	7734	7839	7943	

Proportional Parts.

Diff.	1	2	3	4	5	6	7	8	9
118	11.8	23.6	35.4	47.2	59.0	70.8	82.6	94.4	106.2
117	11.7	23.4	35.1	46.8	58.5	70.2	81.9	93.6	105.3
116	11.6	23.2	34.8	46.4	58.0	69.6	81.2	92.8	104.4
115	11.5	23.0	34.5	46.0	57.5	69.0	80.5	92.0	103.5
114	11.4	22.8	34.2	45.6	57.0	68.4	79.8	91.2	102.6
113	11.3	22.6	33.9	45.2	56.5	67.8	79.1	90.4	101.7
112	11.2	22.4	33.6	44.8	56.0	67.2	78.4	89.6	100.8
111	11.1	22.2	33.3	44.4	55.5	66.6	77.7	88.8	99.9
110	11.0	22.0	33.0	44.0	55.0	66.0	77.0	88.0	99.0
109	10.9	21.8	32.7	43.6	54.5	65.4	76.3	87.2	98.1
108	10.8	21.6	32.4	43.2	54.0	64.8	75.6	86.4	97.2
107	10.7	21.4	32.1	42.8	53.5	64.2	74.9	85.6	96.3
106	10.6	21.2	31.8	42.4	53.0	63.6	74.2	84.8	95.4
105	10.5	21.0	31.5	42.0	52.5	63.0	73.5	84.0	94.5
105	10.5	21.0	31.5	42.0	52.5	63.0	73.5	84.0	94.5
104	10.4	20.8	31.2	41.6	52.0	62.4	72.8	83.2	93.6

No. 415 L. 618.] [No. 459 L. 662.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
415	618048	8153	8257	8362	8466	8571	8676	8780	8884	8989	105
6	9093	9198	9302	9406	9511	9615	9719	9824	9928	0032	
7	620136	0240	0344	0448	0552	0656	0760	0864	0968	1072	104
8	1176	1280	1384	1488	1592	1695	1799	1903	2007	2110	
9	2214	2318	2421	2525	2628	2732	2835	2939	3042	3146	
420	3249	3353	3456	3559	3663	3766	3869	3973	4076	4179	
1	4282	4385	4488	4591	4695	4798	4901	5004	5107	5210	103
2	5312	5415	5518	5621	5724	5827	5929	6032	6135	6238	
3	6340	6443	6546	6648	6751	6853	6956	7058	7161	7263	
4	7366	7468	7571	7673	7775	7878	7980	8082	8185	8287	
5	8389	8491	8593	8695	8797	8900	9002	9104	9206	9308	102
6	9410	9512	9613	9715	9817	9919	0021	0123	0224	0326	
7	630428	0530	0631	0733	0835	0936	1038	1139	1241	1342	
8	1444	1545	1647	1748	1849	1951	2052	2153	2255	2356	
9	2457	2559	2660	2761	2862	2963	3064	3165	3266	3367	
430	3468	3569	3670	3771	3872	3973	4074	4175	4276	4376	101
1	4477	4578	4679	4779	4880	4981	5081	5182	5283	5383	
2	5484	5584	5685	5785	5886	5986	6087	6187	6287	6388	
3	6488	6588	6688	6789	6889	6989	7089	7189	7290	7390	
4	7490	7590	7690	7790	7890	7990	8090	8190	8290	8389	100
5	8489	8589	8689	8789	8888	8988	9088	9188	9287	9387	
6	9486	9586	9686	9785	9885	9984	0084	0183	0283	0382	
7	640481	0581	0680	0779	0879	0978	1077	1177	1276	1375	
8	1474	1573	1672	1771	1871	1970	2069	2168	2267	2366	
9	2465	2563	2662	2761	2860	2959	3058	3156	3255	3354	99
440	3453	3551	3650	3749	3847	3946	4044	4143	4242	4340	
1	4439	4537	4636	4734	4832	4931	5029	5127	5226	5324	
2	5422	5521	5619	5717	5815	5913	6011	6110	6208	6306	
3	6404	6502	6600	6698	6796	6894	6992	7089	7187	7285	98
4	7383	7481	7579	7676	7774	7872	7969	8067	8165	8262	
5	8360	8458	8555	8653	8750	8848	8945	9043	9140	9237	
6	9335	9432	9530	9627	9724	9821	9919	0016	0113	0210	
7	650308	0405	0502	0599	0696	0793	0890	0987	1084	1181	
8	1278	1375	1472	1569	1666	1762	1859	1956	2053	2150	97
9	2246	2343	2440	2536	2633	2730	2826	2923	3019	3116	
450	3213	3309	3405	3502	3598	3695	3791	3888	3984	4080	
1	4177	4273	4369	4465	4562	4658	4754	4850	4946	5042	
2	5138	5235	5331	5427	5523	5619	5715	5810	5906	6002	96
3	6098	6194	6290	6386	6482	6577	6673	6769	6864	6960	
4	7056	7152	7247	7343	7438	7534	7629	7725	7820	7916	
5	8011	8107	8202	8298	8393	8488	8584	8679	8774	8870	
6	8965	9060	9155	9250	9346	9441	9536	9631	9726	9821	
7	9916	0011	0106	0201	0296	0391	0486	0581	0676	0771	95
8	660865	0960	1055	1150	1245	1339	1434	1529	1623	1718	
9	1813	1907	2002	2096	2191	2286	2380	2475	2569	2663	

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
105	10.5	21.0	31.5	42.0	52.5	63.0	73.5	84.0	94.5
104	10.4	20.8	31.2	41.6	52.0	62.4	72.8	83.2	93.6
103	10.3	20.6	30.9	41.2	51.5	61.8	72.1	82.4	92.7
102	10.2	20.4	30.6	40.8	51.0	61.2	71.4	81.6	91.8
101	10.1	20.2	30.3	40.4	50.5	60.6	70.7	80.8	90.9
100	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0
99	9.9	19.8	29.7	39.6	49.5	59.4	69.3	79.2	89.1

No. 460 L. 662.] [No. 499 L. 698.

N	0	1	2	3	4	5	6	7	8	9	Diff.
460	662758	2852	2947	3041	3135	3230	3324	3418	3512	3607	
1	3701	3795	3889	3983	4078	4172	4266	4360	4454	4548	
2	4642	4736	4830	4924	5018	5112	5206	5299	5393	5487	94
3	5581	5675	5769	5862	5956	6050	6143	6237	6331	6424	
4	6518	6612	6705	6799	6892	6986	7079	7173	7266	7360	
5	7453	7546	7640	7733	7826	7920	8013	8106	8199	8293	
6	8386	8479	8572	8665	8759	8852	8945	9038	9131	9224	
7	9317	9410	9503	9596	9689	9782	9875	9967			
									0060	0153	93
8	670246	0339	0431	0524	0617	0710	0802	0895	0988	1080	
9	1173	1265	1358	1451	1543	1636	1728	1821	1913	2005	
470	2098	2190	2283	2375	2467	2560	2652	2744	2836	2929	
1	3021	3113	3205	3297	3390	3482	3574	3666	3758	3850	
2	3942	4034	4126	4218	4310	4402	4494	4586	4677	4769	92
3	4861	4953	5045	5137	5228	5320	5412	5503	5595	5687	
4	5778	5870	5962	6053	6145	6236	6328	6419	6511	6602	
5	6694	6785	6876	6968	7059	7151	7242	7333	7424	7516	
6	7607	7698	7789	7881	7972	8063	8154	8245	8336	8427	
7	8518	8609	8700	8791	8882	8973	9064	9155	9246	9337	91
8	9428	9519	9610	9700	9791	9882	9973				
								0063	0154	0245	
9	680336	0426	0517	0607	0698	0789	0879	0970	1060	1151	
480	1241	1332	1422	1513	1603	1693	1784	1874	1964	2055	
1	2145	2235	2326	2416	2506	2596	2686	2777	2867	2957	
2	3047	3137	3227	3317	3407	3497	3587	3677	3767	3857	90
3	3947	4037	4127	4217	4307	4396	4486	4576	4666	4756	
4	4845	4935	5025	5114	5204	5294	5383	5473	5563	5652	
5	5742	5831	5921	6010	6100	6189	6279	6368	6458	6547	
6	6636	6726	6815	6904	6994	7083	7172	7261	7351	7440	
7	7529	7618	7707	7796	7886	7975	8064	8153	8242	8331	89
8	8420	8509	8598	8687	8776	8865	8953	9042	9131	9220	
9	9309	9398	9486	9575	9664	9753	9841	9930			
									0019	0107	
490	690196	0285	0373	0462	0550	0639	0728	0816	0905	0993	
1	1081	1170	1258	1347	1435	1524	1612	1700	1789	1877	
2	1965	2053	2142	2230	2318	2406	2494	2583	2671	2759	
3	2847	2935	3023	3111	3199	3287	3375	3463	3551	3639	88
4	3727	3815	3903	3991	4078	4166	4254	4342	4430	4517	
5	4605	4693	4781	4868	4956	5044	5131	5219	5307	5394	
6	5482	5569	5657	5744	5832	5919	6007	6094	6182	6269	
7	6356	6444	6531	6618	6706	6793	6880	6968	7055	7142	
8	7229	7317	7404	7491	7578	7665	7752	7839	7926	8014	
9	8100	8188	8275	8362	8449	8535	8622	8709	8796	8883	87

Proportional Parts.

Diff.	1	2	3	4	5	6	7	8	9
98	9.8	19.6	29.4	39.2	49.0	58.8	68.6	78.4	88.2
97	9.7	19.4	29.1	38.8	48.5	58.2	67.9	77.6	87.3
96	9.6	19.2	28.8	38.4	48.0	57.6	67.2	76.8	86.4
95	9.5	19.0	28.5	38.0	47.5	57.0	66.5	76.0	85.5
94	9.4	18.8	28.2	37.6	47.0	56.4	65.8	75.2	84.6
93	9.3	18.6	27.9	37.2	46.5	55.8	65.1	74.4	83.7
92	9.2	18.4	27.6	36.8	46.0	55.2	64.4	73.6	82.8
91	9.1	18.2	27.3	36.4	45.5	54.6	63.7	72.8	81.9
90	9.0	18.0	27.0	36.0	45.0	54.0	63.0	72.0	81.0
89	8.9	17.8	26.7	35.6	44.5	53.4	62.3	71.2	80.1
88	8.8	17.6	26.4	35.2	44.0	52.8	61.6	70.4	79.2
87	8.7	17.4	26.1	34.8	43.5	52.2	60.9	69.6	78.3
86	8.6	17.2	25.8	34.4	43.0	51.6	60.2	68.8	77.4

No. 500 L. 698.] [No. 544 L. 736.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
500	698970	9057	9144	9231	9317	9404	9491	9578	9664	9751	
1	9838	9924									
			0011	0098	0184	0271	0358	0444	0531	0617	
2	700704	0790	0877	0963	1050	1136	1222	1309	1395	1482	
3	1568	1654	1741	1827	1913	1999	2086	2172	2258	2344	
4	2431	2517	2603	2689	2775	2861	2947	3033	3119	3205	
5	3291	3377	3463	3549	3635	3721	3807	3893	3979	4065	86
6	4151	4236	4322	4408	4494	4579	4665	4751	4837	4922	
7	5008	5094	5179	5265	5350	5436	5522	5607	5693	5778	
8	5864	5949	6035	6120	6206	6291	6376	6462	6547	6632	
9	6718	6803	6888	6974	7059	7144	7229	7315	7400	7485	
510	7570	7655	7740	7826	7911	7996	8081	8166	8251	8336	85
1	8421	8506	8591	8676	8761	8846	8931	9015	9100	9185	
2	9270	9355	9440	9524	9609	9694	9779	9863	9948		
										0033	
3	710117	0202	0287	0371	0456	0540	0625	0710	0794	0879	
4	0963	1048	1132	1217	1301	1385	1470	1554	1639	1723	
5	1807	1892	1976	2060	2144	2229	2313	2397	2481	2566	
6	2650	2734	2818	2902	2986	3070	3154	3238	3323	3407	
7	3491	3575	3659	3742	3826	3910	3994	4078	4162	4246	84
8	4330	4414	4497	4581	4665	4749	4833	4916	5000	5084	
9	5167	5251	5335	5418	5502	5586	5669	5753	5836	5920	
520	6003	6087	6170	6254	6337	6421	6504	6588	6671	6754	
1	6838	6921	7004	7088	7171	7254	7338	7421	7504	7587	
2	7671	7754	7837	7920	8003	8086	8169	8253	8336	8419	
3	8502	8585	8668	8751	8834	8917	9000	9083	9165	9248	83
4	9331	9414	9497	9580	9663	9745	9828	9911	9994		
										0077	
5	720159	0242	0325	0407	0490	0573	0655	0738	0821	0903	
6	0986	1068	1151	1233	1316	1398	1481	1563	1646	1728	
7	1811	1893	1975	2058	2140	2222	2305	2387	2469	2552	
8	2634	2716	2798	2881	2963	3045	3127	3209	3291	3374	
9	3456	3538	3620	3702	3784	3866	3948	4030	4112	4194	82
530	4276	4358	4440	4522	4604	4685	4767	4849	4931	5013	
1	5095	5176	5258	5340	5422	5503	5585	5667	5748	5830	
2	5912	5993	6075	6156	6238	6320	6401	6483	6564	6646	
3	6727	6809	6890	6972	7053	7134	7216	7297	7379	7460	
4	7541	7623	7704	7785	7866	7948	8029	8110	8191	8273	
5	8354	8435	8516	8597	8678	8759	8841	8922	9003	9084	
6	9165	9246	9327	9408	9489	9570	9651	9732	9813	9893	81
7	9974										
		0055	0136	0217	0298	0378	0459	0540	0621	0702	
8	730782	0863	0944	1024	1105	1186	1266	1347	1428	1508	
9	1589	1669	1750	1830	1911	1991	2072	2152	2233	2313	
540	2394	2474	2555	2635	2715	2796	2876	2956	3037	3117	
1	3197	3278	3358	3438	3518	3598	3679	3759	3839	3919	
2	3999	4079	4160	4240	4320	4400	4480	4560	4640	4720	80
3	4800	4880	4960	5040	5120	5200	5279	5359	5439	5519	
4	5599	5679	5759	5838	5918	5998	6078	6157	6237	6317	

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
87	8.7	17.4	26.1	34.8	43.5	52.2	60.9	69.6	78.3
86	8.6	17.2	25.8	34.4	43.0	51.6	60.2	68.8	77.4
85	8.5	17.0	25.5	34.0	42.5	51.0	59.5	68.0	76.5
84	8.4	16.8	25.2	33.6	42.0	50.4	58.8	67.2	75.6

No. 545 L. 736.] [No. 584 L. 767.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
545	736397	6476	6556	6635	6715	6795	6874	6954	7034	7113	
6	7193	7272	7352	7431	7511	7590	7670	7749	7829	7908	
7	7987	8067	8146	8225	8305	8384	8463	8543	8622	8701	
8	8781	8860	8939	9018	9097	9177	9256	9335	9414	9493	
9	9572	9651	9731	9810	9889	9968	0047	0126	0205	0284	79
550	740363	0442	0521	0600	0678	0757	0836	0915	0994	1073	
1	1152	1230	1309	1388	1467	1546	1624	1703	1782	1860	
2	1939	2018	2096	2175	2254	2332	2411	2489	2568	2647	
3	2725	2804	2882	2961	3039	3118	3196	3275	3353	3431	
4	3510	3588	3667	3745	3823	3902	3980	4058	4136	4215	
5	4293	4371	4449	4528	4606	4684	4762	4840	4919	4997	
6	5075	5153	5231	5309	5387	5465	5543	5621	5699	5777	78
7	5855	5933	6011	6089	6167	6245	6323	6401	6479	6556	
8	6634	6712	6790	6868	6945	7023	7101	7179	7256	7334	
9	7412	7489	7567	7645	7722	7800	7878	7955	8033	8110	
560	8188	8266	8343	8421	8498	8576	8653	8731	8808	8885	
1	8963	9040	9118	9195	9272	9350	9427	9504	9582	9659	
2	9736	9814	9891	9968	0045	0123	0200	0277	0354	0431	
3	750508	0586	0663	0740	0817	0894	0971	1048	1125	1202	
4	1279	1356	1433	1510	1587	1664	1741	1818	1895	1972	
5	2048	2125	2202	2279	2356	2433	2509	2586	2663	2740	77
6	2816	2893	2970	3047	3123	3200	3277	3353	3430	3506	
7	3583	3660	3736	3813	3889	3966	4042	4119	4195	4272	
8	4348	4425	4501	4578	4654	4730	4807	4883	4960	5036	
9	5112	5189	5265	5341	5417	5494	5570	5646	5722	5799	
570	5875	5951	6027	6103	6180	6256	6332	6408	6484	6560	
1	6636	6712	6788	6864	6940	7016	7092	7168	7244	7320	76
2	7396	7472	7548	7624	7700	7775	7851	7927	8003	8079	
3	8155	8230	8306	8382	8458	8533	8609	8685	8761	8836	
4	8912	8988	9063	9139	9214	9290	9366	9441	9517	9592	
5	9668	9743	9819	9894	9970	0045	0121	0196	0272	0347	
6	760422	0498	0573	0649	0724	0799	0875	0950	1025	1101	
7	1176	1251	1326	1402	1477	1552	1627	1702	1778	1853	
8	1928	2003	2078	2153	2228	2303	2378	2453	2529	2604	
9	2679	2754	2829	2904	2978	3053	3128	3203	3278	3353	75
580	3428	3503	3578	3653	3727	3802	3877	3952	4027	4101	
1	4176	4251	4326	4400	4475	4550	4624	4699	4774	4848	
2	4923	4998	5072	5147	5221	5296	5370	5445	5520	5594	
3	5669	5743	5818	5892	5966	6041	6115	6190	6264	6338	
4	6413	6487	6562	6636	6710	6785	6859	6933	7007	7082	

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
83	8.3	16.6	24.9	33.2	41.5	49.8	58.1	66.4	74.7
82	8.2	16.4	24.6	32.8	41.0	49.2	57.4	65.6	73.8
81	8.1	16.2	24.3	32.4	40.5	48.6	56.7	64.8	72.9
80	8.0	16.0	24.0	32.0	40.0	48.0	56.0	64.0	72.0
79	7.9	15.8	23.7	31.6	39.5	47.4	55.3	63.2	71.1
78	7.8	15.6	23.4	31.2	39.0	46.8	54.6	62.4	70.2
77	7.7	15.4	23.1	30.8	38.5	46.2	53.9	61.6	69.3
76	7.6	15.2	22.8	30.4	38.0	45.6	53.2	60.8	68.4
75	7.5	15.0	22.5	30.0	37.5	45.0	52.5	60.0	67.5
74	7.4	14.8	22.2	29.6	37.0	44.4	51.8	59.2	66.6

No. 585 L. 767.] [No. 629 L. 799.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
585	767156	7230	7304	7379	7453	7527	7601	7675	7749	7823	
6	7898	7972	8046	8120	8194	8268	8342	8416	8490	8564	74
7	8638	8712	8786	8860	8934	9008	9082	9156	9230	9303	
8	9377	9451	9525	9599	9673	9746	9820	9894	9968		
										0042	
9	770115	0189	0263	0336	0410	0484	0557	0631	0705	0778	
590	0852	0926	0999	1073	1146	1220	1293	1367	1440	1514	
1	1587	1661	1734	1808	1881	1955	2028	2102	2175	2248	
2	2322	2395	2468	2542	2615	2688	2762	2835	2908	2981	
3	3055	3128	3201	3274	3348	3421	3494	3567	3640	3713	
4	3786	3860	3933	4006	4079	4152	4225	4298	4371	4444	73
5	4517	4590	4663	4736	4809	4882	4955	5028	5100	5173	
6	5246	5319	5392	5465	5538	5610	5683	5756	5829	5902	
7	5974	6047	6120	6193	6265	6338	6411	6483	6556	6629	
8	6701	6774	6846	6919	6992	7064	7137	7209	7282	7354	
9	7427	7499	7572	7644	7717	7789	7862	7934	8006	8079	
600	8151	8224	8296	8368	8441	8513	8585	8658	8730	8802	
1	8874	8947	9019	9091	9163	9236	9308	9380	9452	9524	
2	9596	9669	9741	9813	9885	9957					
							0029	0101	0173	0245	
3	780317	0389	0461	0533	0605	0677	0749	0821	0893	0965	72
4	1037	1109	1181	1253	1324	1396	1468	1540	1612	1684	
5	1755	1827	1899	1971	2042	2114	2186	2258	2329	2401	
6	2473	2544	2616	2688	2759	2831	2902	2974	3046	3117	
7	3189	3260	3332	3403	3475	3546	3618	3689	3761	3832	
8	3904	3975	4046	4118	4189	4261	4332	4403	4475	4546	
9	4617	4689	4760	4831	4902	4974	5045	5116	5187	5259	
610	5330	5401	5472	5543	5615	5686	5757	5828	5899	5970	
1	6041	6112	6183	6254	6325	6396	6467	6538	6609	6680	71
2	6751	6822	6893	6964	7035	7106	7177	7248	7319	7390	
3	7460	7531	7602	7673	7744	7815	7885	7956	8027	8098	
4	8168	8239	8310	8381	8451	8522	8593	8663	8734	8804	
5	8875	8946	9016	9087	9157	9228	9299	9369	9440	9510	
6	9581	9651	9722	9792	9863	9933					
							0004	0074	0144	0215	
7	790285	0356	0426	0496	0567	0637	0707	0778	0848	0918	
8	0988	1059	1129	1199	1269	1340	1410	1480	1550	1620	
9	1691	1761	1831	1901	1971	2041	2111	2181	2252	2322	
620	2392	2462	2532	2602	2672	2742	2812	2882	2952	3022	70
1	3092	3162	3231	3301	3371	3441	3511	3581	3651	3721	
2	3790	3860	3930	4000	4070	4139	4209	4279	4349	4418	
3	4488	4558	4627	4697	4767	4836	4906	4976	5045	5115	
4	5185	5254	5324	5393	5463	5532	5602	5672	5741	5811	
5	5880	5949	6019	6088	6158	6227	6297	6366	6436	6505	
6	6574	6644	6713	6782	6852	6921	6990	7060	7129	7198	
7	7268	7337	7406	7475	7545	7614	7683	7752	7821	7890	
8	7960	8029	8098	8167	8236	8305	8374	8443	8513	8582	
9	8651	8720	8789	8858	8927	8996	9065	9134	9203	9272	69

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
75	7.5	15.0	22.5	30.0	37.5	45.0	52.5	60.0	67.5
74	7.4	14.8	22.2	29.6	37.0	44.4	51.8	59.2	66.6
73	7.3	14.6	21.9	29.2	36.5	43.8	51.1	58.4	65.7
72	7.2	14.4	21.6	28.8	36.0	43.2	50.4	57.6	64.8
71	7.1	14.2	21.3	28.4	35.5	42.6	49.7	56.8	63.9
70	7.0	14.0	21.0	28.0	35.0	42.0	49.0	56.0	63.0
69	6.9	13.8	20.7	27.6	34.5	41.4	48.3	55.2	62.1

No. 630 L. 799.] [No. 674 L. 829.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
630	799341	9409	9478	9547	9616	9685	9754	9823	9892	9961	
1	800029	0098	0167	0236	0305	0373	0442	0511	0580	0648	
2	0717	0786	0854	0923	0992	1061	1129	1198	1266	1335	
3	1404	1472	1541	1609	1678	1747	1815	1884	1952	2021	
4	2089	2158	2226	2295	2363	2432	2500	2568	2637	2705	
5	2774	2842	2910	2979	3047	3116	3184	3252	3321	3389	
6	3457	3525	3594	3662	3730	3798	3867	3935	4003	4071	
7	4139	4208	4276	4344	4412	4480	4548	4616	4685	4753	
8	4821	4889	4957	5025	5093	5161	5229	5297	5365	5433	68
9	5501	5569	5637	5705	5773	5841	5908	5976	6044	6112	
640	806180	6248	6316	6384	6451	6519	6587	6655	6723	6790	
1	6858	6926	6994	7061	7129	7197	7264	7332	7400	7467	
2	7535	7603	7670	7738	7806	7873	7941	8008	8076	8143	
3	8211	8279	8346	8414	8481	8549	8616	8684	8751	8818	
4	8886	8953	9021	9088	9156	9223	9290	9358	9425	9492	
5	9560	9627	9694	9762	9829	9896	9964	0031	0098	0165	
6	810233	0300	0367	0434	0501	0569	0636	0703	0770	0837	
7	0904	0971	1039	1106	1173	1240	1307	1374	1441	1508	67
8	1575	1642	1709	1776	1843	1910	1977	2044	2111	2178	
9	2245	2312	2379	2445	2512	2579	2646	2713	2780	2847	
650	2913	2980	3047	3114	3181	3247	3314	3381	3448	3514	
1	3581	3648	3714	3781	3848	3914	3981	4048	4114	4181	
2	4248	4314	4381	4447	4514	4581	4647	4714	4780	4847	
3	4913	4980	5046	5113	5179	5246	5312	5378	5445	5511	
4	5578	5644	5711	5777	5843	5910	5976	6042	6109	6175	
5	6241	6308	6374	6440	6506	6573	6639	6705	6771	6838	
6	6904	6970	7036	7102	7169	7235	7301	7367	7433	7499	
7	7565	7631	7698	7764	7830	7896	7962	8028	8094	8160	
8	8226	8292	8358	8424	8490	8556	8622	8688	8754	8820	
9	8885	8951	9017	9083	9149	9215	9281	9346	9412	9478	66
660	9544	9610	9676	9741	9807	9873	9939	0004	0070	0136	
1	820201	0267	0333	0399	0464	0530	0595	0661	0727	0792	
2	0858	0924	0989	1055	1120	1186	1251	1317	1382	1448	
3	1514	1579	1645	1710	1775	1841	1906	1972	2037	2103	
4	2168	2233	2299	2364	2430	2495	2560	2626	2691	2756	
5	2822	2887	2952	3018	3083	3148	3213	3279	3344	3409	
6	3474	3539	3605	3670	3735	3800	3865	3930	3996	4061	
7	4126	4191	4256	4321	4386	4451	4516	4581	4646	4711	65
8	4776	4841	4906	4971	5036	5101	5166	5231	5296	5361	
9	5426	5491	5556	5621	5686	5751	5815	5880	5945	6010	
670	6075	6140	6204	6269	6334	6399	6464	6528	6593	6658	
1	6723	6787	6852	6917	6981	7046	7111	7175	7240	7305	
2	7369	7434	7499	7563	7628	7692	7757	7821	7886	7951	
3	8015	8080	8144	8209	8273	8338	8402	8467	8531	8595	
4	8660	8724	8789	8853	8918	8982	9046	9111	9175	9239	

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
68	6.8	13.6	20.4	27.2	34.0	40.8	47.6	54.4	61.2
67	6.7	13.4	20.1	26.8	33.5	40.2	46.9	53.6	60.3
66	6.6	13.2	19.8	26.4	33.0	39.6	46.2	52.8	59.4
65	6.5	13.0	19.5	26.0	32.5	39.0	45.5	52.0	58.5
64	6.4	12.8	19.2	25.6	32.0	38.4	44.8	51.2	57.6

No. 675 L. 829.] [No. 719 L. 857.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
675	829304	9368	9432	9497	9561	9625	9690	9754	9818	9882	
6	9947	0011	0075	0139	0204	0268	0332	0396	0460	0525	
7	830589	0653	0717	0781	0845	0909	0973	1037	1102	1166	
8	1230	1294	1358	1422	1486	1550	1614	1678	1742	1806	64
9	1870	1934	1998	2062	2126	2189	2253	2317	2381	2445	
680	2509	2573	2637	2700	2764	2828	2892	2956	3020	3083	
1	3147	3211	3275	3338	3402	3466	3530	3593	3657	3721	
2	3784	3848	3912	3975	4039	4103	4166	4230	4294	4357	
3	4421	4484	4548	4611	4675	4739	4802	4866	4929	4993	
4	5056	5120	5183	5247	5310	5373	5437	5500	5564	5627	
5	5691	5754	5817	5881	5944	6007	6071	6134	6197	6261	
6	6324	6387	6451	6514	6577	6641	6704	6767	6830	6894	
7	6957	7020	7083	7146	7210	7273	7336	7399	7462	7525	
8	7588	7652	7715	7778	7841	7904	7967	8030	8093	8156	
9	8219	8282	8345	8408	8471	8534	8597	8660	8723	8786	63
690	8849	8912	8975	9038	9101	9164	9227	9289	9352	9415	
1	9478	9541	9604	9667	9729	9792	9855	9918	9981	0043	
2	840106	0169	0232	0294	0357	0420	0482	0545	0608	0671	
3	0733	0796	0859	0921	0984	1046	1109	1172	1234	1297	
4	1359	1422	1485	1547	1610	1672	1735	1797	1860	1922	
5	1985	2047	2110	2172	2235	2297	2360	2422	2484	2547	
6	2609	2672	2734	2796	2859	2921	2983	3046	3108	3170	
7	3233	3295	3357	3420	3482	3544	3606	3669	3731	3793	
8	3855	3918	3980	4042	4104	4166	4229	4291	4353	4415	
9	4477	4539	4601	4664	4726	4788	4850	4912	4974	5036	
700	5098	5160	5222	5284	5346	5408	5470	5532	5594	5656	62
1	5718	5780	5842	5904	5966	6028	6090	6151	6213	6275	
2	6337	6399	6461	6523	6585	6646	6708	6770	6832	6894	
3	6955	7017	7079	7141	7202	7264	7326	7388	7449	7511	
4	7573	7634	7696	7758	7819	7881	7943	8004	8066	8128	
5	8189	8251	8312	8374	8435	8497	8559	8620	8682	8743	
6	8805	8866	8928	8989	9051	9112	9174	9235	9297	9358	
7	9419	9481	9542	9604	9665	9726	9788	9849	9911	9972	
8	850033	0095	0156	0217	0279	0340	0401	0462	0524	0585	
9	0646	0707	0769	0830	0891	0952	1014	1075	1136	1197	
710	1258	1320	1381	1442	1503	1564	1625	1686	1747	1809	
1	1870	1931	1992	2053	2114	2175	2236	2297	2358	2419	
2	2480	2541	2602	2663	2724	2785	2846	2907	2968	3029	61
3	3090	3150	3211	3272	3333	3394	3455	3516	3577	3637	
4	3698	3759	3820	3881	3941	4002	4063	4124	4185	4245	
5	4306	4367	4428	4488	4549	4610	4670	4731	4792	4852	
6	4913	4974	5034	5095	5156	5216	5277	5337	5398	5459	
7	5519	5580	5640	5701	5761	5822	5882	5943	6003	6064	
8	6124	6185	6245	6306	6366	6427	6487	6548	6608	6668	
9	6729	6789	6850	6910	6970	7031	7091	7152	7212	7272	

Proportional Parts.

Diff.	1	2	3	4	5	6	7	8	9
65	6.5	13.0	19.5	26.0	32.5	39.0	45.5	52.0	58.5
64	6.4	12.8	19.2	25.6	32.0	38.4	44.8	51.2	57.6
63	6.3	12.6	18.9	25.2	31.5	37.8	44.1	50.4	56.7
62	6.2	12.4	18.6	24.8	31.0	37.2	43.4	49.6	55.8
61	6.1	12.2	18.3	24.4	30.5	36.6	42.7	48.8	54.9
60	6.0	12.0	18.0	24.0	30.0	36.0	42.0	48.0	54.0

N.	0	1	2	3	4	5	6	7	8	9	Diff.
720	857332	7393	7453	7513	7574	7634	7694	7755	7815	7875	
1	7935	7995	8056	8116	8176	8236	8297	8357	8417	8477	
2	8537	8597	8657	8718	8778	8838	8898	8958	9018	9078	
3	9138	9198	9258	9318	9379	9439	9499	9559	9619	9679	60
4	9739	9799	9859	9918	9978	0038	0098	0158	0218	0278	
5	860338	0398	0458	0518	0578	0637	0697	0757	0817	0877	
6	0937	0996	1056	1116	1176	1236	1295	1355	1415	1475	
7	1534	1594	1654	1714	1773	1833	1893	1952	2012	2072	
8	2131	2191	2251	2310	2370	2430	2489	2549	2608	2668	
9	2728	2787	2847	2906	2966	3025	3085	3144	3204	3263	
730	3323	3382	3442	3501	3561	3620	3680	3739	3799	3858	
1	3917	3977	4036	4096	4155	4214	4274	4333	4392	4452	
2	4511	4570	4630	4689	4748	4808	4867	4926	4985	5045	
3	5104	5163	5222	5282	5341	5400	5459	5519	5578	5637	
4	5696	5755	5814	5874	5933	5992	6051	6110	6169	6228	
5	6287	6346	6405	6465	6524	6583	6642	6701	6760	6819	59
6	6878	6937	6996	7055	7114	7173	7232	7291	7350	7409	
7	7467	7526	7585	7644	7703	7762	7821	7880	7939	7998	
8	8056	8115	8174	8233	8292	8350	8409	8468	8527	8586	
9	8644	8703	8762	8821	8879	8938	8997	9056	9114	9173	
740	9232	9290	9349	9408	9466	9525	9584	9642	9701	9760	
1	9818	9877	9935	9994	0053	0111	0170	0228	0287	0345	
2	870404	0462	0521	0579	0638	0696	0755	0813	0872	0930	
3	0989	1047	1106	1164	1223	1281	1339	1398	1456	1515	
4	1573	1631	1690	1748	1806	1865	1923	1981	2040	2098	
5	2156	2215	2273	2331	2389	2448	2506	2564	2622	2681	
6	2739	2797	2855	2913	2972	3030	3088	3146	3204	3262	
7	3321	3379	3437	3495	3553	3611	3669	3727	3785	3844	
8	3902	3960	4018	4076	4134	4192	4250	4308	4366	4424	58
9	4482	4540	4598	4656	4714	4772	4830	4888	4945	5003	
750	5061	5119	5177	5235	5293	5351	5409	5466	5524	5582	
1	5640	5698	5756	5813	5871	5929	5987	6045	6102	6160	
2	6218	6276	6333	6391	6449	6507	6564	6622	6680	6737	
3	6795	6853	6910	6968	7026	7083	7141	7199	7256	7314	
4	7371	7429	7487	7544	7602	7659	7717	7774	7832	7889	
5	7947	8004	8062	8119	8177	8234	8292	8349	8407	8464	
6	8522	8579	8637	8694	8752	8809	8866	8924	8981	9039	
7	9096	9153	9211	9268	9325	9383	9440	9497	9555	9612	
8	9669	9726	9784	9841	9898	9956	0013	0070	0127	0185	
9	880242	0299	0356	0413	0471	0528	0585	0642	0699	0756	
760	0814	0871	0928	0985	1042	1099	1156	1213	1271	1328	
1	1385	1442	1499	1556	1613	1670	1727	1784	1841	1898	
2	1955	2012	2069	2126	2183	2240	2297	2354	2411	2468	57
3	2525	2581	2638	2695	2752	2809	2866	2923	2980	3037	
4	3093	3150	3207	3264	3321	3377	3434	3491	3548	3605	

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
59	5.9	11.8	17.7	23.6	29.5	35.4	41.3	47.2	53.1
58	5.8	11.6	17.4	23.2	29.0	34.8	40.6	46.4	52.2
57	5.7	11.4	17.1	22.8	28.5	34.2	39.9	45.6	51.3
56	5.6	11.2	16.8	22.4	28.0	33.6	39.2	44.8	50.4

N.	0	1	2	3	4	5	6	7	8	9	Diff.
765	883661	3718	3775	3832	3888	3945	4002	4059	4115	4172	
6	4229	4285	4342	4399	4455	4512	4569	4625	4682	4739	
7	4795	4852	4909	4965	5022	5078	5135	5192	5248	5305	
8	5361	5418	5474	5531	5587	5644	5700	5757	5813	5870	
9	5926	5983	6039	6096	6152	6209	6265	6321	6378	6434	
770	6491	6547	6604	6660	6716	6773	6829	6885	6942	6998	
1	7054	7111	7167	7223	7280	7336	7392	7449	7505	7561	
2	7617	7674	7730	7786	7842	7898	7955	8011	8067	8123	
3	8179	8236	8292	8348	8404	8460	8516	8573	8629	8685	
4	8741	8797	8853	8909	8965	9021	9077	9134	9190	9246	
5	9302	9358	9414	9470	9526	9582	9638	9694	9750	9806	56
6	9862	9918	9974	0030	0086	0141	0197	0253	0309	0365	
7	890421	0477	0533	0589	0645	0700	0756	0812	0868	0924	
8	0980	1035	1091	1147	1203	1259	1314	1370	1426	1482	
9	1537	1593	1649	1705	1760	1816	1872	1928	1983	2039	
780	2095	2150	2206	2262	2317	2373	2429	2484	2540	2595	
1	2651	2707	2762	2818	2873	2929	2985	3040	3096	3151	
2	3207	3262	3318	3373	3429	3484	3540	3595	3651	3706	
3	3762	3817	3873	3928	3984	4039	4094	4150	4205	4261	
4	4316	4371	4427	4482	4538	4593	4648	4704	4759	4814	
5	4870	4925	4980	5036	5091	5146	5201	5257	5312	5367	
6	5423	5478	5533	5588	5644	5699	5754	5809	5864	5920	
7	5975	6030	6085	6140	6195	6251	6306	6361	6416	6471	
8	6526	6581	6636	6692	6747	6802	6857	6912	6967	7022	
9	7077	7132	7187	7242	7297	7352	7407	7462	7517	7572	55
790	7627	7682	7737	7792	7847	7902	7957	8012	8067	8122	
1	8176	8231	8286	8341	8396	8451	8506	8561	8615	8670	
2	8725	8780	8835	8890	8944	8999	9054	9109	9164	9218	
3	9273	9328	9383	9437	9492	9547	9602	9656	9711	9766	
4	9821	9875	9930	9985	0039	0094	0149	0203	0258	0312	
5	900367	0422	0476	0531	0586	0640	0695	0749	0804	0859	
6	0913	0968	1022	1077	1131	1186	1240	1295	1349	1404	
7	1458	1513	1567	1622	1676	1731	1785	1840	1894	1948	
8	2003	2057	2112	2166	2221	2275	2329	2384	2438	2492	
9	2547	2601	2655	2710	2764	2818	2873	2927	2981	3036	
800	3090	3144	3199	3253	3307	3361	3416	3470	3524	3578	
1	3633	3687	3741	3795	3849	3904	3958	4012	4066	4120	
2	4174	4229	4283	4337	4391	4445	4499	4553	4607	4661	
3	4716	4770	4824	4878	4932	4986	5040	5094	5148	5202	54
4	5256	5310	5364	5418	5472	5526	5580	5634	5688	5742	
5	5796	5850	5904	5958	6012	6066	6119	6173	6227	6281	
6	6335	6389	6443	6497	6551	6604	6658	6712	6766	6820	
7	6874	6927	6981	7035	7089	7143	7196	7250	7304	7358	
8	7411	7465	7519	7573	7626	7680	7734	7787	7841	7895	
9	7949	8002	8056	8110	8163	8217	8270	8324	8378	8431	

Proportional Parts.

Diff.	1	2	3	4	5	6	7	8	9
57	5.7	11.4	17.1	22.8	28.5	34.2	39.9	45.6	51.3
56	5.6	11.2	16.8	22.4	28.0	33.6	39.2	44.8	50.4
55	5.5	11.0	16.5	22.0	27.5	33.0	38.5	44.0	49.5
54	5.4	10.8	16.2	21.6	27.0	32.4	37.8	43.2	48.6

No. 810 L. 908.] [No. 854 L. 931.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
810	908485	8539	8592	8646	8699	8753	8807	8860	8914	8967	
1	9021	9074	9128	9181	9235	9289	9342	9396	9449	9503	
2	9556	9610	9663	9716	9770	9823	9877	9930	9984	0037	
3	910091	0144	0197	0251	0304	0358	0411	0464	0518	0571	
4	0624	0678	0731	0784	0838	0891	0944	0998	1051	1104	
5	1158	1211	1264	1317	1371	1424	1477	1530	1584	1637	
6	1690	1743	1797	1850	1903	1956	2009	2063	2116	2169	
7	2222	2275	2328	2381	2435	2488	2541	2594	2647	2700	
8	2753	2806	2859	2913	2966	3019	3072	3125	3178	3231	
9	3284	3337	3390	3443	3496	3549	3602	3655	3708	3761	53
820	3814	3867	3920	3973	4026	4079	4132	4184	4237	4290	
1	4343	4396	4449	4502	4555	4608	4660	4713	4766	4819	
2	4872	4925	4977	5030	5083	5136	5189	5241	5294	5347	
3	5400	5453	5505	5558	5611	5664	5716	5769	5822	5875	
4	5927	5980	6033	6085	6138	6191	6243	6296	6349	6401	
5	6454	6507	6559	6612	6664	6717	6770	6822	6875	6927	
6	6980	7033	7085	7138	7190	7243	7295	7348	7400	7453	
7	7506	7558	7611	7663	7716	7768	7820	7873	7925	7978	
8	8030	8083	8135	8188	8240	8293	8345	8397	8450	8502	
9	8555	8607	8659	8712	8764	8816	8869	8921	8973	9026	
830	9078	9130	9183	9235	9287	9340	9392	9444	9496	9549	
1	9601	9653	9706	9758	9810	9862	9914	9967	0019	0071	
2	920123	0176	0228	0280	0332	0384	0436	0489	0541	0593	
3	0645	0697	0749	0801	0853	0906	0958	1010	1062	1114	
4	1166	1218	1270	1322	1374	1426	1478	1530	1582	1634	52
5	1686	1738	1790	1842	1894	1946	1998	2050	2102	2154	
6	2206	2258	2310	2362	2414	2466	2518	2570	2622	2674	
7	2725	2777	2829	2881	2933	2985	3037	3089	3140	3192	
8	3244	3296	3348	3399	3451	3503	3555	3607	3658	3710	
9	3762	3814	3865	3917	3969	4021	4072	4124	4176	4228	
840	4279	4331	4383	4434	4486	4538	4589	4641	4693	4744	
1	4796	4848	4899	4951	5003	5054	5106	5157	5209	5261	
2	5312	5364	5415	5467	5518	5570	5621	5673	5725	5776	
3	5828	5879	5931	5982	6034	6085	6137	6188	6240	6291	
4	6342	6394	6445	6497	6548	6600	6651	6702	6754	6805	
5	6857	6908	6959	7011	7062	7114	7165	7216	7268	7319	
6	7370	7422	7473	7524	7576	7627	7678	7730	7781	7832	
7	7883	7935	7986	8037	8088	8140	8191	8242	8293	8345	
8	8396	8447	8498	8549	8601	8652	8703	8754	8805	8857	
9	8908	8959	9010	9061	9112	9163	9215	9266	9317	9368	
850	9419	9470	9521	9572	9623	9674	9725	9776	9827	9879	51
1	9930	9981	0032	0083	0134	0185	0236	0287	0338	0389	
2	930440	0491	0542	0592	0643	0694	0745	0796	0847	0898	
3	0949	1000	1051	1102	1153	1204	1254	1305	1356	1407	
4	1458	1509	1560	1610	1661	1712	1763	1814	1865	1915	

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
53	5.3	10.6	15.9	21.2	26.5	31.8	37.1	42.4	47.7
52	5.2	10.4	15.6	20.8	26.0	31.2	36.4	41.6	46.8
51	5.1	10.2	15.3	20.4	25.5	30.6	35.7	40.8	45.9
50	5.0	10.0	15.0	20.0	25.0	30.0	35.0	40.0	45.0

No. 855 L. 931.] [No. 899 L. 954.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
855	931966	2017	2068	2118	2169	2220	2271	2322	2372	2423	
6	2474	2524	2575	2626	2677	2727	2778	2829	2879	2930	
7	2981	3031	3082	3133	3183	3234	3285	3335	3386	3437	
8	3487	3538	3589	3639	3690	3740	3791	3841	3892	3943	
9	3993	4044	4094	4145	4195	4246	4296	4347	4397	4448	
860	4498	4549	4599	4650	4700	4751	4801	4852	4902	4953	
1	5003	5054	5104	5154	5205	5255	5306	5356	5406	5457	
2	5507	5558	5608	5658	5709	5759	5809	5860	5910	5960	
3	6011	6061	6111	6162	6212	6262	6313	6363	6413	6463	
4	6514	6564	6614	6665	6715	6765	6815	6865	6916	6966	
5	7016	7066	7116	7167	7217	7267	7317	7367	7418	7468	
6	7518	7568	7618	7668	7718	7769	7819	7869	7919	7969	
7	8019	8069	8119	8169	8219	8269	8320	8370	8420	8470	50
8	8520	8570	8620	8670	8720	8770	8820	8870	8920	8970	
9	9020	9070	9120	9170	9220	9270	9320	9369	9419	9469	
870	9519	9569	9619	9669	9719	9769	9819	9869	9918	9968	
1	940018	0068	0118	0168	0218	0267	0317	0367	0417	0467	
2	0516	0566	0616	0666	0716	0765	0815	0865	0915	0964	
3	1014	1064	1114	1163	1213	1263	1313	1362	1412	1462	
4	1511	1561	1611	1660	1710	1760	1809	1859	1909	1958	
5	2008	2058	2107	2157	2207	2256	2306	2355	2405	2455	
6	2504	2554	2603	2653	2702	2752	2801	2851	2901	2950	
7	3000	3049	3099	3148	3198	3247	3297	3346	3396	3445	
8	3495	3544	3593	3643	3692	3742	3791	3841	3890	3939	
9	3989	4038	4088	4137	4186	4236	4285	4335	4384	4433	
880	4483	4532	4581	4631	4680	4729	4779	4828	4877	4927	
1	4976	5025	5074	5124	5173	5222	5272	5321	5370	5419	
2	5469	5518	5567	5616	5665	5715	5764	5813	5862	5912	
3	5961	6010	6059	6108	6157	6207	6256	6305	6354	6403	
4	6452	6501	6551	6600	6649	6698	6747	6796	6845	6894	
5	6943	6992	7041	7090	7139	7189	7238	7287	7336	7385	49
6	7434	7483	7532	7581	7630	7679	7728	7777	7826	7875	
7	7924	7973	8022	8070	8119	8168	8217	8266	8315	8364	
8	8413	8462	8511	8560	8608	8657	8706	8755	8804	8853	
9	8902	8951	8999	9048	9097	9146	9195	9244	9292	9341	
890	9390	9439	9488	9536	9585	9634	9683	9731	9780	9829	
1	9878	9926	9975	0024	0073	0121	0170	0219	0267	0316	
2	950365	0414	0462	0511	0560	0608	0657	0706	0754	0803	
3	0851	0900	0949	0997	1046	1095	1143	1192	1240	1289	
4	1338	1386	1435	1483	1532	1580	1629	1677	1726	1775	
5	1823	1872	1920	1969	2017	2066	2114	2163	2211	2260	
6	2308	2356	2405	2453	2502	2550	2599	2647	2696	2744	
7	2792	2841	2889	2938	2986	3034	3083	3131	3180	3228	
8	3276	3325	3373	3421	3470	3518	3566	3615	3663	3711	
9	3760	3808	3856	3905	3953	4001	4049	4098	4146	4194	

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
51	5.1	10.2	15.3	20.4	25.5	30.6	35.7	40.8	45.9
50	5.0	10.0	15.0	20.0	25.0	30.0	35.0	40.0	45.0
49	4.9	9.8	14.7	19.6	24.5	29.4	34.3	39.2	44.1
48	4.8	9.6	14.4	19.2	24.0	28.8	33.6	38.4	43.2

N.	0	1	2	3	4	5	6	7	8	9	Diff.
900	954243	4291	4339	4387	4435	4484	4532	4580	4628	4677	
1	4725	4773	4821	4869	4918	4966	5014	5062	5110	5158	
2	5207	5255	5303	5351	5399	5447	5495	5543	5592	5640	
3	5688	5736	5784	5832	5880	5928	5976	6024	6072	6120	
4	6168	6216	6265	6313	6361	6409	6457	6505	6553	6601	
5	6649	6697	6745	6793	6840	6888	6936	6984	7032	7080	48
6	7128	7176	7224	7272	7320	7368	7416	7464	7512	7559	
7	7607	7655	7703	7751	7799	7847	7894	7942	7990	8038	
8	8086	8134	8181	8229	8277	8325	8373	8421	8468	8516	
9	8564	8612	8659	8707	8755	8803	8850	8898	8946	8994	
910	9041	9089	9137	9185	9232	9280	9328	9375	9423	9471	
1	9518	9566	9614	9661	9709	9757	9804	9852	9900	9947	
2	9995	0042	0090	0138	0185	0233	0280	0328	0676	0423	
3	960471	0518	0566	0613	0661	0709	0756	0804	0851	0899	
4	0946	0994	1041	1089	1136	1184	1231	1279	1326	1374	
5	1421	1469	1516	1563	1611	1658	1706	1753	1801	1848	
6	1895	1943	1990	2038	2085	2132	2180	2227	2275	2322	
7	2369	2417	2464	2511	2559	2606	2653	2701	2748	2795	
8	2843	2890	2937	2985	3032	3079	3126	3174	3221	3268	
9	3316	3363	3410	3457	3504	3552	3599	3646	3693	3741	
920	3788	3835	3882	3929	3977	4024	4071	4118	4165	4212	
1	4260	4307	4354	4401	4448	4495	4542	4590	4637	4684	
2	4731	4778	4825	4872	4919	4966	5013	5061	5108	5155	
3	5202	5249	5296	5343	5390	5437	5484	5531	5578	5625	
4	5672	5719	5766	5813	5860	5907	5954	6001	6048	6095	47
5	6142	6189	6236	6283	6329	6376	6423	6470	6517	6564	
6	6611	6658	6705	6752	6799	6845	6892	6939	6986	7033	
7	7080	7127	7173	7220	7267	7314	7361	7408	7454	7501	
8	7548	7595	7642	7688	7735	7782	7829	7875	7922	7969	
9	8016	8062	8109	8156	8203	8249	8296	8343	8390	8436	
930	8483	8530	8576	8623	8670	8716	8763	8810	8856	8903	
1	8950	8996	9043	9090	9136	9183	9229	9276	9323	9369	
2	9416	9463	9509	9556	9602	9649	9695	9742	9789	9835	
3	9882	9928	9975	0021	0068	0114	0161	0207	0254	0300	
4	970347	0393	0440	0486	0533	0579	0626	0672	0719	0765	
5	0812	0858	0904	0951	0997	1044	1090	1137	1183	1229	
6	1276	1322	1369	1415	1461	1508	1554	1601	1647	1693	
7	1740	1786	1832	1879	1925	1971	2018	2064	2110	2157	
8	2203	2249	2295	2342	2388	2434	2481	2527	2573	2619	
9	2666	2712	2758	2804	2851	2897	2943	2989	3035	3082	
940	3128	3174	3220	3266	3313	3359	3405	3451	3497	3543	
1	3590	3636	3682	3728	3774	3820	3866	3913	3959	4005	
2	4051	4097	4143	4189	4235	4281	4327	4374	4420	4466	
3	4512	4558	4604	4650	4696	4742	4788	4834	4880	4926	
4	4972	5018	5064	5110	5156	5202	5248	5294	5340	5386	46

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
47	4.7	9.4	14.1	18.8	23.5	28.2	32.9	37.6	42.3
46	4.6	9.2	13.8	18.4	23.0	27.6	32.2	36.8	41.4

N.	0	1	2	3	4	5	6	7	8	9	Diff.
945	975432	5478	5524	5570	5616	5662	5707	5753	5799	5845	
6	5891	5937	5983	6029	6075	6121	6167	6212	6258	6304	
7	6350	6396	6442	6488	6533	6579	6625	6671	6717	6763	
8	6808	6854	6900	6946	6992	7037	7083	7129	7175	7220	
9	7266	7312	7358	7403	7449	7495	7541	7586	7632	7678	
950	7724	7769	7815	7861	7906	7952	7998	8043	8089	8135	
1	8181	8226	8272	8317	8363	8409	8454	8500	8546	8591	
2	8637	8683	8728	8774	8819	8865	8911	8956	9002	9047	
3	9093	9138	9184	9230	9275	9321	9366	9412	9457	9503	
4	9548	9594	9639	9685	9730	9776	9821	9867	9912	9958	
5	980003	0049	0094	0140	0185	0231	0276	0322	0367	0412	
6	0458	0503	0549	0594	0640	0685	0730	0776	0821	0867	
7	0912	0957	1003	1048	1093	1139	1184	1229	1275	1320	
8	1366	1411	1456	1501	1547	1592	1637	1683	1728	1773	
9	1819	1864	1909	1954	2000	2045	2090	2135	2181	2226	
960	2271	2316	2362	2407	2452	2497	2543	2588	2633	2678	
1	2723	2769	2814	2859	2904	2949	2994	3040	3085	3130	
2	3175	3220	3265	3310	3356	3401	3446	3491	3536	3581	
3	3626	3671	3716	3762	3807	3852	3897	3942	3987	4032	
4	4077	4122	4167	4212	4257	4302	4347	4392	4437	4482	
5	4527	4572	4617	4662	4707	4752	4797	4842	4887	4932	45
6	4977	5022	5067	5112	5157	5202	5247	5292	5337	5382	
7	5426	5471	5516	5561	5606	5651	5696	5741	5786	5830	
8	5875	5920	5965	6010	6055	6100	6144	6189	6234	6279	
9	6324	6369	6413	6458	6503	6548	6593	6637	6682	6727	
970	6772	6817	6861	6906	6951	6996	7040	7085	7130	7175	
1	7219	7264	7309	7353	7398	7443	7488	7532	7577	7622	
2	7666	7711	7756	7800	7845	7890	7934	7979	8024	8068	
3	8113	8157	8202	8247	8291	8336	8381	8425	8470	8514	
4	8559	8604	8648	8693	8737	8782	8826	8871	8916	8960	
5	9005	9049	9094	9138	9183	9227	9272	9316	9361	9405	
6	9450	9494	9539	9583	9628	9672	9717	9761	9806	9850	
7	9895	9939	9983	0028	0072	0117	0161	0206	0250	0294	
8	990339	0383	0428	0472	0516	0561	0605	0650	0694	0738	
9	0783	0827	0871	0916	0960	1004	1049	1093	1137	1182	
980	1226	1270	1315	1359	1403	1448	1492	1536	1580	1625	
1	1669	1713	1758	1802	1846	1890	1935	1979	2023	2067	
2	2111	2156	2200	2244	2288	2333	2377	2421	2465	2509	
3	2554	2598	2642	2686	2730	2774	2819	2863	2907	2951	
4	2995	3039	3083	3127	3172	3216	3260	3304	3348	3392	
5	3436	3480	3524	3568	3613	3657	3701	3745	3789	3833	
6	3877	3921	3965	4009	4053	4097	4141	4185	4229	4273	
7	4317	4361	4405	4449	4493	4537	4581	4625	4669	4713	44
8	4757	4801	4845	4889	4933	4977	5021	5065	5108	5152	
9	5196	5240	5284	5328	5372	5416	5460	5504	5547	5591	

PROPORTIONAL PARTS.

Diff.	1	2	3	4	5	6	7	8	9
46	4.6	9.2	13.8	18.4	23.0	27.6	32.2	36.8	41.
45	4.5	9.0	13.5	18.0	22.5	27.0	31.5	36.0	40.
44	4.4	8.8	13.2	17.6	22.0	26.4	30.8	35.2	39.
43	4.3	8.6	12.9	17.2	21.5	25.8	30.1	34.4	38.

No. 990 L. 995.] [No. 999 L. 999.

N.	0	1	2	3	4	5	6	7	8	9	Diff.
990	995635	5679	5723	5767	5811	5854	5898	5942	5986	6030	
1	6074	6117	6161	6205	6249	6293	6337	6380	6424	6468	44
2	6512	6555	6599	6643	6687	6731	6774	6818	6862	6906	
3	6949	6993	7037	7080	7124	7168	7212	7255	7299	7343	
4	7386	7430	7474	7517	7561	7605	7648	7692	7736	7779	
5	7823	7867	7910	7954	7998	8041	8085	8129	8172	8216	
6	8259	8303	8347	8390	8434	8477	8521	8564	8608	8652	
7	8695	8739	8782	8826	8869	8913	8956	9000	9043	9087	
8	9131	9174	9218	9261	9305	9348	9392	9435	9479	9522	
9	9565	9609	9652	9696	9739	9783	9826	9870	9913	9957	43

Constant Numbers and their Logarithms.

Symbol.	Number.	Logarithm.
π	3.141 592 653 590	0.497 149 872 694
2π	6.283 185 307 180	0.798 179 868 358
3π	9.424 777 960 769	0.974 271 127 414
4π	12.566 370 614 359	1.099 209 864 022
5π	15.707 963 267 950	1.196 119 877 030
6π	18.849 555 921 539	1.275 301 123 078
7π	21.991 148 575 119	1.342 247 912 708
8π	25.132 741 228 718	1.400 239 859 686
9π	28.274 333 882 308	1.451 392 382 133
$\frac{1}{6}\pi$	0.523 598 775 598	$\bar{1}$.718 998 622 810
$\frac{1}{4}\pi$	0.785 398 163 397	$\bar{1}$.895 089 881 366
$\frac{1}{2}\pi$	1.570 796 326 795	0.196 119 877 030
$\frac{4}{3}\pi$	4.188 790 204 786	0.622 088 609 302
π^2	9.869 604 401 089	0.994 299 745 388
π^3	31.006 276 680 293	1.491 449 618 082
$\sqrt{\pi}$	1.772 453 850 906	0.248 574 936 347
$\sqrt[3]{\pi}$	1.464 591 887 562	0.165 716 624 231
$1/\pi$	0.318 309 886 184	$\bar{1}$.502 850 127 306
$180/\pi$	57.295 779 513 025	1.758 122 632 409
$1/\pi^2$	0.101 321 183 642	$\bar{1}$.005 700 254 612
$1/\sqrt{\pi}$	0.564 189 583 548	$\bar{1}$.751 425 063 653
$\log_e \pi$	1.144 729 885 849	0.058 703 021 240
arc 1°	0.017 453 292 520	$\bar{2}$.241 877 367 591
sin 1°	0.017 452 406 417	$\bar{2}$.241 855 318 418
arc 1′	0.000 290 888 209	$\bar{4}$.463 726 117 207
sin 1′	0.000 290 888 205	$\bar{4}$.463 726 111 082
arc 1″	0.000 004 848 137	$\bar{6}$.685 574 866 824
sin 1″	0.000 004 848 137	$\bar{6}$.685 574 866 822
e	2.718 281 828 459	0.434 294 481 903
M	0.434 294 481 903	$\bar{1}$.637 784 311 301
$1/M$	2.302 585 092 994	0.362 215 688 699
$\sqrt{2}$	1.414 213 562 373	0.150 514 997 832
$\sqrt{3}$	1.732 050 807 569	0.238 560 627 360
$\sqrt{5}$	2.236 067 977 477	0.349 485 002 168

TABLE XII.

LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

Pages 198–242 give values of these functions to six decimal places for every minute of the first and second quadrants. The degrees are at the top and bottom of the pages and the minutes at the sides below or above the degrees. For example, on page 208, the angles 10° 26′ and 169° 34′ have log sin = 9.257898, while 79° 20′ and 100° 40′ have log cot = 9.274964.

The columns headed D. 1″ enable interpolation to be made for seconds; thus for 10° 26′ 15″ the D. 1″ is 11.42 for log sin, whence 11.42 × 15 = 171 and log sin for this angle is 9.257898 + 171 = 9.258069. Also for 163° 38′ 15″ the log tan is 9.467880 − 117 = 9.467763. The computed difference is to be added or subtracted according as the tabular values of the function increase or decrease with an increase in the angle.

The columns of D. 1″ are omitted on pages 198 and 199, except for log cos; while other columns are added which enable intermediate values of the other functions to be found for small angles more accurately than can be done by interpolation. Thus to find log sin A and log tan A, when A contains seconds, the equations

$$\log \sin A = S + \log A'', \qquad \log \tan A = T + \log A'',$$

are to be used, A'' signifying the number of seconds in the angle A. For example, let the angle A be 1° 6′ 33″ or 3993″; for 1° 6′ the value of S is taken from the fourth column on page 199 and log 3993 from Table XI. Then

For 1° 6′	S = 4.685548
log 3993	= 3.601299
log sin 1° 6′ 33″	= 8.286847

Similarly for 0° 54′ 12″ or 3252″ the log tan is found as follows:

For 0° 54′	T = 4.685611
log 3252	= 3.512151
log tan 0° 54′ 12″	= 8.197762

To find log cot for a small angle the equation log cot $A = C - \log A''$ is to be used where C is taken from the eighth column. For example, for 1° 0′ 16″ or 3616″ the value of C is 15.314381 and that of log 3616 is 3.558228, whence log cot 1° 0′ 16″ = 11.756153.

To find the angle from a given logarithmic function, the eye must run along the table until the tabular value nearest to it is found. Thus, when log tan is given as 9.516910 this is found on page 216 and the angle is either 18° 12′ or 161° 48′. Again, when log tan is given as 9.526004, this is found to lie between 9.525778 and 9.526197; to the first value corresponds the angle 18° 33′ and the D. 1″ is 6.98; the difference 9.526004 − 9.525778 is 226 and 226/6.98 = 32.4″, so that the required angle is 18° 33′ 32″.4.

When the given function falls on page 198 or 199, the number of seconds is found by the equations

$$\log A'' = \log \sin A - S, \quad \log A'' = \log \tan A - T, \quad \log A'' = C - \log \cot A.$$

For example, given log tan A as 8.465371 for which T is 4.685700; then log A'' = 8.465371 − 4.685700 = 3.779671 from which by Table XI there is found A'' = 6021″, and hence A = 1° 40′ 21″.

"	'	Sine.	S	T	Tang.	Cotang.	C	D 1"	Cosine.	'
			4.685				15.314			
0	0	Inf. neg.	575	575	Inf. neg.	Inf. pos.	425		ten	60
60	1	6.463726	575	575	6.463726	13.536274	425		ten	59
120	2	.764756	575	575	.764756	.235244	425		ten	58
180	3	6.940847	575	575	6.940847	13.059153	425		ten	57
240	4	7.065786	575	575	7.065786	12.934214	425		ten	56
300	5	.162696	575	575	.162696	.837304	425		ten	55
360	6	.241877	575	575	.241878	.758122	425	.02	9.999999	54
420	7	.308824	575	575	.308825	.691175	425	.00	.999999	53
480	8	.366816	574	576	.366817	.633183	424	.00	.999999	52
540	9	.417968	574	576	.417970	.582030	424	.00	.999999	51
600	10	.463726	574	576	.463727	.536273	424	.02	.999998	50
660	11	7.505118	574	576	7.505120	12.494880	424	.00	9.999998	49
720	12	.542906	574	577	.542909	.457091	423	.02	.999997	48
780	13	.577668	574	577	.577672	.422328	423	.00	.999997	47
840	14	.609853	574	577	.609857	.390143	423	.02	.999996	46
900	15	.639816	573	578	.639820	.360180	422	.00	.999996	45
960	16	.667845	573	578	.667849	.332151	422	.02	.999995	44
1020	17	.694173	573	578	.694179	.305821	422	.00	.999995	43
1080	18	.718997	573	579	.719003	.280997	421	.02	.999994	42
1140	19	.742478	573	579	.742484	.257516	421	.02	.999993	41
1200	20	.764754	572	580	.764761	.235239	420	.00	.999993	40
1260	21	7.785943	572	580	7.785951	12.214049	420	.02	9.999992	39
1320	22	.806146	572	581	.806155	.193845	419	.02	.999991	38
1380	23	.825451	572	581	.825460	.174540	419	.02	.999990	37
1440	24	.843934	571	582	.843944	.156056	418	.02	.999989	36
1500	25	.861662	571	583	.861674	.138326	417	.00	.999989	35
1560	26	.878695	571	583	.878708	.121292	417	.02	.999988	34
1620	27	.895085	570	584	.895099	.104901	416	.02	.999987	33
1680	28	.910879	570	584	.910894	.089106	416	.02	.999986	32
1740	29	.926119	570	585	.926134	.073866	415	.02	.999985	31
1800	30	.940842	569	586	.940858	.059142	414	.03	.999983	30
1860	31	7.955082	569	587	7.955100	12.044900	413	.02	9.999982	29
1920	32	.968870	569	587	.968889	.031111	413	.02	.999981	28
1980	33	.982233	568	588	.982253	.017747	412	.02	.999980	27
2040	34	7.995198	568	589	7.995219	12.004781	411	.02	.999979	26
2100	35	8.007787	567	590	8.007809	11.992191	410	.03	.999977	25
2160	36	.020021	567	591	.020044	.979956	409	.02	.999976	24
2220	37	.031919	566	592	.031945	.968055	408	.02	.999975	23
2280	38	.043501	566	593	.043527	.956473	407	.03	.999973	22
2340	39	.054781	566	593	.054809	.945191	407	.02	.999972	21
2400	40	.065776	565	594	.065806	.934194	406	.02	.999971	20
2460	41	8.076500	565	595	8.076531	11.923469	405	.03	9.999969	19
2520	42	.086965	564	596	.086997	.913003	404	.02	.999968	18
2580	43	.097183	564	598	.097217	.902783	402	.03	.999966	17
2640	44	.107167	563	599	.107203	.892797	401	.03	.999964	16
2700	45	.116926	562	600	.116963	.883037	400	.02	.999963	15
2760	46	.126471	562	601	.126510	.873490	399	.03	.999961	14
2820	47	.135810	561	602	.135851	.864149	398	.03	.999959	13
2880	48	.144953	561	603	.144996	.855004	397	.02	.999958	12
2940	49	.153907	560	604	.153952	.846048	396	.03	.999956	11
3000	50	.162681	560	605	.162727	.837273	395	.03	.999954	10
3060	51	8.171280	559	607	8.171328	11.828672	393	.03	9.999952	9
3120	52	.179713	558	608	.179763	.820237	392	.03	.999950	8
3180	53	.187985	558	609	.188036	.811964	391	.03	.999948	7
3240	54	.196102	557	611	.196156	.803844	389	.03	.999946	6
3300	55	.204070	556	612	.204126	.795874	388	.03	.999944	5
3360	56	.211895	556	613	.211953	.788047	387	.03	.999942	4
3420	57	.219581	555	615	.219641	.780359	385	.03	.999940	3
3480	58	.227134	554	616	.227195	.772805	384	.03	.999938	2
3540	59	.234557	554	618	.234621	.765379	382	.03	.999936	1
3600	60	8.241855	553	619	8.241921	11.758079	381	.03	9.999934	0
			4.685				15.314			
"	'	Cosine.			Cotang.	Tang.		D 1"	Sine.	'

″	′	Sine.	S	T	Tang.	Cotang.	C	D 1″	Cosine.
			4.685				15.314		
3600	0	8.241855	553	619	8.241921	11.758079	381	.03	9.999934
3660	1	.249033	552	620	.249102	.750898	380	.05	.999932
3720	2	.256094	551	622	.256165	.743835	378	.03	.999929
3780	3	.263042	551	623	.263115	.736885	377	.03	.999927
3840	4	.269881	550	625	.269956	.730044	375	.05	.999925
3900	5	.276614	549	627	.276691	.723309	373	.03	.999922
3960	6	.283243	548	628	.283323	.716677	372	.03	.999920
4020	7	.289773	547	630	.289856	.710144	370	.05	.999918
4080	8	.296207	546	632	.296292	.703708	368	.03	.999915
4140	9	.302546	546	633	.302634	.697366	367	.05	.999913
4200	10	.308794	545	635	.308884	.691116	365	.05	.999910
4260	11	8.314954	544	637	8.315046	11.684954	363	.03	9.999907
4320	12	.321027	543	638	.321122	.678878	362	.05	.999905
4380	13	.327016	542	640	.327114	.672886	360	.05	.999902
4440	14	.332924	541	642	.333025	.666975	358	.03	.999899
4500	15	.338753	540	644	.338856	.661144	356	.05	.999897
4560	16	.344504	539	646	.344610	.655390	354	.05	.999894
4620	17	.350181	539	648	.350289	.649711	352	.05	.999891
4680	18	.355783	538	649	.355895	.644105	351	.05	.999888
4740	19	.361315	537	651	.361430	.638570	349	.05	.999885
4800	20	.366777	536	653	.366895	.633105	347	.05	.999882
4860	21	8.372171	535	655	8.372292	11.627708	345	.05	9.999879
4920	22	.377499	534	657	.377622	.622378	343	.05	.999876
4980	23	.382762	533	659	.382889	.617111	341	.05	.999873
5040	24	.387962	532	661	.388092	.611908	339	.05	.999870
5100	25	.393101	531	663	.393234	.606766	337	.05	.999867
5160	26	.398179	530	666	.398315	.601685	334	.05	.999864
5220	27	.403199	529	668	.403338	.596662	332	.05	.999861
5280	28	.408161	527	670	.408304	.591696	330	.07	.999858
5340	29	.413068	526	672	.413213	.586787	328	.05	.999854
5400	30	.417919	525	674	.418068	.581932	326	.05	.999851
5460	31	8.422717	524	676	8.422869	11.577131	324	.07	9.999848
5520	32	.427462	523	679	.427618	.572382	321	.05	.999844
5580	33	.432156	522	681	.432315	.567685	319	.05	.999841
5640	34	.436800	521	683	.436962	.563038	317	.07	.999838
5700	35	.441394	520	685	.441560	.558440	315	.05	.999834
5760	36	.445941	518	688	.446110	.553890	312	.07	.999831
5820	37	.450440	517	690	.450613	.549387	310	.05	.999827
5880	38	.454893	516	693	.455070	.544930	307	.07	.999824
5940	39	.459301	515	695	.459481	.540519	305	.07	.999820
6000	40	.463665	514	697	.463849	.536151	303	.05	.999816
6060	41	8.467985	512	700	8.468172	11.531828	300	.07	9.999813
6120	42	.472263	511	702	.472454	.527546	298	.07	.999809
6180	43	.476498	510	705	.476693	.523307	295	.07	.999805
6240	44	.480693	509	707	.480892	.519108	293	.07	.999801
6300	45	.484848	507	710	.485050	.514950	290	.05	.999797
6360	46	.488963	506	713	.489170	.510830	287	.07	.999794
6420	47	.493040	505	715	.493250	.506750	285	.07	.999790
6480	48	.497078	503	718	.497293	.502707	282	.07	.999786
6540	49	.501080	502	720	.501298	.498702	280	.07	.999782
6600	50	.505045	501	723	.505267	.494733	277	.07	.999778
6660	51	8.508974	499	726	8.509200	11.490800	274	.08	9.999774
6720	52	.512867	498	729	.513098	.486902	271	.07	.999769
6780	53	.516726	497	731	.516961	.483039	269	.07	.999765
6840	54	.520551	495	734	.520790	.479210	266	.07	.999761
6900	55	.524343	494	737	.524586	.475414	263	.07	.999757
6960	56	.528102	492	740	.528349	.471651	260	.08	.999753
7020	57	.531828	491	743	.532080	.467920	257	.07	.999748
7080	58	.535523	490	745	.535779	.464221	255	.07	.999744
7140	59	.539186	488	748	.539447	.460553	252	.08	.999740
7200	60	8.542819	487	751	8.543084	11.456916	249		9.999735
			4.685				15.314		
″	′	Cosine.			Cotang.	Tang.		D 1″	Sine.

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	8 542819	60.05	9.999735	.07	8.543084	60.12	11.456916	60
1	.546422	59.55	.999731	.08	.546691	59.62	.453309	59
2	.549995	59.07	.999726	.07	.550268	59.15	.449732	58
3	.553539	58.58	.999722	.08	.553817	58.65	.446183	57
4	.557054	58.10	.999717	.07	.557336	58.20	.442664	56
5	.560540	57.65	.999713	.08	.560828	57.72	.439172	55
6	.563999	57.20	.999708	.07	.564291	57.27	.435709	54
7	.567431	56.75	.999704	.08	.567727	56.83	.432273	53
8	.570836	56.30	.999699	.08	.571137	56.38	.428863	52
9	.574214	55.87	.999694	.08	.574520	55.95	.425480	51
10	.577566	55.43	.999689	.07	.577877	55.52	.422123	50
11	8.580892	55.02	9.999685	.08	8.581208	55.10	11.418792	49
12	.584193	54.60	.999680	.08	.584514	54.68	.415486	48
13	.587469	54.20	.999675	.08	.587795	54.27	.412205	47
14	.590721	53.78	.999670	.08	.591051	53.87	.408949	46
15	.593948	53.40	.999665	.08	.594283	53.48	.405717	45
16	.597152	53.00	.999660	.08	.597492	53.08	.402508	44
17	.600332	52.62	.999655	.08	.600677	52.70	.399323	43
18	.603489	52.23	.999650	.08	.603839	52.32	.396161	42
19	.606623	51.85	.999645	.08	.606978	51.98	.393022	41
20	.609734	51.48	.999640	.08	.610094	51.58	.389906	40
21	8.612823	51.13	9.999635	.10	8.613189	51.22	11.386811	39
22	.615891	50.77	.999629	.08	.616262	50.85	.383738	38
23	.618937	50.42	.999624	.08	.619313	50.50	.380687	37
24	.621962	50.05	.999619	.08	.622343	50.15	.377657	36
25	.624965	49.72	.999614	.10	.625352	49.80	.374648	35
26	.627948	49.38	.999608	.08	.628340	49.47	.371660	34
27	.630911	49.05	.999603	.10	.631308	49.13	.368692	33
28	.633854	48.70	.999597	.08	.634256	48.80	.365744	32
29	.636776	48.40	.999592	.10	.637184	48.48	.362816	31
30	.639680	48.05	.999586	.08	.640093	48.15	.359907	30
31	8.642563	47.75	9.999581	.10	8.642982	47.85	11.357018	29
32	.645428	47.43	.999575	.08	.645853	47.52	.354147	28
33	.648274	47.13	.999570	.10	.648704	47.22	.351296	27
34	.651102	46.82	.999564	.10	.651537	46.92	.348463	26
35	.653911	46.52	.999558	.08	.654352	46.62	.345648	25
36	.656702	46.22	.999553	.10	.657149	46.32	.342851	24
37	.659475	45.92	.999547	.10	.659928	46.02	.340072	23
38	.662230	45.63	.999541	.10	.662689	45.73	.337311	22
39	.664968	45.35	.999535	.10	.665433	45.45	.334567	21
40	.667689	45.07	.999529	.08	.668160	45.17	.331840	20
41	8.670393	44.78	9.999524	.10	8.670870	44.88	11.329130	19
42	.673080	44.52	.999518	.10	.673563	44.60	.326437	18
43	.675751	44.23	.999512	.10	.676239	44.35	.323761	17
44	.678405	43.97	.999506	.10	.678900	44.07	.321100	16
45	.681043	43.70	.999500	.12	.681544	43.80	.318456	15
46	.683665	43.45	.999493	.10	.684172	43.53	.315828	14
47	.686272	43.18	.999487	.10	.686784	43.28	.313216	13
48	.688863	42.92	.999481	.10	.689381	43.03	.310619	12
49	.691438	42.67	.999475	.10	.691963	42.77	.308037	11
50	.693998	42.42	.999469	.10	.694529	42.53	.305471	10
51	8.696543	42.17	9.999463	.12	8.697081	42.27	11.302919	9
52	.699073	41.93	.999456	.10	.699617	42.03	.300383	8
53	.701589	41.68	.999450	.12	.702139	41.78	.297861	7
54	.704090	41.45	.999443	.10	.704646	41.57	.295354	6
55	.706577	41.20	.999437	.10	.707140	41.30	.292860	5
56	.709049	40.97	.999431	.12	.709618	41.08	.290382	4
57	.711507	40.75	.999424	.10	.712083	40.85	.287917	3
58	.713952	40.52	.999418	.12	.714534	40.63	.285466	2
59	.716383	40.28	.999411	.12	.716972	40.40	.283028	1
60	8.718800		9.999404		8.719396		11.280604	0
′	Cosine.	D 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	8.718800	40.07	9.999404	.10	8.719396	40.17	11.280604	60
1	.721204	39.85	.999398	.12	.721806	39.97	.278194	59
2	.723595	39.62	.999391	.12	.724204	39.73	.275796	58
3	.725972	39.42	.999384	.10	.726588	39.52	.273412	57
4	.728337	39.18	.999378	.12	.728959	39.30	.271041	56
5	.730688	38.98	.999371	.12	.731317	39.10	.268683	55
6	.733027	38.78	.999364	.12	.733663	38.88	.266337	54
7	.735354	38.55	.999357	.12	.735996	38.68	.264004	53
8	.737667	38.37	.999350	.12	.738317	38.48	.261683	52
9	.739969	38.17	.999343	.12	.740626	38.27	.259374	51
10	.742259	37.95	.999336	.12	.742922	38.08	.257078	50
11	8.744536	37.77	9.999329	.12	8.745207	37.87	11.254793	49
12	.746802	37.55	.999322	.12	.747479	37.68	.252521	48
13	.749055	37.37	.999315	.12	.749740	37.48	.250260	47
14	.751297	37.18	.999308	.12	.751989	37.30	.248011	46
15	.753528	36.98	.999301	.12	.754227	37.10	.245773	45
16	.755747	36.80	.999294	.12	.756453	36.92	.243547	44
17	.757955	36.60	.999287	.13	.758668	36.73	.241332	43
18	.760151	36.43	.999279	.12	.760872	36.55	.239128	42
19	.762337	36.23	.999272	.12	.763065	36.35	.236935	41
20	.764511	36.07	.999265	.13	.765246	36.18	.234754	40
21	8.766675	35.88	9.999257	.12	8.767417	36.02	11.232583	39
22	.768828	35.70	.999250	.13	.769578	35.82	.230422	38
23	.770970	35.52	.999242	.12	.771727	35.65	.228273	37
24	.773101	35.37	.999235	.13	.773866	35.48	.226134	36
25	.775223	35.17	.999227	.12	.775995	35.32	.224005	35
26	.777333	35.02	.999220	.13	.778114	35.13	.221886	34
27	.779434	34.83	.999212	.12	.780222	34.97	.219778	33
28	.781524	34.68	.999205	.13	.782320	34.80	.217680	32
29	.783605	34.50	.999197	.13	.784408	34.63	.215592	31
30	.785675	34.35	.999189	.13	.786486	34.47	.213514	30
31	8.787736	34.18	9.999181	.12	8.788554	34.32	11.211446	29
32	.789787	34.02	.999174	.13	.790613	34.15	.209387	28
33	.791828	33.85	.999166	.13	.792662	33.98	.207338	27
34	.793859	33.70	.999158	.13	.794701	33.83	.205299	26
35	.795881	33.55	.999150	.13	.796731	33.68	.203269	25
36	.797894	33.38	.999142	.13	.798752	33.52	.201248	24
37	.799897	33.25	.999134	.13	.800763	33.37	.199237	23
38	.801892	33.07	.999126	.13	.802765	33.22	.197235	22
39	.803876	32.93	.999118	.13	.804758	33.07	.195242	21
40	.805852	32.78	.999110	.13	.806742	32.92	.193258	20
41	8.807819	32.63	9.999102	.13	8.808717	32.77	11.191283	19
42	.809777	32.48	.999094	.13	.810683	32.63	.189317	18
43	.811726	32.35	.999086	.15	.812641	32.47	.187359	17
44	.813667	32.20	.999077	.13	.814589	32.33	.185411	16
45	.815599	32.05	.999069	.13	.816529	32.20	.183471	15
46	.817522	31.90	.999061	.13	.818461	32.05	.181539	14
47	.819436	31.78	.999053	.15	.820384	31.90	.179616	13
48	.821343	31.62	.999044	.13	.822298	31.78	.177702	12
49	.823240	31.50	.999036	.15	.824205	31.63	.175795	11
50	.825130	31.35	.999027	.13	.826103	31.48	.173897	10
51	8.827011	31.22	9.999019	.15	8.827992	31.37	11.172008	9
52	.828884	31.08	.999010	.13	.829874	31.23	.170126	8
53	.830749	30.97	.999002	.15	.831748	31.08	.168252	7
54	.832607	30.82	.998993	.15	.833613	30.97	.166387	6
55	.834456	30.68	.998984	.13	.835471	30.83	.164529	5
56	.836297	30.55	.998976	.15	.837321	30.70	.162679	4
57	.838130	30.43	.998967	.15	.839163	30.58	.160837	3
58	.839956	30.30	.998958	.13	.840998	30.45	.159002	2
59	.841774	30.18	.998950	.15	.842825	30.32	.157175	1
60	8.843585		9.998941		8.844644		11.155356	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	8.843585	30.03	9.998941	.15	8.844644	30.18	11.155356	60
1	.845387	29.93	.998932	.15	.846455	30.08	.153545	59
2	.847183	29.80	.998923	.15	.848260	29.95	.151740	58
3	.848971	29.67	.998914	.15	.850057	29.82	.149943	57
4	.850751	29.57	.998905	.15	.851846	29.70	.148154	56
5	.852525	29.43	.998896	.15	.853628	29.58	.146372	55
6	.854291	29.30	.998887	.15	.855403	29.47	.144597	54
7	.856049	29.20	.998878	.15	.857171	29.35	.142829	53
8	.857801	29.08	.998869	.15	.858932	29.23	.141068	52
9	.859546	28.95	.998860	.15	.860686	29.12	.139314	51
10	.861283	28.85	.998851	.17	.862433	29.00	.137567	50
11	8.863014	28.73	9.998841	.15	8.864173	28.88	11.135827	49
12	.864738	28.62	.998832	.15	.865906	28.77	.134094	48
13	.866455	28.50	.998823	.17	.867632	28.65	.132368	47
14	.868165	28.38	.998813	.15	.869351	28.55	.130649	46
15	.869868	28.28	.998804	.15	.871064	28.43	.128936	45
16	.871565	28.17	.998795	.17	.872770	28.32	.127230	44
17	.873255	28.05	.998785	.15	.874469	28.22	.125531	43
18	.874938	27.95	.998776	.17	.876162	28.12	.123838	42
19	.876615	27.83	.998766	.15	.877849	28.00	.122151	41
20	.878285	27.73	.998757	.17	.879529	27.88	.120471	40
21	8.879949	27.63	9.998747	.15	8.881202	27.78	11.118798	39
22	.881607	27.52	.998738	.17	.882869	27.68	.117131	38
23	.883258	27.42	.998728	.17	.884530	27.58	.115470	37
24	.884903	27.32	.998718	.17	.886185	27.47	.113815	36
25	.886542	27.20	.998708	.15	.887833	27.38	.112167	35
26	.888174	27.12	.998699	.17	.889476	27.27	.110524	34
27	.889801	27.00	.998689	.17	.891112	27.17	.108888	33
28	.891421	26.90	.998679	.17	.892742	27.07	.107258	32
29	.893035	26.80	.998669	.17	.894366	26.97	.105634	31
30	.894643	26.72	.998659	.17	.895984	26.87	.104016	30
31	8.896246	26.60	9.998649	.17	8.897596	26.78	11.102404	29
32	.897842	26.50	.998639	.17	.899203	26.67	.100797	28
33	.899432	26.42	.998629	.17	.900803	26.58	.099197	27
34	.901017	26.32	.998619	.17	.902398	26.48	.097602	26
35	.902596	26.22	.998609	.17	.903987	26.38	.096013	25
36	.904169	26.12	.998599	.17	.905570	26.28	.094430	24
37	.905736	26.02	.998589	.18	.907147	26.20	.092853	23
38	.907297	25.93	.998578	.17	.908719	26.10	.091281	22
39	.908853	25.85	.998568	.17	.910285	26.02	.089715	21
40	.910404	25.75	.998558	.17	.911846	25.92	.088154	20
41	8.911949	25.65	9.998548	.18	8.913401	25.83	11.086599	19
42	.913488	25.57	.998537	.17	.914951	25.73	.085049	18
43	.915022	25.47	.998527	.18	.916495	25.63	.083505	17
44	.916550	25.38	.998516	.17	.918034	25.57	.081966	16
45	.918073	25.30	.998506	.18	.919568	25.47	.080432	15
46	.919591	25.20	.998495	.17	.921096	25.38	.078904	14
47	.921103	25.12	.998485	.18	.922619	25.28	.077381	13
48	.922610	25.03	.998474	.17	.924136	25.22	.075864	12
49	.924112	24.95	.998464	.18	.925649	25.12	.074351	11
50	.925609	24.85	.998453	.18	.927156	25.03	.072844	10
51	8.927100	24.78	9.998442	.18	8.928658	24.95	11.071342	9
52	.928587	24.68	.998431	.17	.930155	24.87	.069845	8
53	.930068	24.60	.998421	.18	.931647	24.78	.068353	7
54	.931544	24.52	.998410	.18	.933134	24.70	.066866	6
55	.933015	24.43	.998399	.18	.934616	24.62	.065384	5
56	.934481	24.35	.998388	.18	.936093	24.53	.063907	4
57	.935942	24.27	.998377	.18	.937565	24.45	.062435	3
58	.937398	24.20	.998366	.18	.939032	24.37	.060968	2
59	.938850	24.10	.998355	.18	.940494	24.30	.059506	1
60	8.940296		9.998344		8.941952		11.058048	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.
0	8.940296	24.08	9.998344	.18	8.941952	24.20	11.058048
1	.941738	23.98	.998333	.18	.943404	24.13	.056596
2	.943174	23.87	.998322	.18	.944852	24.05	.055148
3	.944606	23.80	.998311	.18	.946295	23.98	.053705
4	.946034	23.70	.998300	.18	.947734	23.90	.052266
5	.947456	23.63	.998289	.20	.949168	23.82	.050832
6	.948874	23.55	.998277	.18	.950597	23.73	.049403
7	.950287	23.48	.998266	.18	.952021	23.67	.047979
8	.951696	23.40	.998255	.20	.953441	23.58	.046559
9	.953100	23.32	.998243	.18	.954856	23.52	.045144
10	.954499	23.25	.998232	.20	.956267	23.45	.043733
11	8.955894	23.17	9.998220	.18	8.957674	23.35	11.042326
12	.957284	23.10	.998209	.20	.959075	23.30	.040925
13	.958670	23.03	.998197	.18	.960473	23.22	.039527
14	.960052	22.95	.998186	.20	.961866	23.15	.038134
15	.961429	22.87	.998174	.18	.963255	23.07	.036745
16	.962801	22.82	.998163	.20	.964639	23.00	.035361
17	.964170	22.73	.998151	.20	.966019	22.92	.033981
18	.965534	22.65	.998139	.18	.967394	22.87	.032606
19	.966893	22.60	.998128	.20	.968766	22.78	.031234
20	.968249	22.52	.998116	.20	.970133	22.72	.029867
21	8.969600	22.45	9.998104	.20	8.971496	22.65	11.028504
22	.970947	22.37	.998092	.20	.972855	22.57	.027145
23	.972289	22.32	.998080	.20	.974209	22.52	.025791
24	.973628	22.23	.998068	.20	.975560	22.43	.024440
25	.974962	22.18	.998056	.20	.976906	22.37	.023094
26	.976293	22.10	.998044	.20	.978248	22.30	.021752
27	.977619	22.03	.998032	.20	.979586	22.25	.020414
28	.978941	21.97	.998020	.20	.980921	22.17	.019079
29	.980259	21.90	.998008	.20	.982251	22.10	.017749
30	.981573	21.83	.997996	.20	.983577	22.03	.016423
31	8.982883	21.77	9.997984	.20	8.984899	21.97	11.015101
32	.984189	21.72	.997972	.22	.986217	21.92	.013783
33	.985491	21.63	.997959	.20	.987532	21.83	.012468
34	.986789	21.57	.997947	.20	.988842	21.78	.011158
35	.988083	21.52	.997935	.22	.990149	21.70	.009851
36	.989374	21.43	.997922	.20	.991451	21.65	.008549
37	.990660	21.38	.997910	.22	.992750	21.58	.007250
38	.991943	21.32	.997897	.20	.994045	21.53	.005955
39	.993222	21.25	.997885	.22	.995337	21.45	.004663
40	.994497	21.18	.997872	.20	.996624	21.40	.003376
41	8.995768	21.13	9.997860	.22	8.997908	21.33	11.002092
42	.997036	21.05	.997847	.20	8.999188	21.28	11.000812
43	.998299	21.02	.997835	.22	9.000465	21.22	10.999535
44	8.999560	20.93	.997822	.22	.001738	21.15	.998262
45	9.000816	20.88	.997809	.20	.003007	21.08	.996993
46	.002069	20.82	.997797	.22	.004272	21.03	.995728
47	.003318	20.75	.997784	.22	.005534	20.97	.994466
48	.004563	20.70	.997771	.22	.006792	20.92	.993208
49	.005805	20.65	.997758	.22	.008047	20.85	.991953
50	.007044	20.57	.997745	.22	.009298	20.80	.990702
51	9.008278	20.53	9.997732	.22	9.010546	20.73	10.989454
52	.009510	20.45	.997719	.22	.011790	20.68	.988210
53	.010737	20.42	.997706	.22	.013031	20.62	.986969
54	.011962	20.33	.997693	.22	.014268	20.57	.985732
55	.013182	20.30	.997680	.22	.015502	20.50	.984498
56	.014400	20.22	.997667	.22	.016732	20.45	.983268
57	.015613	20.18	.997654	.22	.017959	20.40	.982041
58	.016824	20.12	.997641	.22	.019183	20.33	.980817
59	.018031	20.07	.997628	.23	.020403	20.28	.979597
60	9.019235		9.997614		9.021620		10.978380
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.019235	20.00	9.997614	.22	9.021620	20.23	10.978380	60
1	.020435	19.95	.997601	.22	.022834	20.17	.977166	59
2	.021632	19.88	.997588	.23	.024044	20.12	.975956	58
3	.022825	19.85	.997574	.22	.025251	20.07	.974749	57
4	.024016	19.78	.997561	.23	.026455	20.00	.973545	56
5	.025203	19.72	.997547	.22	.027655	19.95	.972345	55
6	.026386	19.68	.997534	.23	.028852	19.90	.971148	54
7	.027567	19.62	.997520	.22	.030046	19.85	.969954	53
8	.028744	19.57	.997507	.23	.031237	19.80	.968763	52
9	.029918	19.52	.997493	.22	.032425	19.73	.967575	51
10	.031089	19.47	.997480	.23	.033609	19.70	.966391	50
11	9.032257	19.40	9.997466	.23	9.034791	19.63	10.965209	49
12	.033421	19.35	.997452	.22	.035969	19.58	.964031	48
13	.034582	19.32	.997439	.23	.037144	19.53	.962856	47
14	.035741	19.25	.997425	.23	.038316	19.48	.961684	46
15	.036896	19.20	.997411	.23	.039485	19.43	.960515	45
16	.038048	19.15	.997397	.23	.040651	19.37	.959349	44
17	.039197	19.08	.997383	.23	.041813	19.33	.958187	43
18	.040342	19.05	.997369	.23	.042973	19.28	.957027	42
19	.041485	19.00	.997355	.23	.044130	19.23	.955870	41
20	.042625	18.95	.997341	.23	.045284	19.17	.954716	40
21	9.043762	18.88	9.997327	.23	9.046434	19.13	10.953566	39
22	.044895	18.85	.997313	.23	.047582	19.08	.952418	38
23	.046026	18.80	.997299	.23	.048727	19.03	.951273	37
24	.047154	18.75	.997285	.23	.049869	18.98	.950131	36
25	.048279	18.68	.997271	.23	.051008	18.93	.948992	35
26	.049400	18.65	.997257	.25	.052144	18.88	.947856	34
27	.050519	18.60	.997242	.23	.053277	18.83	.946723	33
28	.051635	18.57	.997228	.23	.054407	18.80	.945593	32
29	.052749	18.50	.997214	.25	.055535	18.73	.944465	31
30	.053859	18.45	.997199	.23	.056659	18.70	.943341	30
31	9.054966	18.42	9.997185	.25	9.057781	18.65	10.942219	29
32	.056071	18.35	.997170	.23	.058900	18.60	.941100	28
33	.057172	18.32	.997156	.25	.060016	18.57	.939984	27
34	.058271	18.27	.997141	.23	.061130	18.50	.938870	26
35	.059367	18.22	.997127	.25	.062240	18.47	.937760	25
36	.060460	18.18	.997112	.23	.063348	18.42	.936652	24
37	.061551	18.13	.997098	.25	.064453	18.38	.935547	23
38	.062639	18.08	.997083	.25	.065556	18.32	.934444	22
39	.063724	18.03	.997068	.25	.066655	18.28	.933345	21
40	.064806	17.98	.997053	.23	.067752	18.25	.932248	20
41	9.065885	17.95	9.997039	.25	9.068846	18.20	10.931154	19
42	.066962	17.90	.997024	.25	.069938	18.15	.930062	18
43	.068036	17.85	.997009	.25	.071027	18.10	.928973	17
44	.069107	17.82	.996994	.25	.072113	18.07	.927887	16
45	.070176	17.77	.996979	.25	.073197	18.02	.926803	15
46	.071242	17.73	.996964	.25	.074278	17.97	.925722	14
47	.072306	17.67	.996949	.25	.075356	17.93	.924644	13
48	.073366	17.63	.996934	.25	.076432	17.88	.923568	12
49	.074424	17.60	.996919	.25	.077505	17.85	.922495	11
50	.075480	17.55	.996904	.25	.078576	17.80	.921424	10
51	9.076533	17.50	9.996889	.25	9.079644	17.77	10.920356	9
52	.077583	17.47	.996874	.27	.080710	17.72	.919290	8
53	.078631	17.42	.996858	.25	.081773	17.67	.918227	7
54	.079676	17.38	.996843	.27	.082833	17.63	.917167	6
55	.080719	17.33	.996828	.27	.083891	17.60	.916109	5
56	.081759	17.30	.996812	.25	.084947	17.55	.915053	4
57	.082797	17.25	.996797	.25	.086000	17.50	.914000	3
58	.083832	17.20	.996782	.27	.087050	17.47	.912950	2
59	.084864	17.17	.996766	.25	.088098	17.43	.911902	1
60	9.085894		9.996751		9.089144		10.910856	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	
0	9.085894	17.13	9.996751	.27	9.089144	17.38	10.910856	60
1	.086922	17.08	.996735	.25	.090187	17.35	.909813	59
2	.087947	17.05	.996720	.27	.091228	17.30	.908772	58
3	.088970	17.00	.996704	.27	.092266	17.27	.907734	57
4	.089990	16.97	.996688	.25	.093302	17.23	.906698	56
5	.091008	16.93	.996673	.27	.094336	17.18	.905664	55
6	.092024	16.88	.996657	.27	.095367	17.13	.904633	54
7	.093037	16.83	.996641	.27	.096395	17.12	.903605	53
8	.094047	16.82	.996625	.25	.097422	17.07	.902578	52
9	.095056	16.77	.996610	.27	.098446	17.03	.901554	51
10	.096062	16.72	.996594	.27	.099468	16.98	.900532	50
11	9.097065	16.68	9.996578	.27	9.100487	16.95	10.899513	49
12	.098066	16.65	.996562	.27	.101504	16.92	.898496	48
13	.099065	16.62	.996546	.27	.102519	16.88	.897481	47
14	.100062	16.57	.996530	.27	.103532	16.83	.896468	46
15	.101056	16.53	.996514	.27	.104542	16.80	.895458	45
16	.102048	16.48	.996498	.27	.105550	16.77	.894450	44
17	.103037	16.47	.996482	.28	.106556	16.72	.893444	43
18	.104025	16.42	.996465	.27	.107559	16.68	.892441	42
19	.105010	16.37	.996449	.27	.108560	16.65	.891440	41
20	.105992	16.35	.996433	.27	.109559	16.62	.890441	40
21	9.106973	16.30	9.996417	.28	9.110556	16.58	10.889444	39
22	.107951	16.27	.996400	.27	.111551	16.53	.888449	38
23	.108927	16.23	.996384	.27	.112543	16.50	.887457	37
24	.109901	16.20	.996368	.28	.113533	16.47	.886467	36
25	.110873	16.15	.996351	.27	.114521	16.43	.885479	35
26	.111842	16.12	.996335	.28	.115507	16.40	.884493	34
27	.112809	16.08	.996318	.27	.116491	16.35	.883509	33
28	.113774	16.05	.996302	.28	.117472	16.33	.882528	32
29	.114737	16.02	.996285	.27	.118452	16.28	.881548	31
30	.115698	15.97	.996269	.28	.119429	16.25	.880571	30
31	9.116656	15.95	9.996252	.28	9.120404	16.22	10.879596	29
32	.117613	15.90	.996235	.27	.121377	16.18	.878623	28
33	.118567	15.87	.996219	.28	.122348	16.15	.877652	27
34	.119519	15.83	.996202	.28	.123317	16.12	.876683	26
35	.120469	15.80	.996185	.28	.124284	16.08	.875716	25
36	.121417	15.75	.996168	.28	.125249	16.03	.874751	24
37	.122362	15.73	.996151	.28	.126211	16.02	.873789	23
38	.123306	15.70	.996134	.28	.127172	15.97	.872828	22
39	.124248	15.65	.996117	.28	.128130	15.95	.871870	21
40	.125187	15.63	.996100	.28	.129087	15.90	.870913	20
41	9.126125	15.58	9.996083	.28	9.130041	15.88	10.869959	19
42	.127060	15.55	.996066	.28	.130994	15.83	.869006	18
43	.127993	15.53	.996049	.28	.131944	15.82	.868056	17
44	.128925	15.48	.996032	.28	.132893	15.77	.867107	16
45	.129854	15.45	.996015	.28	.133839	15.75	.866161	15
46	.130781	15.42	.995998	.30	.134784	15.70	.865216	14
47	.131706	15.40	.995980	.28	.135726	15.68	.864274	13
48	.132630	15.35	.995963	.28	.136667	15.63	.863333	12
49	.133551	15.32	.995946	.30	.137605	15.62	.862395	11
50	.134470	15.28	.995928	.28	.138542	15.57	.861458	10
51	9.135387	15.27	9.995911	.28	9.139476	15.55	10.860524	9
52	.136303	15.22	.995894	.30	.140409	15.52	.859591	8
53	.137216	15.20	.995876	.28	.141340	15.48	.858660	7
54	.138128	15.15	.995859	.30	.142269	15.45	.857731	6
55	.139037	15.12	.995841	.30	.143196	15.42	.856804	5
56	.139944	15.10	.995823	.28	.144121	15.38	.855879	4
57	.140850	15.07	.995806	.30	.145044	15.37	.854956	3
58	.141754	15.02	.995788	.28	.145966	15.32	.854034	2
59	.142655	15.00	.995771	.30	.146885	15.30	.853115	1
60	9.143555		9.995753		9.147803		10.852197	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.143555	14.97	9.995753	.30	9.147803	15.25	10.852197	60
1	.144453	14.93	.995735	.30	.148718	15.23	.851282	59
2	.145349	14.90	.995717	.30	.149632	15.20	.850368	58
3	.146243	14.88	.995699	.30	.150544	15.17	.849456	57
4	.147136	14.83	.995681	.28	.151454	15.15	.848546	56
5	.148026	14.82	.995664	.30	.152363	15.10	.847637	55
6	.148915	14.78	.995646	.30	.153269	15.08	.846731	54
7	.149802	14.73	.995628	.30	.154174	15.05	.845826	53
8	.150686	14.72	.995610	.32	.155077	15.02	.844923	52
9	.151569	14.70	.995591	.30	.155978	14.98	.844022	51
10	.152451	14.65	.995573	.30	.156877	14.97	.843123	50
11	9.153330	14.63	9.995555	.30	9.157775	14.93	10.842225	49
12	.154208	14.58	.995537	.30	.158671	14.90	.841329	48
13	.155083	14.57	.995519	.30	.159565	14.87	.840435	47
14	.155957	14.55	.995501	.32	.160457	14.83	.839543	46
15	.156830	14.50	.995482	.30	.161347	14.82	.838653	45
16	.157700	14.48	.995464	.30	.162236	14.78	.837764	44
17	.158569	14.43	.995446	.32	.163123	14.75	.836877	43
18	.159435	14.43	.995427	.30	.164008	14.73	.835992	42
19	.160301	14.38	.995409	.32	.164892	14.70	.835108	41
20	.161164	14.35	.995390	.30	.165774	14.67	.834226	40
21	9.162025	14.33	9.995372	.32	9.166654	14.63	10.833346	39
22	.162885	14.30	.995353	.32	.167532	14.62	.832468	38
23	.163743	14.28	.995334	.30	.168409	14.58	.831591	37
24	.164600	14.23	.995316	.32	.169284	14.55	.830716	36
25	.165454	14.22	.995297	.32	.170157	14.53	.829843	35
26	.166307	14.20	.995278	.30	.171029	14.50	.828971	34
27	.167159	14.15	.995260	.32	.171899	14.47	.828101	33
28	.168008	14.13	.995241	.32	.172767	14.45	.827233	32
29	.168856	14.10	.995222	.32	.173634	14.42	.826366	31
30	.169702	14.08	.995203	.32	.174499	14.38	.825501	30
31	9.170547	14.03	9.995184	.32	9.175362	14.37	10.824638	29
32	.171389	14.02	.995165	.32	.176224	14.33	.823776	28
33	.172230	14.00	.995146	.32	.177084	14.30	.822916	27
34	.173070	13.97	.995127	.32	.177942	14.28	.822058	26
35	.173908	13.93	.995108	.32	.178799	14.27	.821201	25
36	.174744	13.90	.995089	.32	.179655	14.22	.820345	24
37	.175578	13.88	.995070	.32	.180508	14.20	.819492	23
38	.176411	13.85	.995051	.32	.181360	14.18	.818640	22
39	.177242	13.83	.995032	.32	.182211	14.13	.817789	21
40	.178072	13.80	.995013	.33	.183059	14.13	.816941	20
41	9.178900	13.77	9.994993	.32	9.183907	14.08	10.816093	19
42	.179726	13.75	.994974	.32	.184752	14.08	.815248	18
43	.180551	13.72	.994955	.33	.185597	14.03	.814403	17
44	.181374	13.70	.994935	.32	.186439	14.02	.813561	16
45	.182196	13.67	.994916	.33	.187280	14.00	.812720	15
46	.183016	13.63	.994896	.32	.188120	13.97	.811880	14
47	.183834	13.62	.994877	.33	.188958	13.93	.811042	13
48	.184651	13.58	.994857	.32	.189794	13.92	.810206	12
49	.185466	13.57	.994838	.33	.190629	13.88	.809371	11
50	.186280	13.53	.994818	.33	.191462	13.87	.808538	10
51	9.187092	13.52	9.994798	.32	9.192294	13.83	10.807706	9
52	.187903	13.48	.994779	.33	.193124	13.82	.806876	8
53	.188712	13.45	.994759	.33	.193953	13.78	.806047	7
54	.189519	13.43	.994739	.32	.194780	13.77	.805220	6
55	.190325	13.42	.994720	.33	.195606	13.73	.804394	5
56	.191130	13.38	.994700	.33	.196430	13.72	.803570	4
57	.191933	13.35	.994680	.33	.197253	13.68	.802747	3
58	.192734	13.33	.994660	.33	.198074	13.67	.801926	2
59	.193534	13.30	.994640	.33	.198894	13.65	.801106	1
60	9.194332		9.994620		9.199713		10.800287	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.194332	13.28	9.994620	.33	9.199713	13.60	10.800287	60
1	.195129	13.27	.994600	.33	.200529	13.60	.799471	59
2	.195925	13.23	.994580	.33	.201345	13.57	.798655	58
3	.196719	13.20	.994560	.33	.202159	13.53	.797841	57
4	.197511	13.18	.994540	.35	.202971	13.52	.797029	56
5	.198302	13.15	.994519	.33	.203782	13.50	.796218	55
6	.199091	13.13	.994499	.33	.204592	13.47	.795408	54
7	.199879	13.12	.994479	.33	.205400	13.45	.794600	53
8	.200666	13.08	.994459	.35	.206207	13.43	.793793	52
9	.201451	13.05	.994438	.33	.207013	13.40	.792987	51
10	.202234	13.05	.994418	.33	.207817	13.37	.792183	50
11	9.203017	13.00	9.994398	.35	9.208619	13.35	10.791381	49
12	.203797	13.00	.994377	.33	.209420	13.33	.790580	48
13	.204577	12.95	.994357	.35	.210220	13.30	.789780	47
14	.205354	12.95	.994336	.33	.211018	13.28	.788982	46
15	.206131	12.92	.994316	.35	.211815	13.27	.788185	45
16	.206906	12.88	.994295	.35	.212611	13.23	.787389	44
17	.207679	12.88	.994274	.33	.213405	13.22	.786595	43
18	.208452	12.83	.994254	.35	.214198	13.18	.785802	42
19	.209222	12.83	.994233	.35	.214989	13.18	.785011	41
20	.209992	12.80	.994212	.35	.215780	13.13	.784220	40
21	9.210760	12.77	9.994191	.33	9.216568	13.13	10.783432	39
22	.211526	12.75	.994171	.35	.217356	13.10	.782644	38
23	.212291	12.73	.994150	.35	.218142	13.07	.781858	37
24	.213055	12.72	.994129	.35	.218926	13.07	.781074	36
25	.213818	12.68	.994108	.35	.219710	13.03	.780290	35
26	.214579	12.65	.994087	.35	.220492	13.00	.779508	34
27	.215338	12.65	.994066	.35	.221272	13.00	.778728	33
28	.216097	12.62	.994045	.35	.222052	12.97	.777948	32
29	.216854	12.58	.994024	.35	.222830	12.95	.777170	31
30	.217609	12.57	.994003	.35	.223607	12.92	.776393	30
31	9.218363	12.55	9.993982	.37	9.224382	12.90	10.775618	29
32	.219116	12.53	.993960	.35	.225156	12.88	.774844	28
33	.219868	12.50	.993939	.35	.225929	12.85	.774071	27
34	.220618	12.48	.993918	.35	.226700	12.85	.773300	26
35	.221367	12.47	.993897	.37	.227471	12.80	.772529	25
36	.222115	12.43	.993875	.35	.228239	12.80	.771761	24
37	.222861	12.42	.993854	.37	.229007	12.77	.770993	23
38	.223606	12.38	.993832	.35	.229773	12.77	.770227	22
39	.224349	12.38	.993811	.37	.230539	12.72	.769461	21
40	.225092	12.35	.993789	.35	.231302	12.72	.768698	20
41	9.225833	12.33	9.993768	.37	9.232065	12.68	10.767935	19
42	.226573	12.30	.993746	.35	.232826	12.67	.767174	18
43	.227311	12.28	.993725	.37	.233586	12.65	.766414	17
44	.228048	12.27	.993703	.37	.234345	12.63	.765655	16
45	.228784	12.23	.993681	.35	.235103	12.60	.764897	15
46	.229518	12.23	.993660	.37	.235859	12.58	.764141	14
47	.230252	12.20	.993638	.37	.236614	12.57	.763386	13
48	.230984	12.18	.993616	.37	.237368	12.53	.762632	12
49	.231715	12.15	.993594	.37	.238120	12.53	.761880	11
50	.232444	12.13	.993572	.37	.238872	12.50	.761128	10
51	9.233172	12.12	9.993550	.37	9.239622	12.48	10.760378	9
52	.233899	12.10	.993528	.37	.240371	12.45	.759629	8
53	.234625	12.07	.993506	.37	.241118	12.45	.758882	7
54	.235349	12.07	.993484	.37	.241865	12.42	.758135	6
55	.236073	12.03	.993462	.37	.242610	12.40	.757390	5
56	.236795	12.00	.993440	.37	.243354	12.38	.756646	4
57	.237515	12.00	.993418	.37	.244097	12.37	.755903	3
58	.238235	11.97	.993396	.37	.244839	12.33	.755161	2
59	.238953	11.95	.993374	.38	.245579	12.33	.754421	1
60	9.239670		9.993351		9.246319		10.753681	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.239670	11.93	9.993351	.37	9.246319	12.30	10.753681	60
1	.240386	11.92	.993329	.37	.247057	12.28	.752943	59
2	.241101	11.88	.993307	.38	.247794	12.27	.752206	58
3	.241814	11.87	.993284	.37	.248530	12.23	.751470	57
4	.242526	11.85	.993262	.37	.249264	12.23	.750736	56
5	.243237	11.83	.993240	.38	.249998	12.20	.750002	55
6	.243947	11.82	.993217	.37	.250730	12.18	.749270	54
7	.244656	11.78	.993195	.38	.251461	12.17	.748539	53
8	.245363	11.77	.993172	.38	.252191	12.15	.747809	52
9	.246069	11.77	.993149	.37	.252920	12.13	.747080	51
10	.246775	11.72	.993127	.38	.253648	12.10	.746352	50
11	9.247478	11.72	9.993104	.38	9.254374	12.10	10.745626	49
12	.248181	11.70	.993081	.37	.255100	12.07	.744900	48
13	.248883	11.67	.993059	.38	.255824	12.05	.744176	47
14	.249583	11.65	.993036	.38	.256547	12.03	.743453	46
15	.250282	11.63	.993013	.38	.257269	12.02	.742731	45
16	.250980	11.62	.992990	.38	.257990	12.00	.742010	44
17	.251677	11.60	.992967	.38	.258710	11.98	.741290	43
18	.252373	11.57	.992944	.38	.259429	11.95	.740571	42
19	.253067	11.57	.992921	.38	.260146	11.95	.739854	41
20	.253761	11.53	.992898	.38	.260863	11.92	.739137	40
21	9.254453	11.52	9.992875	.38	9.261578	11.90	10.738422	39
22	.255144	11.50	.992852	.38	.262292	11.88	.737708	38
23	.255834	11.48	.992829	.38	.263005	11.87	.736995	37
24	.256523	11.47	.992806	.38	.263717	11.85	.736283	36
25	.257211	11.45	.992783	.40	.264428	11.83	.735572	35
26	.257898	11.42	.992759	.38	.265138	11.82	.734862	34
27	.258583	11.42	.992736	.38	.265847	11.80	.734153	33
28	.259268	11.38	.992713	.38	.266555	11.77	.733445	32
29	.259951	11.37	.992690	.40	.267261	11.77	.732739	31
30	.260633	11.35	.992666	.38	.267967	11.73	.732033	30
31	9.261314	11.33	9.992643	.40	9.268671	11.73	10.731329	29
32	.261994	11.32	.992619	.38	.269375	11.70	.730625	28
33	.262673	11.30	.992596	.40	.270077	11.70	.729923	27
34	.263351	11.27	.992572	.38	.270779	11.67	.729221	26
35	.264027	11.27	.992549	.40	.271479	11.65	.728521	25
36	.264703	11.23	.992525	.40	.272178	11.63	.727822	24
37	.265377	11.23	.992501	.38	.272876	11.62	.727124	23
38	.266051	11.20	.992478	.40	.273573	11.60	.726427	22
39	.266723	11.20	.992454	.40	.274269	11.58	.725731	21
40	.267395	11.17	.992430	.40	.274964	11.57	.725036	20
41	9.268065	11.15	9.992406	.40	9.275658	11.55	10.724342	19
42	.268734	11.13	.992382	.38	.276351	11.53	.723649	18
43	.269402	11.12	.992359	.40	.277043	11.52	.722957	17
44	.270069	11.10	.992335	.40	.277734	11.50	.722266	16
45	.270735	11.08	.992311	.40	.278424	11.48	.721576	15
46	.271400	11.07	.992287	.40	.279113	11.47	.720887	14
47	.272064	11.03	.992263	.40	.279801	11.45	.720199	13
48	.272726	11.03	.992239	.42	.280488	11.43	.719512	12
49	.273388	11.02	.992214	.40	.281174	11.40	.718826	11
50	.274049	10.98	.992190	.40	.281858	11.40	.718142	10
51	9.274708	10.98	9.992166	.40	9.282542	11.38	10.717458	9
52	.275367	10.97	.992142	.40	.283225	11.37	.716775	8
53	.276025	10.93	.992118	.42	.283907	11.35	.716093	7
54	.276681	10.93	.992093	.40	.284588	11.33	.715412	6
55	.277337	10.90	.992069	.42	.285268	11.32	.714732	5
56	.277991	10.90	.992044	.40	.285947	11.28	.714053	4
57	.278645	10.87	.992020	.40	.286624	11.28	.713376	3
58	279297	10.85	.991996	.42	.287301	11.27	.712699	2
59	.279948	10.85	.991971	.40	.287977	11.25	.712023	1
60	9.280599		9.991947		9.288652		10.711348	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.280599	10.82	9.991947	.42	9.288652	11.23	10.711348	60
1	.281248	10.82	.991922	.42	.289326	11.22	.710674	59
2	.281897	10.78	.991897	.40	.289999	11.20	.710001	58
3	.282544	10.77	.991873	.42	.290671	11.18	.709329	57
4	.283190	10.77	.991848	.42	.291342	11.18	.708658	56
5	.283836	10.73	.991823	.40	.292013	11.15	.707987	55
6	.284480	10.73	.991799	.42	.292682	11.13	.707318	54
7	.285124	10.70	.991774	.42	.293350	11.12	.706650	53
8	.285766	10.70	.991749	.42	.294017	11.12	.705983	52
9	.286408	10.67	.991724	.42	.294684	11.08	.705316	51
10	.287048	10.67	.991699	.42	.295349	11.07	.704651	50
11	9.287688	10.63	9.991674	.42	9.296013	11.07	10.703987	49
12	.288326	10.63	.991649	.42	.296677	11.03	.703323	48
13	.288964	10.60	.991624	.42	.297339	11.03	.702661	47
14	.289600	10.60	.991599	.42	.298001	11.02	.701999	46
15	.290236	10.57	.991574	.42	.298662	11.00	.701338	45
16	.290870	10.57	.991549	.42	.299322	10.97	.700678	44
17	.291504	10.55	.991524	.43	.299980	10.97	.700020	43
18	.292137	10.52	.991498	.42	.300638	10.95	.699362	42
19	.292768	10.52	.991473	.42	.301295	10.93	.698705	41
20	.293399	10.50	.991448	.43	.301951	10.93	.698049	40
21	9.294029	10.48	9.991422	.42	9.302607	10.90	10.697393	39
22	.294658	10.47	.991397	.42	.303261	10.88	.696739	38
23	.295286	10.45	.991372	.43	.303914	10.88	.696086	37
24	.295913	10.43	.991346	.42	.304567	10.85	.695433	36
25	.296539	10.42	.991321	.43	.305218	10.85	.694782	35
26	.297164	10.40	.991295	.42	.305869	10.83	.694131	34
27	.297788	10.40	.991270	.43	.306519	10.82	.693481	33
28	.298412	10.37	.991244	.43	.307168	10.80	.692832	32
29	.299034	10.35	.991218	.42	.307816	10.78	.692184	31
30	.299655	10.35	.991193	.43	.308463	10.77	.691537	30
31	9.300276	10.32	9.991167	.43	9.309109	10.75	10.690891	29
32	.300895	10.32	.991141	.43	.309754	10.75	.690246	28
33	.301514	10.30	.991115	.42	.310399	10.72	.689601	27
34	.302132	10.27	.991090	.43	.311042	10.72	.688958	26
35	.302748	10.27	.991064	.43	.311685	10.70	.688315	25
36	.303364	10.25	.991038	.43	.312327	10.68	.687673	24
37	.303979	10.23	.991012	.43	.312968	10.67	.687032	23
38	.304593	10.23	.990986	.43	.313608	10.65	.686392	22
39	.305207	10.20	.990960	.43	.314247	10.63	.685753	21
40	.305819	10.18	.990934	.43	.314885	10.63	.685115	20
41	9.306430	10.18	9.990908	.43	9.315523	10.60	10.684477	19
42	.307041	10.15	.990882	.45	.316159	10.60	.683841	18
43	.307650	10.15	.990855	.43	.316795	10.58	.683205	17
44	.308259	10.13	.990829	.43	.317430	10.57	.682570	16
45	.308867	10.12	.990803	.43	.318064	10.55	.681936	15
46	.309474	10.10	.990777	.45	.318697	10.55	.681303	14
47	.310080	10.08	.990750	.43	319330	10.52	.680670	13
48	.310685	10.07	.990724	.45	.319961	10.52	.680039	12
49	.311289	10.07	.990697	.43	.320592	10.50	.679408	11
50	.311893	10.03	.990671	.43	.321222	10.48	.678778	10
51	9.312495	10.03	9.990645	.45	9.321851	10.47	10.678149	9
52	.313097	10.02	.990618	.45	.322479	10.45	.677521	8
53	.313698	9.98	.990591	.43	.323106	10.45	.676894	7
54	.314297	10.00	.990565	.45	.323733	10.42	.676267	6
55	.314897	9.97	.990538	.45	.324358	10.42	.675642	5
56	.315495	9.95	.990511	.43	.324983	10.40	.675017	4
57	.316092	9.95	.990485	.45	.325607	10.40	.674393	3
58	.316689	9.92	.990458	.45	.326231	10.37	.673769	2
59	.317284	9.92	.990431	.45	.326853	10.37	.673147	1
60	9.317879		9.990404		9.327475		10.672525	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.317879	9.90	9.990404	.43	9.327475	10.33	10.672525	60
1	.318473	9.88	.990378	.45	.328095	10.33	.671905	59
2	.319066	9.87	.990351	.45	.328715	10.32	.671285	58
3	.319658	9.85	.990324	.45	.329334	10.32	.670666	57
4	.320249	9.85	.990297	.45	.329953	10.28	.670047	56
5	.320840	9.83	.990270	.45	.330570	10.28	.669430	55
6	.321430	9.82	.990243	.47	.331187	10.27	.668813	54
7	.322019	9.80	.990215	.45	.331803	10.25	.668197	53
8	.322607	9.78	.990188	.45	.332418	10.25	.667582	52
9	.323194	9.77	.990161	.45	.333033	10.22	.666967	51
10	.323780	9.77	.990134	.45	.333646	10.22	.666354	50
11	9.324366	9.73	9.990107	.47	9.334259	10.20	10.665741	49
12	.324950	9.73	.990079	.45	.334871	10.18	.665129	48
13	.325534	9.72	.990052	.45	.335482	10.18	.664518	47
14	.326117	9.72	.990025	.47	.336093	10.15	.663907	46
15	.326700	9.68	.989997	.45	.336702	10.15	.663298	45
16	.327281	9.68	.989970	.47	.337311	10.13	.662689	44
17	.327862	9.67	.989942	.45	.337919	10.13	.662081	43
18	.328442	9.65	.989915	.47	.338527	10.10	.661473	42
19	.329021	9.63	.989887	.45	.339133	10.10	.660867	41
20	.329599	9.62	.989860	.47	.339739	10.08	.660261	40
21	9.330176	9.62	9.989832	.47	9.340344	10.07	10.659656	39
22	.330753	9.60	.989804	.45	.340948	10.07	.659052	38
23	.331329	9.57	.989777	.47	.341552	10.05	.658448	37
24	.331903	9.58	.989749	.47	.342155	10.03	.657845	36
25	.332478	9.55	.989721	.47	.342757	10.02	.657243	35
26	.333051	9.55	.989693	.47	.343358	10.00	.656642	34
27	.333624	9.52	.989665	.47	.343958	10.00	.656042	33
28	.334195	9.53	.989637	.45	.344558	9.98	.655442	32
29	.334767	9.50	.989610	.47	.345157	9.97	.654843	31
30	.335337	9.48	.989582	.48	.345755	9.97	.654245	30
31	9.335906	9.48	9.989553	.47	9.346353	9.93	10.653647	29
32	.336475	9.47	.989525	.47	.346949	9.93	.653051	28
33	.337043	9.45	.989497	.47	.347545	9.93	.652455	27
34	.337610	9.43	.989469	.47	.348141	9.90	.651859	26
35	.338176	9.43	.989441	.47	.348735	9.90	.651265	25
36	.338742	9.42	.989413	.47	.349329	9.88	.650671	24
37	.339307	9.40	.989385	.48	.349922	9.87	.650078	23
38	.339871	9.38	.989356	.47	.350514	9.87	.649486	22
39	.340434	9.37	.989328	.47	.351106	9.85	.648894	21
40	.340996	9.37	.989300	.48	.351697	9.83	.648303	20
41	9.341558	9.35	9.989271	.47	9.352287	9.82	10.647713	19
42	.342119	9.33	.989243	.48	.352876	9.82	.647124	18
43	.342679	9.33	.989214	.47	.353465	9.80	.646535	17
44	.343239	9.30	.989186	.48	.354053	9.78	.645947	16
45	.343797	9.30	.989157	.48	.354640	9.78	.645360	15
46	.344355	9.28	.989128	.47	.355227	9.77	.644773	14
47	.344912	9.28	.989100	.48	.355813	9.75	.644187	13
48	.345469	9.25	.989071	.48	.356398	9.73	.643602	12
49	.346024	9.25	.989042	.47	.356982	9.73	.643018	11
50	.346579	9.25	.989014	.48	.357566	9.72	.642434	10
51	9.347134	9.22	9.988985	.48	9.358149	9.70	10.641851	9
52	.347687	9.22	.988956	.48	.358731	9.70	.641269	8
53	.348240	9.20	.988927	.48	.359313	9.67	.640687	7
54	.348792	9.18	.988898	.48	.359893	9.68	.640107	6
55	.349343	9.17	.988869	.48	.360474	9.65	.639526	5
56	.349893	9.17	.988840	.48	.361053	9.65	.638947	4
57	.350443	9.15	.988811	.48	.361632	9.63	.638368	3
58	.350992	9.13	.988782	.48	.362210	9.62	.637790	2
59	.351540	9.13	.988753	.48	.362787	9.62	.637213	1
60	9.352088		9.988724		9.363364		10.636636	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.352088	9.12	9.988724	.48	9.363364	9.60	10.636636	60
1	.352635	9.10	.988695	.48	.363940	9.58	.636060	59
2	.353181	9.08	.988666	.50	.364515	9.58	.635485	58
3	.353726	9.08	.988636	.48	.365090	9.57	.634910	57
4	.354271	9.07	.988607	.48	.365664	9.55	.634336	56
5	.354815	9.05	.988578	.50	.366237	9.55	.633763	55
6	.355358	9.05	.988548	.48	.366810	9.53	.633190	54
7	.355901	9.03	.988519	.50	.367382	9.52	.632618	53
8	.356443	9.02	.988489	.48	.367953	9.52	.632047	52
9	.356984	9.00	.988460	.50	.368524	9.50	.631476	51
10	.357524	9.00	.988430	.48	.369094	9.48	.630906	50
11	9.358064	8.98	9.988401	.50	9.369663	9.48	10.630337	49
12	.358603	8.97	.988371	.48	.370232	9.45	.629768	48
13	.359141	8.95	.988342	.50	.370799	9.47	.629201	47
14	.359678	8.95	.988312	.50	.371367	9.43	.628633	46
15	.360215	8.95	.988282	.50	.371933	9.43	.628067	45
16	.360752	8.92	.988252	.48	.372499	9.42	.627501	44
17	.361287	8.92	.988223	.50	.373064	9.42	.626936	43
18	.361822	8.90	.988193	.50	.373629	9.40	.626371	42
19	.362356	8.88	.988163	.50	.374193	9.38	.625807	41
20	.362889	8.88	.988133	.50	.374756	9.38	.625244	40
21	9.363422	8.87	9.988103	.50	9.375319	9.37	10.624681	39
22	.363954	8.85	.988073	.50	.375881	9.35	.624119	38
23	.364485	8.85	.988043	.50	.376442	9.35	.623558	37
24	.365016	8.83	.988013	.50	.377003	9.33	.622997	36
25	.365546	8.82	.987983	.50	.377563	9.32	.622437	35
26	.366075	8.82	.987953	.52	.378122	9.32	.621878	34
27	.366604	8.78	.987922	.50	.378681	9.30	.621319	33
28	.367131	8.80	.987892	.50	.379239	9.30	.620761	32
29	.367659	8.77	.987862	.50	.379797	9.28	.620203	31
30	.368185	8.77	.987832	.52	.380354	9.27	.619646	30
31	9.368711	8.75	9.987801	.50	9.380910	9.27	10.619090	29
32	.369236	8.75	.987771	.52	.381466	9.23	.618534	28
33	.369761	8.72	.987740	.50	.382020	9.25	.617980	27
34	.370285	8.72	.987710	.52	.382575	9.23	.617425	26
35	.370808	8.70	.987679	.50	.383129	9.22	.616871	25
36	.371330	8.70	.987649	.52	.383682	9.20	.616318	24
37	.371852	8.68	.987618	.50	.384234	9.20	.615766	23
38	.372373	8.68	.987588	.52	.384786	9.18	.615214	22
39	.372894	8.67	.987557	.52	.385337	9.18	.614663	21
40	.373414	8.65	.987526	.50	.385888	9.17	.614112	20
41	9.373933	8.65	9.987496	.52	9.386438	9.15	10.613562	19
42	.374452	8.63	.987465	.52	.386987	9.15	.613013	18
43	.374970	8.62	.987434	.52	.387536	9.13	.612464	17
44	.375487	8.60	.987403	.52	.388084	9.12	.611916	16
45	.376003	8.60	.987372	.52	.388631	9.12	.611369	15
46	.376519	8.60	.987341	.52	.389178	9.10	.610822	14
47	.377035	8.57	.987310	.52	.389724	9.10	.610276	13
48	.377549	8.57	.987279	.52	.390270	9.08	.609730	12
49	.378063	8.57	.987248	.52	.390815	9.08	.609185	11
50	.378577	8.53	.987217	.52	.391360	9.05	.608640	10
51	9.379089	8.53	9.987186	.52	9.391903	9.07	10.608097	9
52	.379601	8.53	.987155	.52	.392447	9.03	.607553	8
53	.380118	8.52	.987124	.53	.392989	9.03	.607011	7
54	.380624	8.50	.987092	.52	.393531	9.03	.606469	6
55	.381134	8.48	.987061	.52	.394073	9.02	.605927	5
56	.381643	8.48	.987030	.53	.394614	9.00	.605386	4
57	.382152	8.48	.986998	.52	.395154	9.00	.604846	3
58	.382661	8.45	.986967	.52	.395694	8.98	.604306	2
59	.383168	8.45	.986936	.53	.396233	8.97	.603767	1
60	9.383675		9.986904		9.396771		10.603229	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.383675	8.45	9.986904	.52	9.396771	8.97	10.603229	60
1	.384182	8.42	.986873	.53	.397309	8.95	.602691	59
2	.384687	8.42	.986841	.53	.397846	8.95	.602154	58
3	.385192	8.42	.986809	.52	.398383	8.93	.601617	57
4	.385697	8.40	.986778	.53	.398919	8.93	.601081	56
5	.386201	8.38	.986746	.53	.399455	8.92	.600545	55
6	.386704	8.38	.986714	.52	.399990	8.90	.600010	54
7	.387207	8.37	.986683	.53	.400524	8.90	.599476	53
8	.387709	8.35	.986651	.53	.401058	8.88	.598942	52
9	.388210	8.35	.986619	.53	.401591	8.88	.598409	51
10	.388711	8.33	.986587	.53	.402124	8.87	.597876	50
11	9.389211	8.33	9.986555	.53	9.402656	8.85	10.597344	49
12	.389711	8.32	.986523	.53	.403187	8.85	.596813	48
13	.390210	8.30	.986491	.53	.403718	8.85	.596282	47
14	.390708	8.30	.986459	.53	.404249	8.82	.595751	46
15	.391206	8.28	.986427	.53	.404778	8.83	.595222	45
16	.391703	8.27	.986395	.53	.405308	8.80	.594692	44
17	.392199	8.27	.986363	.53	.405836	8.80	.594164	43
18	.392695	8.27	.986331	.53	.406364	8.80	.593636	42
19	.393191	8.23	.986299	.55	.406892	8.78	.593108	41
20	.393685	8.23	.986266	.53	.407419	8.77	.592581	40
21	9.394179	8.23	9.986234	.53	9.407945	8.77	10.592055	39
22	.394673	8.22	.986202	.55	.408471	8.75	.591529	38
23	.395166	8.20	.986169	.53	.408996	8.75	.591004	37
24	.395658	8.20	.986137	.55	.409521	8.73	.590479	36
25	.396150	8.18	.986104	.53	.410045	8.73	.589955	35
26	.396641	8.18	.986072	.55	.410569	8.72	.589431	34
27	.397132	8.15	.986039	.53	.411092	8.72	.588908	33
28	.397621	8.17	.986007	.55	.411615	8.70	.588385	32
29	.398111	8.15	.985974	.53	.412137	8.68	.587863	31
30	.398600	8.13	.985942	.55	.412658	8.68	.587342	30
31	9.399088	8.12	9.985909	.55	9.413179	8.67	10.586821	29
32	.399575	8.12	.985876	.55	.413699	8.67	.586301	28
33	.400062	8.12	.985843	.53	.414219	8.65	.585781	27
34	.400549	8.10	.985811	.55	.414738	8.65	.585262	26
35	.401035	8.08	.985778	.55	.415257	8.63	.584743	25
36	.401520	8.08	.985745	.55	.415775	8.63	.584225	24
37	.402005	8.07	.985712	.55	.416293	8.62	.583707	23
38	.402489	8.05	.985679	.55	.416810	8.60	.583190	22
39	.402972	8.05	.985646	.55	.417326	8.60	.582674	21
40	.403455	8.05	.985613	.55	.417842	8.60	.582158	20
41	9.403938	8.03	9.985580	.55	9.418358	8.58	10.581642	19
42	.404420	8.02	.985547	.55	.418873	8.57	.581127	18
43	.404901	8.02	.985514	.57	.419387	8.57	.580613	17
44	.405382	8.00	.985480	.55	.419901	8.57	.580099	16
45	.405862	7.98	.985447	.55	.420415	8.55	.579585	15
46	.406341	7.98	.985414	.55	.420927	8.55	.579073	14
47	.406820	7.98	.985381	.57	.421440	8.53	.578560	13
48	.407299	7.97	.985347	.55	.421952	8.52	.578048	12
49	.407777	7.95	.985314	.57	.422463	8.52	.577537	11
50	.408254	7.95	.985280	.55	.422974	8.50	.577026	10
51	9.408731	7.93	9.985247	.57	9.423484	8.48	10.576516	9
52	.409207	7.93	.985213	.55	.423993	8.50	.576007	8
53	.409682	7.92	.985180	.57	.424503	8.47	.575497	7
54	.410157	7.92	.985146	.55	.425011	8.47	.574989	6
55	.410632	7.90	.985113	.57	.425519	8.47	.574481	5
56	.411106	7.88	.985079	.57	.426027	8.45	.573973	4
57	.411579	7.88	.985045	.57	.426534	8.45	.573466	3
58	.412052	7.87	.985011	.55	.427041	8.43	.572959	2
59	.412524	7.87	.984978	.57	.427547	8.42	.572453	1
60	9.412996		9.984944		9.428052		10.571948	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.412996	7.85	9.984944	.57	9.428052	8.43	10.571948	60
1	.413467	7.85	.984910	.57	.428558	8.40	.571442	59
2	.413938	7.83	.984876	.57	.429062	8.40	.570938	58
3	.414408	7.83	.984842	.57	.429566	8.40	.570434	57
4	.414878	7.82	.984808	.57	.430070	8.38	.569930	56
5	.415347	7.80	.984774	.57	.430573	8.37	.569427	55
6	.415815	7.80	.984740	.57	.431075	8.37	.568925	54
7	.416283	7.80	.984706	.57	.431577	8.37	.568423	53
8	.416751	7.77	.984672	.57	.432079	8.35	.567921	52
9	.417217	7.78	.984638	.58	.432580	8.33	.567420	51
10	.417684	7.77	.984603	.57	.433080	8.33	.566920	50
11	9.418150	7.75	9.984569	.57	9.433580	8.33	10.566420	49
12	.418615	7.73	.984535	.58	.434080	8.32	.565920	48
13	.419079	7.75	.984500	.57	.434579	8.32	.565421	47
14	.419544	7.72	.984466	.57	.435078	8.30	.564922	46
15	.420007	7.72	.984432	.58	.435576	8.28	.564424	45
16	.420470	7.72	.984397	.57	.436073	8.28	.563927	44
17	.420933	7.70	.984363	.58	.436570	8.28	.563430	43
18	.421395	7.70	.984328	.57	.437067	8.27	.562933	42
19	.421857	7.68	.984294	.58	.437563	8.27	.562437	41
20	.422318	7.67	.984259	.58	.438059	8.25	.561941	40
21	9.422778	7.67	9.984224	.57	9.438554	8.23	10.561446	39
22	.423238	7.65	.984190	.58	.439048	8.25	.560952	38
23	.423697	7.65	.984155	.58	.439543	8.22	.560457	37
24	.424156	7.65	.984120	.58	.440036	8.22	.559964	36
25	.424615	7.63	.984085	.58	.440529	8.22	.559471	35
26	.425073	7.62	.984050	.58	.441022	8.20	.558978	34
27	.425530	7.62	.984015	.57	.441514	8.20	.558486	33
28	425987	7.60	.983981	.58	.442006	8.18	.557994	32
29	.426443	7.60	.983946	.58	.442497	8.18	.557503	31
30	.426899	7.58	.983911	.60	.442988	8.18	.557012	30
31	9.427354	7.58	9.983875	.58	9.443479	8.15	10.556521	29
32	.427809	7.57	.983840	.58	.443968	8.17	.556032	28
33	.428263	7.57	.983805	.58	.444458	8.15	.555542	27
34	.428717	7.55	.983770	.58	.444947	8.13	.555053	26
35	.429170	7.55	.983735	.58	.445435	8.13	.554565	25
36	.429623	7.53	.983700	.60	.445923	8.13	.554077	24
37	.430075	7.53	.983664	.58	.446411	8.12	.553589	23
38	.430527	7.52	.983629	.58	.446898	8.10	.553102	22
39	.430978	7.52	.983594	.60	.447384	8.10	.552616	21
40	.431429	7.50	.983558	.58	.447870	8.10	.552130	20
41	9.431879	7.50	9.983523	.60	9.448356	8.08	10.551644	19
42	.432329	7.48	.983487	.58	.448841	8.08	.551159	18
43	.432778	7.47	.983452	.60	.449326	8.07	.550674	17
44	.433226	7.48	.983416	.58	.449810	8.07	.550190	16
45	.433675	7.45	.983381	.60	.450294	8.05	.549706	15
46	.434122	7.45	.983345	.60	.450777	8.05	.549223	14
47	.434569	7.45	.983309	.60	.451260	8.05	.548740	13
48	.435016	7.43	.983273	.58	.451743	8.03	.548257	12
49	.435462	7.43	.983238	.60	.452225	8.02	.547775	11
50	.435908	7.42	.983202	.60	.452706	8.02	.547294	10
51	9.436353	7.42	9.983166	.60	9.453187	8.02	10.546813	9
52	.436798	7.40	.983130	.60	.453668	8.00	.546332	8
53	.437242	7.40	.983094	.60	.454148	8.00	.545852	7
54	.437686	7.38	.983058	.60	.454628	7.98	.545372	6
55	.438129	7.38	.983022	.60	.455107	7.98	.544893	5
56	.438572	7.37	.982986	.60	.455586	7.97	.544414	4
57	.439014	7.37	.982950	.60	.456064	7.97	.543936	3
58	.439456	7.35	.982914	.60	.456542	7.95	.543458	2
59	.439897	7.35	.982878	.60	.457019	7.95	.542981	1
60	9.440338		9.982842		9.457496		10.542504	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.440338	7.33	9.982842	.62	9.457496	7.95	10.542504	60
1	.440778	7.33	.982805	.60	.457973	7.93	.542027	59
2	.441218	7.33	.982769	.60	.458449	7.93	.541551	58
3	.441658	7.30	.982733	.62	.458925	7.92	.541075	57
4	.442096	7.32	.982696	.60	.459400	7.92	.540600	56
5	.442535	7.30	.982660	.60	.459875	7.90	.540125	55
6	.442973	7.28	.982624	.62	.460349	7.90	.539651	54
7	.443410	7.28	.982587	.60	.460823	7.90	.539177	53
8	.443847	7.28	.982551	.62	.461297	7.88	.538703	52
9	.444284	7.27	.982514	.62	.461770	7.87	.538230	51
10	.444720	7.25	.982477	.60	.462242	7.88	.537758	50
11	9.445155	7.25	9.982441	.62	9.462715	7.85	10.537285	49
12	.445590	7.25	.982404	.62	.463186	7.87	.536814	48
13	.446025	7.23	.982367	.60	.463658	7.83	.536342	47
14	.446459	7.23	.982331	.62	.464128	7.85	.535872	46
15	.446893	7.22	.982294	.62	.464599	7.83	.535401	45
16	.447326	7.22	.982257	.62	.465069	7.83	.534931	44
17	.447759	7.20	.982220	.62	.465539	7.82	.534461	43
18	.448191	7.20	.982183	.62	.466008	7.82	.533992	42
19	.448623	7.18	.982146	.62	.466477	7.80	.533523	41
20	.449054	7.18	.982109	.62	.466945	7.80	.533055	40
21	9.449485	7.17	9.982072	.62	9.467413	7.78	10.532587	39
22	.449915	7.17	.982035	.62	.467880	7.78	.532120	38
23	.450345	7.17	.981998	.62	.468347	7.78	.531653	37
24	.450775	7.15	.981961	.62	.468814	7.77	.531186	36
25	.451204	7.13	.981924	.63	.469280	7.77	.530720	35
26	.451632	7.13	.981886	.62	.469746	7.75	.530254	34
27	.452060	7.13	.981849	.62	.470211	7.75	.529789	33
28	.452488	7.12	.981812	.63	.470676	7.75	.529324	32
29	.452915	7.12	.981774	.62	.471141	7.73	.528859	31
30	.453342	7.10	.981737	.62	.471605	7.73	.528395	30
31	9.453768	7.10	9.981700	.63	9.472069	7.72	10.527931	29
32	.454194	7.08	.981662	.62	.472532	7.72	.527468	28
33	.454619	7.08	.981625	.63	.472995	7.70	.527005	27
34	.455044	7.08	.981587	.63	.473457	7.70	.526543	26
35	.455469	7.07	.981549	.62	.473919	7.70	.526081	25
36	.455893	7.05	.981512	.63	.474381	7.68	.525619	24
37	.456316	7.05	.981474	.63	.474842	7.68	.525158	23
38	.456739	7.05	.981436	.62	.475303	7.67	.524697	22
39	.457162	7.03	.981399	.63	.475763	7.67	.524237	21
40	.457584	7.03	.981361	.63	.476223	7.67	.523777	20
41	9.458006	7.02	9.981323	.63	9.476683	7.65	10.523317	19
42	.458427	7.02	.981285	.63	.477142	7.65	.522858	18
43	.458848	7.00	.981247	.63	.477601	7.63	.522399	17
44	.459268	7.00	.981209	.63	.478059	7.63	.521941	16
45	.459688	7.00	.981171	.63	.478517	7.63	.521483	15
46	.460108	6.98	.981133	.63	.478975	7.62	.521025	14
47	.460527	6.98	.981095	.63	.479432	7.62	.520568	13
48	.460946	6.97	.981057	.63	.479889	7.60	.520111	12
49	.461364	6.97	.981019	.63	.480345	7.60	.519655	11
50	.461782	6.95	.980981	.65	.480801	7.60	.519199	10
51	9.462199	6.95	9.980942	.63	9.481257	7.58	10.518743	9
52	.462616	6.93	.980904	.63	.481712	7.58	.518288	8
53	.463032	6.93	.980866	.65	.482167	7.57	.517833	7
54	.463448	6.93	.980827	.63	.482621	7.57	.517379	6
55	.463864	6.92	.980789	.65	.483075	7.57	.516925	5
56	.464279	6.92	.980750	.63	.483529	7.55	.516471	4
57	.464694	6.90	.980712	.65	.483982	7.55	.516018	3
58	.465108	6.90	.980673	.63	.484435	7.53	.515565	2
59	.465522	6.88	.980635	.65	.484887	7.53	.515113	1
60	9.465935		9.980596		9.485339		10.514661	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.465935	6.88	9.980596	.63	9.485339	7.53	10.514661	60
1	.466348	6.88	.980558	.65	.485791	7.52	.514209	59
2	.466761	6.87	.980519	.65	.486242	7.52	.513758	58
3	.467173	6.87	.980480	.63	.486693	7.50	.513307	57
4	.467585	6.85	.980442	.65	.487143	7.50	.512857	56
5	.467996	6.85	.980403	.65	.487593	7.50	.512407	55
6	.468407	6.83	.980364	.65	.488043	7.48	.511957	54
7	.468817	6.83	.980325	.65	.488492	7.48	.511508	53
8	.469227	6.83	.980286	.65	.488941	7.48	.511059	52
9	.469637	6.82	.980247	.65	.489390	7.47	.510610	51
10	.470046	6.82	.980208	.65	.489838	7.47	.510162	50
11	9.470455	6.80	9.980169	.65	9.490286	7.45	10.509714	49
12	.470863	6.80	.980130	.65	.490733	7.45	.509267	48
13	.471271	6.80	.980091	.65	.491180	7.45	.508820	47
14	.471679	6.78	.980052	.67	.491627	7.43	.508373	46
15	.472086	6.77	.980012	.65	.492073	7.43	.507927	45
16	.472492	6.77	.979973	.65	.492519	7.43	.507481	44
17	.472898	6.77	.979934	.65	.492965	7.42	.507035	43
18	.473304	6.77	.979895	.67	.493410	7.40	.506590	42
19	.473710	6.75	.979855	.65	.493854	7.42	.506146	41
20	.474115	6.73	.979816	.67	.494299	7.40	.505701	40
21	9.474519	6.73	9.979776	.65	9.494743	7.38	10.505257	39
22	.474923	6.73	.979737	.67	.495186	7.40	.504814	38
23	.475327	6.72	.979697	.65	.495630	7.38	.504370	37
24	.475730	6.72	.979658	.67	.496073	7.37	.503927	36
25	.476133	6.72	.979618	.65	.496515	7.37	.503485	35
26	.476536	6.70	.979579	.67	.496957	7.37	.503043	34
27	.476938	6.70	.979539	.67	.497399	7.37	.502601	33
28	.477340	6.68	.979499	.67	.497841	7.35	.502159	32
29	.477741	6.68	.979459	.65	.498282	7.33	.501718	31
30	.478142	6.67	.979420	.67	.498722	7.35	.501278	30
31	9.478542	6.67	9.979380	.67	9.499163	7.33	10.500837	29
32	.478942	6.67	.979340	.67	.499603	7.32	.500397	28
33	.479342	6.65	.979300	.67	.500042	7.32	.499958	27
34	.479741	6.65	.979260	.67	.500481	7.32	.499519	26
35	.480140	6.65	.979220	.67	.500920	7.32	.499080	25
36	.480539	6.63	.979180	.67	.501359	7.30	.498641	24
37	.480937	6.62	.979140	.67	.501797	7.30	.498203	23
38	.481334	6.62	.979100	.68	.502235	7.28	.497765	22
39	.481731	6.62	.979059	.67	.502672	7.28	.497328	21
40	.482128	6.62	.979019	.67	.503109	7.28	.496891	20
41	9.482525	6.60	9.978979	.67	9.503546	7.27	10.496454	19
42	.482921	6.58	.978939	.68	.503982	7.27	.496018	18
43	.483316	6.60	.978898	.67	.504418	7.27	.495582	17
44	.483712	6.58	.978858	.68	.504854	7.25	.495146	16
45	.484107	6.57	.978817	.67	.505289	7.25	.494711	15
46	.484501	6.57	.978777	.67	.505724	7.25	.494276	14
47	.484895	6.57	.978737	.68	.506159	7.23	.493841	13
48	.485289	6.55	.978696	.68	.506593	7.23	.4934[illegible]	12
49	.485682	6.55	.978655	.67	.507027	7.23	.492973	11
50	.486075	6.53	.978615	.68	.507460	7.22	.492540	10
51	9.486467	6.55	9.978574	.68	9.507893	7.22	10.492107	9
52	.486860	6.52	.978533	.67	.508326	7.22	.491674	8
53	.487251	6.53	.978493	.68	.508759	7.20	.491241	7
54	.487643	6.52	.978452	.68	.509191	7.18	.490809	6
55	.488034	6.50	.978411	.68	.509622	7.20	.490378	5
56	.488424	6.50	.978370	.68	.510054	7.18	.489946	4
57	.488814	6.50	.978329	.68	.510485	7.18	.489515	3
58	.489204	6.48	.978288	.68	.510916	7.17	.489084	2
59	.489593	6.48	.978247	.68	.511346	7.17	.488654	1
60	9.489982		9.978206		9.511776		10.488224	0
′	Cosine.	D 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.489982	6.48	9.978206	.68	9.511776	7.17	10.488224	60
1	.490371	6.47	.978165	.68	.512206	7.15	.487794	59
2	.490759	6.47	.978124	.68	.512635	7.15	.487365	58
3	.491147	6.47	.978083	.68	.513064	7.15	.486936	57
4	.491535	6.45	.978042	.68	.513493	7.13	.486507	56
5	.491922	6.43	.978001	.70	.513921	7.13	.486079	55
6	.492308	6.45	.977959	.68	.514349	7.13	.485651	54
7	.492695	6.43	.977918	.68	.514777	7.12	.485223	53
8	.493081	6.42	.977877	.70	.515204	7.12	.484796	52
9	.493466	6.42	.977835	.68	.515631	7.10	.484369	51
10	.493851	6.42	.977794	.70	.516057	7.12	.483943	50
11	9.494236	6.42	9.977752	.68	9.516484	7.10	10.483516	49
12	.494621	6.40	.977711	.70	.516910	7.08	.483090	48
13	.495005	6.38	.977669	.68	.517335	7.10	.482665	47
14	.495388	6.40	.977628	.70	.517761	7.08	.482239	46
15	.495772	6.37	.977586	.70	.518186	7.07	.481814	45
16	.496154	6.38	.977544	.68	.518610	7.07	.481390	44
17	.496537	6.37	.977503	.70	.519034	7.07	.480966	43
18	.496919	6.37	.977461	.70	.519458	7.07	.480542	42
19	.497301	6.35	.977419	.70	.519882	7.05	.480118	41
20	.497682	6.35	.977377	.70	.520305	7.05	.479695	40
21	9.498064	6.33	9.977335	.70	9.520728	7.05	10.479272	39
22	.498444	6.35	.977293	.70	.521151	7.03	.478849	38
23	.498825	6.32	.977251	.70	.521573	7.03	.478427	37
24	.499204	6.33	.977209	.70	.521995	7.03	.478005	36
25	.499584	6.32	.977167	.70	.522417	7.02	.477583	35
26	.499963	6.32	.977125	.70	.522838	7.02	.477162	34
27	.500342	6.32	.977083	.70	.523259	7.02	.476741	33
28	.500721	6.30	.977041	.70	.523680	7.00	.476320	32
29	.501099	6.28	.976999	.70	.524100	7.00	.475900	31
30	.501476	6.30	.976957	.72	.524520	7.00	.475480	30
31	9.501854	6.28	9.976914	.70	9.524940	6.98	10.475060	29
32	.502231	6.27	.976872	.70	.525359	6.98	.474641	28
33	.502607	6.28	.976830	.72	.525778	6.98	.474222	27
34	.502984	6.27	.976787	.70	.526197	6.97	.473803	26
35	.503360	6.25	.976745	.72	.526615	6.97	.473385	25
36	.503735	6.25	.976702	.70	.527033	6.97	.472967	24
37	.504110	6.25	.976660	.72	.527451	6.95	.472549	23
38	.504485	6.25	.976617	.72	.527868	6.95	.472132	22
39	.504860	6.23	.976574	.70	.528285	6.95	.471715	21
40	.505234	6.23	.976532	.72	.528702	6.95	.471298	20
41	9.505608	6.22	9.976489	.72	9.529119	6.93	10.470881	19
42	.505981	6.22	.976446	.70	.529535	6.93	.470465	18
43	.506354	6.22	.976404	.72	.529951	6.92	.470049	17
44	.506727	6.20	.976361	.72	.530366	6.92	.469634	16
45	.507099	6.20	.976318	.72	.530781	6.92	.469219	15
46	.507471	6.20	.976275	.72	.531196	6.92	.468804	14
47	.507843	6.18	.976232	.72	.531611	6.90	.468389	13
48	.508214	6.18	.976189	.72	.532025	6.90	.467975	12
49	.508585	6.18	.976146	.72	.532439	6.90	.467561	11
50	.508956	6.17	.976103	.72	.532853	6.88	.467147	10
51	9.509326	6.17	9.976060	.72	9.533266	6.88	10.466734	9
52	.509696	6.15	.976017	.72	.533679	6.88	.466321	8
53	.510065	6.15	.975974	.73	.534092	6.87	.465908	7
54	.510434	6.15	.975930	.72	.534504	6.87	.465496	6
55	.510803	6.15	.975887	.72	.534916	6.87	.465084	5
56	.511172	6.13	.975844	.73	.535328	6.85	.464672	4
57	.511540	6.12	.975800	.72	.535739	6.85	.464261	3
58	.511907	6.13	.975757	.72	.536150	6.85	.463850	2
59	.512275	6.12	.975714	.73	.536561	6.85	.463439	1
60	9.512642		9.975670		9.536972		10.463028	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.512642	6.12	9.975670	.72	9.536972	6.83	10.463028	60
1	.513009	6.10	.975627	.73	.537382	6.83	.462618	59
2	.513375	6.10	.975583	.73	.537792	6.83	.462208	58
3	.513741	6.10	.975539	.72	.538202	6.82	.461798	57
4	.514107	6.08	.975496	.73	.538611	6.82	.461389	56
5	.514472	6.08	.975452	.73	.539020	6.82	.460980	55
6	.514837	6.08	.975408	.72	.539429	6.80	.460571	54
7	.515202	6.07	.975365	.73	.539837	6.80	.460163	53
8	.515566	6.07	.975321	.73	.540245	6.80	.459755	52
9	.515930	6.07	.975277	.73	.540653	6.80	.459347	51
10	.516294	6.05	.975233	.73	.541061	6.78	.458939	50
11	9.516657	6.05	9.975189	.73	9.541468	6.78	10.458532	49
12	.517020	6.03	.975145	.73	.541875	6.77	.458125	48
13	.517382	6.05	.975101	.73	.542281	6.78	.457719	47
14	.517745	6.03	.975057	.73	.542688	6.77	.457312	46
15	.518107	6.02	.975013	.73	.543094	6.75	.456906	45
16	.518468	6.02	.974969	.73	.543499	6.77	.456501	44
17	.518829	6.02	.974925	.75	.543905	6.75	.456095	43
18	.519190	6.02	.974880	.73	.544310	6.75	.455690	42
19	.519551	6.00	.974836	.73	.544715	6.73	.455285	41
20	.519911	6.00	.974792	.73	.545119	6.75	.454881	40
21	9.520271	6.00	9.974748	.75	9.545524	6.73	10.454476	39
22	.520631	5.98	.974703	.73	.545928	6.72	.454072	38
23	.520990	5.98	.974659	.75	.546331	6.73	.453669	37
24	.521349	5.97	.974614	.73	.546735	6.72	.453265	36
25	.521707	5.98	.974570	.75	.547138	6.70	.452862	35
26	.522066	5.97	.974525	.73	.547540	6.72	.452460	34
27	.522424	5.95	.974481	.75	.547943	6.70	.452057	33
28	.522781	5.95	.974436	.75	.548345	6.70	.451655	32
29	.523138	5.95	.974391	.73	.548747	6.70	.451253	31
30	.523495	5.95	.974347	.75	.549149	6.68	.450851	30
31	9.523852	5.93	9.974302	.75	9.549550	6.68	10.450450	29
32	.524208	5.93	.974257	.75	.549951	6.68	.450049	28
33	.524564	5.93	.974212	.75	.550352	6.67	.449648	27
34	.524920	5.92	.974167	.75	.550752	6.68	.449248	26
35	.525275	5.92	.974122	.75	.551153	6.65	.448847	25
36	.525630	5.90	.974077	.75	.551552	6.67	.448448	24
37	.525984	5.92	.974032	.75	.551952	6.65	.448048	23
38	.526339	5.90	.973987	.75	.552351	6.65	.447649	22
39	.526693	5.88	.973942	.75	.552750	6.65	.447250	21
40	.527046	5.90	.973897	.75	.553149	6.65	.446851	20
41	9.527400	5.88	9.973852	.75	9.553548	6.63	10.446452	19
42	.527753	5.87	.973807	.77	.553946	6.63	.446054	18
43	.528105	5.88	.973761	.75	.554344	6.62	.445656	17
44	.528458	5.87	.973716	.75	.554741	6.63	.445259	16
45	.528810	5.85	.973671	.77	.555139	6.62	.444861	15
46	.529161	5.87	.973625	.75	.555536	6.62	.444464	14
47	.529513	5.85	.973580	.75	.555933	6.60	.444067	13
48	.529864	5.85	.973535	.77	.556329	6.60	.443671	12
49	.530215	5.83	.973489	.75	.556725	6.60	.443275	11
50	.530565	5.83	.973444	.77	.557121	6.60	.442879	10
51	9.530915	5.83	9.973398	.77	9.557517	6.60	10.442483	9
52	.531265	5.82	.973352	.75	.557913	6.58	.442087	8
53	.531614	5.82	.973307	.77	.558308	6.58	.441692	7
54	.531963	5.82	.973261	.77	.558703	6.57	.441297	6
55	.532312	5.82	.973215	.77	.559097	6.57	.440903	5
56	.532661	5.80	.973169	.75	.559491	6.57	.440509	4
57	.533009	5.80	.973124	.77	.559885	6.57	.440115	3
58	.533357	5.78	.973078	.77	.560279	6.57	.439721	2
59	.533704	5.80	.973032	.77	.560673	6.55	.439327	1
60	9.534052		9.972986		9.561066		10.438934	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.534052	5.78	9.972986	.77	9.561066	6.55	10.438934	60
1	.534399	5.77	.972940	.77	.561459	6.53	.438541	59
2	.534745	5.78	.972894	.77	.561851	6.55	.438149	58
3	.535092	5.77	.972848	.77	.562244	6.53	.437756	57
4	.535438	5.75	.972802	.78	.562636	6.53	.437364	56
5	.535783	5.77	.972755	.77	.563028	6.52	.436972	55
6	.536129	5.75	.972709	.77	.563419	6.53	.436581	54
7	.536474	5.73	.972663	.77	.563811	6.52	.436189	53
8	.536818	5.75	.972617	.78	.564202	6.52	.435798	52
9	.537163	5.73	.972570	.77	.564593	6.50	.435407	51
10	.537507	5.73	.972524	.77	.564983	6.50	.435017	50
11	9.537851	5.72	9.972478	.78	9.565373	6.50	10.434627	49
12	.538194	5.73	.972431	.77	.565763	6.50	.434237	48
13	.538538	5.70	.972385	.78	.566153	6.48	.433847	47
14	.538880	5.72	.972338	.78	.566542	6.50	.433458	46
15	.539223	5.70	.972291	.77	.566932	6.47	.433068	45
16	.539565	5.70	.972245	.78	.567320	6.48	.432680	44
17	.539907	5.68	.972198	.78	.567709	6.48	.432291	43
18	.540249	5.68	.972151	.77	.568098	6.47	.431902	42
19	.540590	5.68	.972105	.78	.568486	6.45	.431514	41
20	.540931	5.68	.972058	.78	.568873	6.47	.431127	40
21	9.541272	5.68	9.972011	.78	9.569261	6.45	10.430739	39
22	.541613	5.67	.971964	.78	.569648	6.45	.430352	38
23	.541953	5.67	.971917	.78	.570035	6.45	.429965	37
24	.542293	5.65	.971870	.78	.570422	6.45	.429578	36
25	.542632	5.65	.971823	.78	.570809	6.43	.429191	35
26	.542971	5.65	.971776	.78	.571195	6.43	.428805	34
27	.543310	5.65	.971729	.78	.571581	6.43	.428419	33
28	.543649	5.63	.971682	.78	.571967	6.42	.428033	32
29	.543987	5.63	.971635	.78	.572352	6.43	.427648	31
30	.544325	5.63	.971588	.80	.572738	6.42	.427262	30
31	9.544663	5.62	9.971540	.78	9.573123	6.40	10.426877	29
32	.545000	5.63	.971493	.78	.573507	6.42	.426493	28
33	.545338	5.60	.971446	.80	.573892	6.40	.426108	27
34	.545674	5.62	.971398	.78	.574276	6.40	.425724	26
35	.546011	5.60	.971351	.80	.574660	6.40	.425340	25
36	.546347	5.60	.971303	.78	.575044	6.38	.424956	24
37	.546683	5.60	.971256	.80	.575427	6.38	.424573	23
38	.547019	5.58	.971208	.78	.575810	6.38	.424190	22
39	.547354	5.58	.971161	.80	.576193	6.38	.423807	21
40	.547689	5.58	.971113	.78	.576576	6.38	.423424	20
41	9.548024	5.58	9.971066	.80	9.576959	6.37	10.423041	19
42	.548359	5.57	.971018	.80	.577341	6.37	.422659	18
43	.548693	5.57	.970970	.80	.577723	6.35	.422277	17
44	.549027	5.55	.970922	.80	.578104	6.37	.421896	16
45	.549360	5.55	.970874	.78	.578486	6.35	.421514	15
46	.549693	5.55	.970827	.80	.578867	6.35	.421133	14
47	.550026	5.55	.970779	.80	.579248	6.35	.420752	13
48	.550359	5.55	.970731	.80	.579629	6.33	.420371	12
49	.550692	5.53	.970683	.80	.580009	6.33	.419991	11
50	.551024	5.53	.970635	.82	.580389	6.33	.419611	10
51	9.551356	5.52	9.970586	.80	9.580769	6.33	10.419231	9
52	.551687	5.52	.970538	.80	.581149	6.32	.418851	8
53	.552018	5.52	.970490	.80	.581528	6.32	.418472	7
54	.552349	5.52	.970442	.80	.581907	6.32	.418093	6
55	.552680	5.50	.970394	.82	.582286	6.32	.417714	5
56	.553010	5.52	.970345	.80	.582665	6.32	.417335	4
57	.553341	5.48	.970297	.80	.583044	6.30	.416956	3
58	.553670	5.50	.970249	.82	.583422	6.30	.416578	2
59	.554000	5.48	.970200	.80	.583800	6.28	.416200	1
60	9.554329		9.970152		9.584177		10.415823	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.
0	9.554329	5.48	9.970152	.82	9.584177	6.30	10.415823
1	.554658	5.48	.970103	.80	.584555	6.28	.415445
2	.554987	5.47	.970055	.82	.584932	6.28	.415068
3	.555315	5.47	.970006	.82	.585309	6.28	.414691
4	.555643	5.47	.969957	.80	.585686	6.27	.414314
5	.555971	5.47	.969909	.82	.586062	6.28	.413938
6	.556299	5.45	.969860	.82	.586439	6.27	.413561
7	.556626	5.45	.969811	.82	.586815	6.25	.413185
8	.556953	5.45	.969762	.80	.587190	6.27	.412810
9	.557280	5.43	.969714	.82	.587566	6.25	.412434
10	.557606	5.43	.969665	.82	.587941	6.25	.412059
11	9.557932	5.43	9.969616	.82	9.588316	6.25	10.411684
12	.558258	5.42	.969567	.82	.588691	6.25	.411309
13	.558583	5.43	.969518	.82	.589066	6.23	.410934
14	.558909	5.42	.969469	.82	.589440	6.23	.410560
15	.559234	5.40	.969420	.83	.589814	6.23	.410186
16	.559558	5.42	.969370	.82	.590188	6.23	.409812
17	.559883	5.40	.969321	.82	.590562	6.22	.409438
18	.560207	5.40	.969272	.82	.590935	6.22	.409065
19	.560531	5.40	.969223	.83	.591308	6.22	.408692
20	.560855	5.38	.969173	.82	.591681	6.22	.408319
21	9.561178	5.38	9.969124	.82	9.592054	6.20	10.407946
22	.561501	5.38	.969075	.83	.592426	6.22	.407574
23	.561824	5.37	.969025	.82	.592799	6.20	.407201
24	.562146	5.37	.968976	.83	.593171	6.18	.406829
25	.562468	5.37	.968926	.82	.593542	6.20	.406458
26	.562790	5.37	.968877	.83	.593914	6.18	.406086
27	.563112	5.35	.968827	.83	.594285	6.18	.405715
28	.563433	5.37	.968777	.82	.594656	6.18	.405344
29	.563755	5.33	.968728	.83	.595027	6.18	.404973
30	.564075	5.35	.968678	.83	.595398	6.17	.404602
31	9.564396	5.33	9.968628	.83	9.595768	6.17	10.404232
32	.564716	5.33	.968578	.83	.596138	6.17	.403862
33	.565036	5.33	.968528	.82	.596508	6.17	.403492
34	.565356	5.33	.968479	.83	.596878	6.15	.403122
35	.565676	5.32	.968429	.83	.597247	6.15	.402753
36	.565995	5.32	.968379	.83	.597616	6.15	.402384
37	.566314	5.30	.968329	.85	.597985	6.15	.402015
38	.566632	5.32	.968278	.83	.598354	6.13	.401646
39	.566951	5.30	.968228	.83	.598722	6.15	.401278
40	.567269	5.30	.968178	.83	.599091	6.13	.400909
41	9.567587	5.28	9.968128	.83	9.599459	6.13	10.400541
42	.567904	5.30	.968078	.85	.599827	6.12	.400173
43	.568222	5.28	.968027	.83	.600194	6.13	.399806
44	.568539	5.28	.967977	.83	.600562	6.12	.399438
45	.568856	5.27	.967927	.85	.600929	6.12	.399071
46	.569172	5.27	.967876	.83	.601296	6.12	.398704
47	.569488	5.27	.967826	.85	.601663	6.10	.398337
48	.569804	5.27	.967775	.83	.602029	6.10	.397971
49	.570120	5.25	.967725	.85	.602395	6.10	.397605
50	.570435	5.27	.967674	.83	.602761	6.10	.397239
51	9.570751	5.25	9.967624	.85	9.603127	6.10	10.396873
52	.571066	5.23	.967573	.85	.603493	6.08	.396507
53	.571380	5.25	.967522	.85	.603858	6.08	.396142
54	.571695	5.23	.967471	.83	.604223	6.08	.395777
55	.572009	5.23	.967421	.85	.604588	6.08	.395412
56	.572323	5.22	.967370	.85	.604953	6.07	.395047
57	.572636	5.23	.967319	.85	.605317	6.08	.394683
58	.572950	5.22	.967268	.85	.605682	6.07	.394318
59	.573263	5.20	.967217	.85	.606046	6.07	.393954
60	9.573575		9.967166		9.606410		10.393590
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.

111°

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.573575	5.22	9.967166	.85	9.606410	6.05	10.393590	60
1	.573888	5.20	.967115	.85	.606773	6.07	.393227	59
2	.574200	5.20	.967064	.85	.607137	6.05	.392863	58
3	.574512	5.20	.967013	.87	.607500	6.05	.392500	57
4	.574824	5.20	.966961	.85	.607863	6.03	.392137	56
5	.575136	5.18	.966910	.85	.608225	6.05	.391775	55
6	.575447	5.18	.966859	.85	..608588	6.03	.391412	54
7	.575758	5.18	.966808	.87	.608950	6.03	.391050	53
8	.576069	5.17	.966756	.85	.609312	6.03	.390688	52
9	.576379	5.17	.966705	.87	.609674	6.03	.390326	51
10	.576689	5.17	.966653	.85	.610036	6.02	.389964	50
11	9.576999	5.17	9.966602	.87	9.610397	6.03	10.389603	49
12	.577309	5.15	.966550	.85	.610759	6.02	.389241	48
13	.577618	5.15	.966499	.87	.611120	6.00	.388880	47
14	.577927	5.15	.966447	.87	.611480	6.02	.388520	46
15	.578236	5.15	.966395	.85	.611841	6.00	.388159	45
16	.578545	5.13	.966344	.87	.612201	6.00	.387799	44
17	.578853	5.15	.966292	.87	.612561	6.00	.387439	43
18	.579162	5.13	.966240	.87	.612921	6.00	.387079	42
19	.579470	5.12	.966188	.87	.613281	6.00	.386719	41
20	.579777	5.13	.966136	.85	.613641	5.98	.386359	40
21	9.580085	5.12	9.966085	.87	9.614000	5.98	10.386000	39
22	.580392	5.12	.966033	.87	.614359	5.98	.385641	38
23	.580699	5.10	.965981	.87	.614718	5.98	.385282	37
24	.581005	5.12	.965929	.88	.615077	5.97	.384923	36
25	.581312	5.10	.965876	.87	.615435	5.97	.384565	35
26	.581618	5.10	.965824	.87	.615793	5.97	.384207	34
27	.581924	5.08	.965772	.87	.616151	5.97	.383849	33
28	.582229	5.10	.965720	.87	.616509	5.97	.383491	32
29	.582535	5.08	.965668	.88	.616867	5.95	.383133	31
30	.582840	5.08	.965615	.87	.617224	5.97	.382776	30
31	9.583145	5.07	9.965563	.87	9.617582	5.95	10.382418	29
32	.583449	5.08	.965511	.88	.617939	5.93	.382061	28
33	.583754	5.07	.965458	.87	.618295	5.95	.381705	27
34	.584058	5.05	.965406	.88	.918652	5.93	.381348	26
35	.584361	5.07	.965353	.87	.619008	5.93	.380992	25
36	.584665	5.05	.965301	.88	.619364	5.93	.380636	24
37	.584968	5.07	.965248	.88	.619720	5.93	.380280	23
38	.585272	5.03	.965195	.87	.620076	5.93	.379924	22
39	.585574	5.05	.965143	.88	.620432	5.92	.379568	21
40	.585877	5.03	.965090	.88	.620787	5.92	.379213	20
41	9.586179	5.05	9.965037	.88	9.621142	5.92	10.378858	19
42	.586482	5.02	.964984	.88	.621497	5.92	.378503	18
43	.586783	5.03	.964931	.87	.621852	5.92	.378148	17
44	.587085	5.02	.964879	.88	.622207	5.90	.377793	16
45	.587386	5.03	.964826	.88	.622561	5.90	.377439	15
46	.587688	5.02	.964773	.88	.622915	5.90	.377085	14
47	.587989	5.00	.964720	.90	.623269	5.90	.376731	13
48	.588289	5.02	.964666	.88	.623623	5.88	.376377	12
49	.588590	5.00	.964613	.88	.623976	5.90	.376024	11
50	.588890	5.00	.964560	.88	.624330	5.88	.375670	10
51	9.589190	4.98	9.964507	.88	9.624683	5.88	10.375317	9
52	.589489	5.00	.964454	.90	.625036	5.87	.374964	8
53	.589789	4.98	.964400	.88	.625388	5.88	.374612	7
54	.590088	4.98	.964347	.88	.625741	5.87	.374259	6
55	.590387	4.98	.964294	.90	.626093	5.87	.373907	5
56	.590686	4.97	.964240	.88	.626445	5.87	.373555	4
57	.590984	4.97	.964187	.90	.626797	5.87	.373203	3
58	.591282	4.97	.964133	.88	.627149	5.87	.372851	2
59	.591580	4.97	.964080	.90	.627501	5.85	.372499	1
60	9.591878		9.964026		9.627852		10.372148	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.
0	9.591878	4.97	9.964026	.90	9.627852	5.85	10.372148
1	.592176	4.95	.963972	.88	.628203	5.85	.371797
2	.592473	4.95	.963919	.90	.628554	5.85	.371446
3	.592770	4.95	.963865	.90	.628905	5.83	.371095
4	.593067	4.93	.963811	.90	.629255	5.85	.370745
5	.593363	4.93	.963757	.88	.629606	5.83	.370394
6	.593659	4.93	.963704	.90	.629956	5.83	.370044
7	.593955	4.93	.963650	.90	.630306	5.83	.369694
8	.594251	4.93	.963596	.90	.630656	5.82	.369344
9	.594547	4.92	.963542	.90	.631005	5.83	.368995
10	.594842	4.92	.963488	.90	.631355	5.82	.368645
11	9.595137	4.92	9.963434	.92	9.631704	5.82	10.368296
12	.595432	4.92	.963379	.90	.632053	5.82	.367947
13	.595727	4.90	.963325	.90	.632402	5.80	.367598
14	.596021	4.90	.963271	.90	.632750	5.82	.367250
15	.596315	4.90	.963217	.90	.633099	5.80	.366901
16	.596609	4.90	.963163	.92	.633447	5.80	.366553
17	.596903	4.88	.963108	.90	.633795	5.80	.366205
18	.597196	4.90	.963054	.92	.634143	5.78	.365857
19	.597490	4.88	.962999	.90	.634490	5.80	.365510
20	.597783	4.87	.962945	.92	.634838	5.78	.365162
21	9.598075	4.88	9.962890	.90	9.635185	5.78	10.364815
22	.598368	4.87	.962836	.92	.635532	5.78	.364468
23	.598660	4.87	.962781	.90	.635879	5.78	.364121
24	.598952	4.87	.962727	.92	.636226	5.77	.363774
25	.599244	4.87	.962672	.92	.636572	5.78	.363428
26	.599536	4.85	.962617	.92	.636919	5.77	.363081
27	.599827	4.85	.962562	.90	.637265	5.77	.362735
28	.600118	4.85	.962508	.92	.637611	5.75	.362389
29	.600409	4.85	.962453	.92	.637956	5.77	.362044
30	.600700	4.83	.962398	.92	.638302	5.75	.361698
31	9.600990	4.83	9.962343	.92	9.638647	5.75	10.361353
32	.601280	4.83	.962288	.92	.638992	5.75	.361008
33	.601570	4.83	.962233	.92	.639337	5.75	.360663
34	.601860	4.83	.962178	.92	.639682	5.75	.360318
35	.602150	4.82	.962123	.93	.640027	5.73	.359973
36	.602439	4.82	.962067	.92	.640371	5.75	.359629
37	.602728	4.82	.962012	.92	.640716	5.73	.359284
38	.603017	4.80	.961957	.92	.641060	5.73	.358940
39	.603305	4.82	.961902	.93	.641404	5.72	.358596
40	.603594	4.80	.961846	.92	.641747	5.73	.358253
41	9.603882	4.80	9.961791	.93	9.642091	5.72	10.357909
42	.604170	4.78	.961735	.92	.642434	5.72	.357566
43	.604457	4.80	.961680	.93	.642777	5.72	.357223
44	.604745	4.78	.961624	.92	.643120	5.72	.356880
45	.605032	4.78	.961569	.93	.643463	5.72	.356537
46	.605319	4.78	.961513	.92	.643806	5.70	.356194
47	.605606	4.77	.961458	.93	.644148	5.70	.355852
48	.605892	4.78	.961402	.93	.644490	5.70	.355510
49	.606179	4.77	.961346	.93	.644832	5.70	.355168
50	.606465	4.77	.961290	.92	.645174	5.70	.354826
51	9.606751	4.75	9.961235	.93	9.645516	5.68	10.354484
52	.607036	4.77	.961179	.93	.645857	5.70	.354143
53	.607322	4.75	.961123	.93	.646199	5.68	.353801
54	.607607	4.75	.961067	.93	.646540	5.68	.353460
55	.607892	4.75	.961011	.93	.646881	5.68	.353119
56	.608177	4.73	.960955	.93	.647222	5.67	.352778
57	.608461	4.73	.960899	.93	.647562	5.68	.352438
58	.608745	4.73	.960843	.95	.647903	5.67	.352097
59	.609029	4.73	.960786	.93	.648243	5.67	.351757
60	9.609313		9.960730		9.648583		10.351417
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.609313	4.73	9.960730	.93	9.648583	5.67	10.351417	60
1	.609597	4.72	.960674	.93	.648923	5.67	.351077	59
2	.609880	4.73	.960618	.95	.649263	5.65	.350737	58
3	.610164	4.72	.960561	.93	.649602	5.67	.350398	57
4	.610447	4.70	.960505	.95	.649942	5.65	.350058	56
5	.610729	4.72	.960448	.93	.650281	5.65	.349719	55
6	.611012	4.70	.960392	.95	.650620	5.65	.349380	54
7	.611294	4.70	.960335	.93	.650959	5.63	.349041	53
8	.611576	4.70	.960279	.95	.651297	5.65	.348703	52
9	.611858	4.70	.960222	.95	.651636	5.63	.348364	51
10	.612140	4.68	.960165	.93	.651974	5.63	.348026	50
11	9.612421	4.68	9.960109	.95	9.652312	5.63	10.347688	49
12	.612702	4.68	.960052	.95	.652650	5.63	.347350	48
13	.612983	4.68	.959995	.95	.652988	5.63	.347012	47
14	.613264	4.68	.959938	.93	.653326	5.62	.346674	46
15	.613545	4.67	.959882	.95	.653663	5.62	.346337	45
16	.613825	4.67	.959825	.95	.654000	5.62	.346000	44
17	.614105	4.67	.959768	.95	.654337	5.62	.345663	43
18	.614385	4.67	.959711	.95	.654674	5.62	.345326	42
19	.614665	4.65	.959654	.97	.655011	5.62	.344989	41
20	.614944	4.65	.959596	.95	.655348	5.60	.344652	40
21	9.615223	4.65	9.959539	.95	9.655684	5.60	10.344316	39
22	.615502	4.65	.959482	.95	.656020	5.60	.343980	38
23	.615781	4.65	.959425	.95	.656356	5.60	.343644	37
24	.616060	4.63	.959368	.97	.656692	5.60	.343308	36
25	.616338	4.63	.959310	.95	.657028	5.60	.342972	35
26	.616616	4.63	.959253	.97	.657364	5.58	.342636	34
27	.616894	4.63	.959195	.95	.657699	5.58	.342301	33
28	.617172	4.63	.959138	.97	.658034	5.58	.341966	32
29	.617450	4.62	.959080	.95	.658369	5.58	.341631	31
30	.617727	4.62	.959023	.97	.658704	5.58	.341296	30
31	9.618004	4.62	9.958965	.95	9.659039	5.57	10.340961	29
32	.618281	4.62	.958908	.97	.659373	5.58	.340627	28
33	.618558	4.60	.958850	.97	.659708	5.57	.340292	27
34	.618834	4.60	.958792	.97	.660042	5.57	.339958	26
35	.619110	4.60	.958734	.95	.660376	5.57	.339624	25
36	.619386	4.60	.958677	.97	.660710	5.55	.339290	24
37	.619662	4.60	.958619	.97	.661043	5.57	.338957	23
38	.619938	4.58	.958561	.97	.661377	5.55	.338623	22
39	.620213	4.58	.958503	.97	.661710	5.55	.338290	21
40	.620488	4.58	.958445	.97	.662043	5.55	.337957	20
41	9.620763	4.58	9.958387	.97	9.662376	5.55	10.337624	19
42	.621038	4.58	.958329	.97	.662709	5.55	.337291	18
43	.621313	4.57	.958271	.97	.663042	5.55	.336958	17
44	.621587	4.57	.958213	.98	.663375	5.53	.336625	16
45	.621861	4.57	.958154	.97	.663707	5.53	.336293	15
46	.622135	4.57	.958096	.97	.664039	5.53	.335961	14
47	.622409	4.55	.958038	.98	.664371	5.53	.335629	13
48	.622682	4.57	.957979	.97	.664703	5.53	.335297	12
49	.622956	4.55	.957921	.97	.665035	5.52	.334965	11
50	.623229	4.55	.957863	.98	.665366	5.53	.334634	10
51	9.623502	4.53	9.957804	.97	9.665698	5.52	10.334302	9
52	.623774	4.55	.957746	.98	.666029	5.52	.333971	8
53	.624047	4.53	.957687	.98	.666360	5.52	.333640	7
54	.624319	4.53	.957628	.97	.666691	5.50	.333309	6
55	.624591	4.53	.957570	.98	.667021	5.52	.332979	5
56	.624863	4.53	.957511	.98	.667352	5.50	.332648	4
57	.625135	4.52	.957452	.98	.667682	5.52	.332318	3
58	.625406	4.52	.957393	.97	.668013	5.50	.331987	2
59	.625677	4.52	.957335	.98	.668343	5.50	.331657	1
60	9.625948		9.957276		9.668673		10.331327	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

'	Sine.	D. 1".	Cosine.	D. 1".	Tang.	D. 1".	Cotang.
0	9.625948	4.52	9.957276	.98	9.668673	5.48	10.331327
1	.626219	4.52	.957217	.98	.669002	5.50	.330998
2	.626490	4.50	.957158	.98	.669332	5.48	.330668
3	.626760	4.50	.957099	.98	.669661	5.50	.330339
4	.627030	4.50	.957040	.98	.669991	5.48	.330009
5	.627300	4.50	.956981	1.00	.670320	5.48	.329680
6	.627570	4.50	.956921	.98	.670649	5.47	.329351
7	.627840	4.48	.956862	.98	.670977	5.48	.329023
8	.628109	4.48	.956803	.98	.671306	5.48	.328694
9	.628378	4.48	.956744	1.00	.671635	5.47	.328365
10	.628647	4.48	.956684	.98	.671963	5.47	.328037
11	9.628916	4.48	9.956625	.98	9.672291	5.47	10.327709
12	.629185	4.47	.956566	1.00	.672619	5.47	.327381
13	.629453	4.47	.956506	.98	.672947	5.45	.327053
14	.629721	4.47	.956447	1.00	.673274	5.47	.326726
15	.629989	4.47	.956387	1.00	.673602	5.45	.326398
16	.630257	4.45	.956327	.98	.673929	5.47	.326071
17	.630524	4.47	.956268	1.00	.674257	5.45	.325743
18	.630792	4.45	.956208	1.00	.674584	5.45	.325416
19	.631059	4.45	.956148	.98	.674911	5.43	.325089
20	.631326	4.45	.956089	1.00	.675237	5.45	.324763
21	9.631593	4.43	9.956029	1.00	9.675564	5.43	10.324436
22	.631859	4.43	.955969	1.00	.675890	5.45	.324110
23	.632125	4.45	.955909	1.00	.676217	5.43	.323783
24	.632392	4.43	.955849	1.00	.676543	5.43	.323457
25	.632658	4.42	.955789	1.00	.676869	5.42	.323131
26	.632923	4.43	.955729	1.00	.677194	5.43	.322806
27	.633189	4.42	.955669	1.00	.677520	5.43	.322480
28	.633454	4.42	.955609	.98	.677846	5.42	.322154
29	.633719	4.42	.955548	1.00	.678171	5.42	.321829
30	.633984	4.42	.955488	1.00	.678496	5.42	.321504
31	9.634249	4.42	9.955428	1.00	9.678821	5.42	10.321179
32	.634514	4.40	.955368	1.02	.679146	5.42	.320854
33	.634778	4.40	.955307	1.00	.679471	5.40	.320529
34	.635042	4.40	.955247	1.02	.679795	5.42	.320205
35	.635306	4.40	.955186	1.00	.680120	5.40	.319880
36	.635570	4.40	.955126	1.02	.680444	5.40	.319556
37	.635834	4.38	.955065	1.00	.680768	5.40	.319232
38	.636097	4.38	.955005	1.02	.681092	5.40	.318908
39	.636360	4.38	.954944	1.02	.681416	5.40	.318584
40	.636623	4.38	.954883	1.00	.681740	5.38	.318260
41	9.636886	4.37	9.954823	1.02	9.682063	5.40	10.317937
42	.637148	4.38	.954762	1.02	.682387	5.38	.317613
43	.637411	4.37	.954701	1.02	.682710	5.38	.317290
44	.637673	4.37	.954640	1.02	.683033	5.38	.316967
45	.637935	4.37	.954579	1.02	.683356	5.38	.316644
46	.638197	4.35	.954518	1.02	.683679	5.37	.316321
47	.638458	4.37	.954457	1.02	.684001	5.38	.315999
48	.638720	4.35	.954396	1.02	.684324	5.37	.315676
49	.638981	4.35	.954335	1.02	.684646	5.37	.315354
50	.639242	4.35	.954274	1.02	.684968	5.37	.315032
51	9.639503	4.35	9.954213	1.02	9.685290	5.37	10.314710
52	.639764	4.33	.954152	1.03	.685612	5.37	.314388
53	.640024	4.33	.954090	1.02	.685934	5.35	.314066
54	.640284	4.33	.954029	1.02	.686255	5.37	.313745
55	.640544	4.33	.953968	1.03	.686577	5.35	.313423
56	.640804	4.33	.953906	1.02	.686898	5.35	.313102
57	.641064	4.33	.953845	1.03	.687219	5.35	.312781
58	.641324	4.32	.953783	1.02	.687540	5.35	.312460
59	.641583	4.32	.953722	1.03	.687861	5.35	.312139
60	9.641842		9.953660		9.688182		10.311818
'	Cosine.	D. 1".	Sine.	D. 1".	Cotang.	D. 1".	Tang.

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.641842	4.32	9.953660	1.02	9.688182	5.33	10.311818	60
1	.642101	4.32	.953599	1.03	.688502	5.32	.311498	59
2	.642360	4.30	.953537	1.03	.688823	5.33	.311177	58
3	.642618	4.32	.953475	1.03	.689143	5.33	.310857	57
4	.642877	4.30	.953413	1.02	.689463	5.33	.310537	56
5	.643135	4.30	.953352	1.03	.689783	5.33	.310217	55
6	.643393	4.28	.953290	1.03	.690103	5.33	.309897	54
7	.643650	4.30	.953228	1.03	.690423	5.32	.309577	53
8	.643908	4.28	.953166	1.03	.690742	5.33	.309258	52
9	.644165	4.30	.953104	1.03	.691062	5.32	.308938	51
10	.644423	4.28	.953042	1.03	.691381	5.32	.308619	50
11	9.644680	4.27	9.952980	1.03	9.691700	5.32	10.308300	49
12	.644936	4.28	.952918	1.05	.692019	5.32	.307981	48
13	.645193	4.28	.952855	1.03	.692338	5.30	.307662	47
14	.645450	4.27	.952793	1.03	.692656	5.32	.307344	46
15	.645706	4.27	.952731	1.03	.692975	5.30	.307025	45
16	.645962	4.27	.952669	1.05	.693293	5.32	.306707	44
17	.646218	4.27	.952606	1.03	.693612	5.30	.306388	43
18	.646474	4.25	.952544	1.05	.693930	5.30	.306070	42
19	.646729	4.25	.952481	1.03	.694248	5.30	.305752	41
20	.646984	4.27	.952419	1.05	.694566	5.28	.305434	40
21	9.647240	4.23	9.952356	1.03	9.694883	5.30	10.305117	39
22	.647494	4.25	.952294	1.05	.695201	5.28	.304799	38
23	.647749	4.25	.952231	1.05	.695518	5.30	.304482	37
24	.648004	4.23	.952168	1.03	.695836	5.28	.304164	36
25	.648258	4.23	.952106	1.05	.696153	5.28	.303847	35
26	.648512	4.23	.952043	1.05	.696470	5.28	.303530	34
27	.648766	4.23	.951980	1.05	.696787	5.27	.303213	33
28	.649020	4.23	.951917	1.05	.697103	5.28	.302897	32
29	.649274	4.22	.951854	1.05	.697420	5.27	.302580	31
30	.649527	4.23	.951791	1.05	.697736	5.28	.302264	30
31	9.649781	4.22	9.951728	1.05	9.698053	5.27	10.301947	29
32	.650034	4.22	.951665	1.05	.698369	5.27	.301631	28
33	.650287	4.20	.951602	1.05	.698685	5.27	.301315	27
34	.650539	4.22	.951539	1.05	.699001	5.25	.300999	26
35	.650792	4.20	.951476	1.07	.699316	5.27	.300684	25
36	.651044	4.22	.951412	1.05	.699632	5.25	.300368	24
37	.651297	4.20	.951349	1.05	.699947	5.27	.300053	23
38	.651549	4.18	.951286	1.07	.700263	5.25	.299737	22
39	.651800	4.20	.951222	1.05	.700578	5.25	.299422	21
40	.652052	4.20	.951159	1.05	.700893	5.25	.299107	20
41	9.652304	4.18	9.951096	1.07	9.701208	5.25	10.298792	19
42	.652555	4.18	.951032	1.07	.701523	5.23	.298477	18
43	.652806	4.18	.950968	1.05	.701837	5.25	.298163	17
44	.653057	4.18	.950905	1.07	.702152	5.23	.297848	16
45	.653308	4.17	.950841	1.05	.702466	5.25	.297534	15
46	.653558	4.17	.950778	1.07	.702781	5.23	.297219	14
47	.653808	4.18	.950714	1.07	.703095	5.23	.296905	13
48	.654059	4.17	.950650	1.07	.703409	5.22	.296591	12
49	.654309	4.15	.950586	1.07	.703722	5.23	.296278	11
50	.654558	4.17	.950522	1.07	.704036	5.23	.295964	10
51	9.654808	4.17	9.950458	1.07	9.704350	5.22	10.295650	9
52	.655058	4.15	.950394	1.07	.704663	5.22	.295337	8
53	.655307	4.15	.950330	1.07	.704976	5.23	.295024	7
54	.655556	4.15	.950266	1.07	.705290	5.22	.294710	6
55	.655805	4.15	.950202	1.07	.705603	5.22	.294397	5
56	.656054	4.13	.950138	1.07	.705916	5.20	.294084	4
57	.656302	4.15	.950074	1.07	.706228	5.22	.293772	3
58	.656551	4.13	.950010	1.08	.706541	5.22	.293459	2
59	.656799	4.13	.949945	1.07	.706854	5.20	.293146	1
60	9.657047		9.949881		9.707166		10.292834	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.657047	4.13	9 949881	1.08	9 707166	5.20	10.292834	60
1	.657295	4.12	.949816	1 07	707478	5 20	.292522	59
2	.657542	4.13	.949752	1.07	.707790	5 20	.292210	58
3	.657790	4 12	.949688	1.08	708102	5.20	.291898	57
4	.658037	4.12	.949623	1.08	.708414	5.20	.291586	56
5	.658284	4.12	.949558	1.07	.708726	5.18	.291274	55
6	.658531	4.12	.949494	1.08	.709037	5 20	.290963	54
7	.658778	4.12	.949429	1.08	.709349	5.18	.290651	53
8	.659025	4.10	.949364	1.07	.709660	5.18	.290340	52
9	.659271	4.10	.949300	1.08	.709971	5.18	.290029	51
10	.659517	4.10	.949235	1.08	.710282	5.18	.289718	50
11	9.659763	4.10	9.949170	1.08	9.710593	5.18	10.289407	49
12	.660009	4 10	.949105	1.08	.710904	5 18	.289096	48
13	.660255	4 10	.949040	1.08	.711215	5.17	.288785	47
14	.660501	4 08	.948975	1.08	.711525	5.18	.288475	46
15	.660746	4.08	.948910	1.08	.711836	5.17	.288164	45
16	.660991	4.08	.948845	1.08	.712146	5.17	.287854	44
17	.661236	4.08	.948780	1.08	.712456	5.17	.287544	43
18	.661481	4.08	.948715	1.08	.712766	5 17	.287234	42
19	.661726	4.07	.948650	1.10	.713076	5.17	.286924	41
20	.661970	4 07	.948584	1 08	.713386	5.17	.286614	40
21	9.662214	4.08	9.948519	1.08	9.713696	5 15	10.286304	39
22	.662459	4.07	.948454	1.10	.714005	5.15	.285995	38
23	.662703	4 05	.948388	1 08	.714314	5.17	.285686	37
24	.662946	4.07	.948323	1.10	.714624	5 15	.285376	36
25	.663190	4.05	.948257	1.08	.714933	5.15	.285067	35
26	.663433	4.07	.948192	1.10	.715242	5.15	.284758	34
27	.663677	4.05	.948126	1.10	.715551	5.15	.284449	33
28	.663920	4.05	.948060	1.08	.715860	5.13	.284140	32
29	.664163	4 05	.947995	1.10	.716168	5.15	.283832	31
30	.664406	4.03	.947929	1.10	.716477	5.13	.283523	30
31	9.664648	4 05	9.947863	1.10	9.716785	5.13	10.283215	29
32	.664891	4.03	.947797	1.10	.717093	5 13	.282907	28
33	.665133	4.03	.947731	1.10	.717401	5.13	.282599	27
34	.665375	4.03	.947665	1.08	.717709	5.13	.282291	26
35	.665617	4.03	.947600	1.12	.718017	5.13	.281983	25
36	.665859	4.02	.947533	1.10	.718325	5.13	.281675	24
37	.666100	4.03	.947467	1.10	.718633	5.12	.281367	23
38	.666342	4.02	.947401	1.10	.718940	5.13	.281060	22
39	.666583	4.02	.947335	1.10	.719248	5.12	.280752	21
40	.666824	4.02	.947269	1.10	.719555	5.12	.280445	20
41	9.667065	4.00	9.947203	1.12	9.719862	5.12	10.280138	19
42	.667305	4.02	.947136	1.10	.720169	5.12	.279831	18
43	.667546	4.00	.947070	1.10	.720476	5.12	.279524	17
44	.667786	4.02	.947004	1.12	.720783	5.10	.279217	16
45	.668027	4.00	.946937	1.10	.721089	5.12	.278911	15
46	.668267	3.98	.946871	1.12	.721396	5.10	.278604	14
47	.668506	4.00	.946804	1.10	.721702	5.12	.278298	13
48	.668746	4.00	.946738	1.12	.722009	5.10	.277991	12
49	.668986	3.98	.946671	1.12	.722315	5.10	.277685	11
50	.669225	3.98	.946604	1.10	.722621	5.10	.277379	10
51	9.669464	3.98	9.946538	1.12	9.722927	5.08	10.277073	9
52	.669703	3.98	.946471	1.12	.723232	5.10	.276768	8
53	.669942	3.98	.946404	1.12	.723538	5.10	.276462	7
54	670181	3.97	.946337	1.12	.723844	5.08	.276156	6
55	.670419	3.98	.946270	1.12	.724149	5.08	.275851	5
56	.670658	3.97	.946203	1.12	.724454	5.10	.275546	4
57	.670896	3.97	.946136	1.12	.724760	5.08	.275240	3
58	.671134	3.97	.946069	1.12	.725065	5.08	.274935	2
59	.671372	3.95	.946002	1.12	.725370	5.07	.274630	1
60	9.671609		9.945935		9.725674		10.274326	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.671609	3.97	9.945935	1.12	9.725674	5.08	10.274326	60
1	.671847	3.95	.945868	1.13	.725979	5.08	.274021	59
2	.672084	3.95	.945800	1.12	.726284	5.07	.273716	58
3	.672321	3.95	.945733	1.12	.726588	5.07	.273412	57
4	.672558	3.95	.945666	1.13	.726892	5.05	.273108	56
5	.672795	3.95	.945598	1.12	.727197	5.07	.272803	55
6	.673032	3.93	.945531	1.12	.727501	5.07	.272499	54
7	.673268	3.95	.945464	1.13	.727805	5.07	.272195	53
8	.673505	3.93	.945396	1.13	.728109	5.05	.271891	52
9	.673741	3.93	.945328	1.12	.728412	5.07	.271588	51
10	.673977	3.93	.945261	1.13	.728716	5.07	.271284	50
11	9.674213	3.92	9.945193	1.13	9.729020	5.05	10.270980	49
12	.674448	3.93	.945125	1.12	.729323	5.05	.270677	48
13	.674684	3.92	.945058	1.13	.729626	5.05	.270374	47
14	.674919	3.93	.944990	1.13	.729929	5.07	.270071	46
15	.675155	3.92	.944922	1.13	.730233	5.03	.269767	45
16	.675390	3.90	.944854	1.13	.730535	5.05	.269465	44
17	.675624	3.92	.944786	1.13	.730838	5.05	.269162	43
18	.675859	3.92	.944718	1.13	.731141	5.05	.268859	42
19	.676094	3.90	.944650	1.13	.731444	5.03	.268556	41
20	.676328	3.90	.944582	1.13	.731746	5.03	.268254	40
21	9.676562	3.90	9.944514	1.13	9.732048	5.05	10.267952	39
22	.676796	3.90	.944446	1.15	.732351	5.03	.267649	38
23	.677030	3.90	.944377	1.13	.732653	5.03	.267347	37
24	.677264	3.90	.944309	1.13	.732955	5.03	.267045	36
25	.677498	3.88	.944241	1.15	.733257	5.02	.266743	35
26	.677731	3.88	.944172	1.13	.733558	5.03	.266442	34
27	.677964	3.88	.944104	1.13	.733860	5.03	.266140	33
28	.678197	3.88	.944036	1.15	.734162	5.02	.265838	32
29	.678430	3.88	.943967	1.13	.734463	5.02	.265537	31
30	.678663	3.87	.943899	1.15	.734764	5.03	.265236	30
31	9.678895	3.88	9.943830	1.15	9.735066	5.02	10.264934	29
32	.679128	3.87	.943761	1.13	.735367	5.02	.264633	28
33	.679360	3.87	.943693	1.15	.735668	5.02	.264332	27
34	.679592	3.87	.943624	1.15	.735969	5.00	.264031	26
35	.679824	3.87	.943555	1.15	.736269	5.02	.263731	25
36	.680056	3.87	.943486	1.15	.736570	5.00	.263430	24
37	.680288	3.85	.943417	1.15	.736870	5.02	.263130	23
38	.680519	3.85	.943348	1.15	.737171	5.00	.262829	22
39	.680750	3.87	.943279	1.15	.737471	5.00	.262529	21
40	.680982	3.85	.943210	1.15	.737771	5.00	.262229	20
41	9.681213	3.83	9.943141	1.15	9.738071	5.00	10.261929	19
42	.681443	3.85	.943072	1.15	.738371	5.00	.261629	18
43	.681674	3.85	.943003	1.15	.738671	5.00	.261329	17
44	.681905	3.83	.942934	1.17	.738971	5.00	.261029	16
45	.682135	3.83	.942864	1.15	.739271	4.98	.260729	15
46	.682365	3.83	.942795	1.15	.739570	5.00	.260430	14
47	.682595	3.83	.942726	1.17	.739870	4.98	.260130	13
48	.682825	3.83	.942656	1.15	.740169	4.98	.259831	12
49	.683055	3.82	.942587	1.17	.740468	4.98	.259532	11
50	.683284	3.83	.942517	1.15	.740767	4.98	.259233	10
51	9.683514	3.82	9.942448	1.17	9.741066	4.98	10.258934	9
52	.683743	3.82	.942378	1.17	.741365	4.98	.258635	8
53	.683972	3.82	.942308	1.15	.741664	4.97	.258336	7
54	.684201	3.82	.942239	1.17	.741962	4.98	.258038	6
55	.684430	3.80	.942169	1.17	.742261	4.97	.257739	5
56	.684658	3.82	.942099	1.17	.742559	4.98	.257441	4
57	.684887	3.80	.942029	1.17	.742858	4.97	.257142	3
58	.685115	3.80	.941959	1.17	.743156	4.97	.256844	2
59	.685343	3.80	.941889	1.17	.743454	4.97	.256546	1
60	9.685571		9.941819		9.743752		10.256248	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.685571	3.80	9.941819	1.17	9.743752	4.97	10.256248	60
1	.685799	3.80	.941749	1.17	.744050	4.97	.255950	59
2	.686027	3.78	.941679	1.17	.744348	4.95	.255652	58
3	.686254	3.80	.941609	1.17	.744645	4.97	.255355	57
4	.686482	3.78	.941539	1.17	.744943	4.95	.255057	56
5	.686709	3.78	.941469	1.18	.745240	4.97	.254760	55
6	.686936	3.78	.941398	1.17	.745538	4.95	.254462	54
7	.687163	3.77	.941328	1.17	.745835	4.95	.254165	53
8	.687389	3.78	.941258	1.18	.746132	4.95	.253868	52
9	.687616	3.78	.941187	1.17	.746429	4.95	.253571	51
10	.687843	3.77	.941117	1.18	.746726	4.95	.253274	50
11	9.688069	3.77	9.941046	1.18	9.747023	4.93	10.252977	49
12	.688295	3.77	.940975	1.17	.747319	4.95	.252681	48
13	.688521	3.77	.940905	1.18	.747616	4.95	.252384	47
14	.688747	3.75	.940834	1.18	.747913	4.93	.252087	46
15	.688972	3.77	.940763	1.17	.748209	4.93	.251791	45
16	.689198	3.75	.940693	1.18	.748505	4.93	.251495	44
17	.689423	3.75	.940622	1.18	.748801	4.93	.251199	43
18	.689648	3.75	.940551	1.18	.749097	4.93	.250903	42
19	.689873	3.75	.940480	1.18	.749393	4.93	.250607	41
20	.690098	3.75	.940409	1.18	.749689	4.93	.250311	40
21	9.690323	3.75	9.940338	1.18	9.749985	4.93	10.250015	39
22	.690548	3.73	.940267	1.18	.750281	4.92	.249719	38
23	.690772	3.73	.940196	1.18	.750576	4.93	.249424	37
24	.690996	3.73	.940125	1.18	.750872	4.92	.249128	36
25	.691220	3.73	.940054	1.20	.751167	4.92	.248833	35
26	.691444	3.73	.939982	1.18	.751462	4.92	.248538	34
27	.691668	3.73	.939911	1.18	.751757	4.92	.248243	33
28	.691892	3.72	.939840	1.20	.752052	4.92	.247948	32
29	.692115	3.73	.939768	1.18	.752347	4.92	.247653	31
30	.692339	3.72	.939697	1.20	.752642	4.92	.247358	30
31	9.692562	3.72	9.939625	1.18	9.752937	4.90	10.247063	29
32	.692785	3.72	.939554	1.20	.753231	4.92	.246769	28
33	.693008	3.72	.939482	1.20	.753526	4.90	.246474	27
34	.693231	3.70	.939410	1.18	.753820	4.92	.246180	26
35	.693453	3.72	.939339	1.20	.754115	4.90	.245885	25
36	.693676	3.70	.939267	1.20	.754409	4.90	.245591	24
37	.693898	3.70	.939195	1.20	.754703	4.90	.245297	23
38	.694120	3.70	.939123	1.18	.754997	4.90	.245003	22
39	.694342	3.70	.939052	1.20	.755291	4.90	.244709	21
40	.694564	3.70	.938980	1.20	.755585	4.88	.244415	20
41	9.694786	3.68	9.938908	1.20	9.755878	4.90	10.244122	19
42	.695007	3.70	.938836	1.22	.756172	4.88	.243828	18
43	.695229	3.68	.938763	1.20	.756465	4.90	.243535	17
44	.695450	3.68	.938691	1.20	.756759	4.88	.243241	16
45	.695671	3.68	.938619	1.20	.757052	4.88	.242948	15
46	.695892	3.68	.938547	1.20	.757345	4.88	.242655	14
47	.696113	3.68	.938475	1.22	.757638	4.88	.242362	13
48	.696334	3.67	.938402	1.20	.757931	4.88	.242069	12
49	.696554	3.68	.938330	1.20	.758224	4.88	.241776	11
50	.696775	3.67	.938258	1.22	.758517	4.88	.241483	10
51	9.696995	3.67	9.938185	1.20	9.758810	4.87	10.241190	9
52	.697215	3.67	.938113	1.22	.759102	4.88	.240898	8
53	.697435	3.65	.938040	1.22	.759395	4.87	.240605	7
54	.697654	3.67	.937967	1.20	.759687	4.87	.240313	6
55	.697874	3.67	.937895	1.22	.759979	4.88	.240021	5
56	.698094	3.65	.937822	1.22	.760272	4.87	.239728	4
57	.698313	3.65	.937749	1.22	.760564	4.87	.239436	3
58	.698532	3.65	.937676	1.20	.760856	4.87	.239144	2
59	.698751	3.65	.937604	1.22	.761148	4.85	.238852	1
60	9.698970		9.937531		9.761439		10.238561	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.671609	3.97	9.945935	1.12	9.725674	5.08	10.274326	60
1	.671847	3.95	.945868	1.13	.725979	5.08	.274021	59
2	.672084	3.95	.945800	1.12	.726284	5.07	.273716	58
3	.672321	3.95	.945733	1.12	.726588	5.07	.273412	57
4	.672558	3.95	.945666	1.13	.726892	5.05	.273108	56
5	.672795	3.95	.945598	1.12	.727197	5.07	.272803	55
6	.673032	3.93	.945531	1.12	.727501	5.07	.272499	54
7	.673268	3.95	.945464	1.13	.727805	5.07	.272195	53
8	.673505	3.93	.945396	1.13	.728109	5.05	.271891	52
9	.673741	3.93	.945328	1.12	.728412	5.07	.271588	51
10	.673977	3.93	.945261	1.13	.728716	5.07	.271284	50
11	9.674213	3.92	9.945193	1.13	9.729020	5.05	10.270980	49
12	.674448	3.93	.945125	1.12	.729323	5.05	.270677	48
13	.674684	3.92	.945058	1.13	.729626	5.05	.270374	47
14	.674919	3.93	.944990	1.13	.729929	5.07	.270071	46
15	.675155	3.92	.944922	1.13	.730233	5.03	.269767	45
16	.675390	3.90	.944854	1.13	.730535	5.05	.269465	44
17	.675624	3.92	.944786	1.13	.730838	5.05	.269162	43
18	.675859	3.92	.944718	1.13	.731141	5.05	.268859	42
19	.676094	3.90	.944650	1.13	.731444	5.03	.268556	41
20	.676328	3.90	.944582	1.13	.731746	5.03	.268254	40
21	9.676562	3.90	9.944514	1.13	9.732048	5.05	10.267952	39
22	.676796	3.90	.944446	1.15	.732351	5.03	.267649	38
23	.677030	3.90	.944377	1.13	.732653	5.03	.267347	37
24	.677264	3.90	.944309	1.13	.732955	5.03	.267045	36
25	.677498	3.88	.944241	1.15	.733257	5.02	.266743	35
26	.677731	3.88	.944172	1.13	.733558	5.03	.266442	34
27	.677964	3.88	.944104	1.13	.733860	5.03	.266140	33
28	.678197	3.88	.944036	1.15	.734162	5.02	.265838	32
29	.678430	3.88	.943967	1.13	.734463	5.02	.265537	31
30	.678663	3.87	.943899	1.15	.734764	5.03	.265236	30
31	9.678895	3.88	9.943830	1.15	9.735066	5.02	10.264934	29
32	.679128	3.87	.943761	1.13	.735367	5.02	.264633	28
33	.679360	3.87	.943693	1.15	.735668	5.02	.264332	27
34	.679592	3.87	.943624	1.15	.735969	5.00	.264031	26
35	.679824	3.87	.943555	1.15	.736269	5.02	.263731	25
36	.680056	3.87	.943486	1.15	.736570	5.00	.263430	24
37	.680288	3.85	.943417	1.15	.736870	5.02	.263130	23
38	.680519	3.85	.943348	1.15	.737171	5.00	.262829	22
39	.680750	3.87	.943279	1.15	.737471	5.00	.262529	21
40	.680982	3.85	.943210	1.15	.737771	5.00	.262229	20
41	9.681213	3.83	9.943141	1.15	9.738071	5.00	10.261929	19
42	.681443	3.85	.943072	1.15	.738371	5.00	.261629	18
43	.681674	3.85	.943003	1.15	.738671	5.00	.261329	17
44	.681905	3.83	.942934	1.17	.738971	5.00	.261029	16
45	.682135	3.83	.942864	1.15	.739271	4.98	.260729	15
46	.682365	3.83	.942795	1.15	.739570	5.00	.260430	14
47	.682595	3.83	.942726	1.17	.739870	4.98	.260130	13
48	.682825	3.83	.942656	1.15	.740169	4.98	.259831	12
49	.683055	3.82	.942587	1.17	.740468	4.98	.259532	11
50	.683284	3.83	.942517	1.15	.740767	4.98	.259233	10
51	9.683514	3.82	9.942448	1.17	9.741066	4.98	10.258934	9
52	.683743	3.82	.942378	1.17	.741365	4.98	.258635	8
53	.683972	3.82	.942308	1.15	.741664	4.97	.258336	7
54	.684201	3.82	.942239	1.17	.741962	4.98	.258038	6
55	.684430	3.80	.942169	1.17	.742261	4.97	.257739	5
56	.684658	3.82	.942099	1.17	.742559	4.98	.257441	4
57	.684887	3.80	.942029	1.17	.742858	4.97	.257142	3
58	.685115	3.80	.941959	1.17	.743156	4.97	.256844	2
59	.685343	3.80	.941889	1.17	.743454	4.97	.256546	1
60	9.685571		9.941819		9.743752		10.256248	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.685571	3.80	9.941819	1.17	9.743752	4.97	10.256248	60
1	.685799	3.80	.941749	1.17	.744050	4.97	.255950	59
2	.686027	3.78	.941679	1.17	.744348	4.95	.255652	58
3	.686254	3.80	.941609	1.17	.744645	4.97	.255355	57
4	.686482	3.78	.941539	1.17	.744943	4.95	.255057	56
5	.686709	3.78	.941469	1.18	.745240	4.97	.254760	55
6	.686936	3.78	.941398	1.17	.745538	4.95	.254462	54
7	.687163	3.77	.941328	1.17	.745835	4.95	.254165	53
8	.687389	3.78	.941258	1.18	.746132	4.95	.253868	52
9	.687616	3.78	.941187	1.17	.746429	4.95	.253571	51
10	.687843	3.77	.941117	1.18	.746726	4.95	.253274	50
11	9.688069	3.77	9.941046	1.18	9.747023	4.93	10.252977	49
12	.688295	3.77	.940975	1.17	.747319	4.95	.252681	48
13	.688521	3.77	.940905	1.18	.747616	4.95	.252384	47
14	.688747	3.75	.940834	1.18	.747913	4.93	.252087	46
15	.688972	3.77	.940763	1.17	.748209	4.93	.251791	45
16	.689198	3.75	.940693	1.18	.748505	4.93	.251495	44
17	.689423	3.75	.940622	1.18	.748801	4.93	.251199	43
18	.689648	3.75	.940551	1.18	.749097	4.93	.250903	42
19	.689873	3.75	.940480	1.18	.749393	4.93	.250607	41
20	.690098	3.75	.940409	1.18	.749689	4.93	.250311	40
21	9.690323	3.75	9.940338	1.18	9.749985	4.93	10.250015	39
22	.690548	3.73	.940267	1.18	.750281	4.92	.249719	38
23	.690772	3.73	.940196	1.18	.750576	4.93	.249424	37
24	.690996	3.73	.940125	1.18	.750872	4.92	.249128	36
25	.691220	3.73	.940054	1.20	.751167	4.92	.248833	35
26	.691444	3.73	.939982	1.18	.751462	4.92	.248538	34
27	.691668	3.73	.939911	1.18	.751757	4.92	.248243	33
28	.691892	3.72	.939840	1.20	.752052	4.92	.247948	32
29	.692115	3.73	.939768	1.18	.752347	4.92	.247653	31
30	.692339	3.72	.939697	1.20	.752642	4.92	.247358	30
31	9.692562	3.72	9.939625	1.18	9.752937	4.90	10.247063	29
32	.692785	3.72	.939554	1.20	.753231	4.92	.246769	28
33	.693008	3.72	.939482	1.20	.753526	4.90	.246474	27
34	.693231	3.70	.939410	1.18	.753820	4.92	.246180	26
35	.693453	3.72	.939339	1.20	.754115	4.90	.245885	25
36	.693676	3.70	.939267	1.20	.754409	4.90	.245591	24
37	.693898	3.70	.939195	1.20	.754703	4.90	.245297	23
38	.694120	3.70	.939123	1.18	.754997	4.90	.245003	22
39	.694342	3.70	.939052	1.20	.755291	4.90	.244709	21
40	.694564	3.70	.938980	1.20	.755585	4.88	.244415	20
41	9.694786	3.68	9.938908	1.20	9.755878	4.90	10.244122	19
42	.695007	3.70	.938836	1.22	.756172	4.88	.243828	18
43	.695229	3.68	.938763	1.20	.756465	4.90	.243535	17
44	.695450	3.68	.938691	1.20	.756759	4.88	.243241	16
45	.695671	3.68	.938619	1.20	.757052	4.88	.242948	15
46	.695892	3.68	.938547	1.20	.757345	4.88	.242655	14
47	.696113	3.68	.938475	1.22	.757638	4.88	.242362	13
48	.696334	3.67	.938402	1.20	.757931	4.88	.242069	12
49	.696554	3.68	.938330	1.20	.758224	4.88	.241776	11
50	.696775	3.67	.938258	1.22	.758517	4.88	.241483	10
51	9.696995	3.67	9.938185	1.20	9.758810	4.87	10.241190	9
52	.697215	3.67	.938113	1.22	.759102	4.88	.240898	8
53	.697435	3.65	.938040	1.22	.759395	4.87	.240605	7
54	.697654	3.67	.937967	1.20	.759687	4.87	.240313	6
55	.697874	3.67	.937895	1.22	.759979	4.88	.240021	5
56	.698094	3.65	.937822	1.22	.760272	4.87	.239728	4
57	.698313	3.65	.937749	1.22	.760564	4.87	.239436	3
58	.698532	3.65	.937676	1.20	.760856	4.87	.239144	2
59	.698751	3.65	.937604	1.22	.761148	4.85	.238852	1
60	9.698970		9.937531		9.761439		10.238561	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.698970	3.65	9.937531	1.22	9.761439	4.87	10.238561	60
1	.699189	3.63	.937458	1.22	.761731	4.87	.238269	59
2	.699407	3.65	.937385	1.22	.762023	4.85	.237977	58
3	.699626	3.63	.937312	1.23	.762314	4.87	.237686	57
4	.699844	3.63	.937238	1.22	.762606	4.85	.237394	56
5	.700062	3.63	.937165	1.22	.762897	4.85	.237103	55
6	.700280	3.63	.937092	1.22	.763188	4.85	.236812	54
7	.700498	3.63	.937019	1.22	.763479	4.85	.236521	53
8	.700716	3.62	.936946	1.23	.763770	4.85	.236230	52
9	.700933	3.63	.936872	1.22	.764061	4.85	.235939	51
10	.701151	3.62	.936799	1.23	.764352	4.85	.235648	50
11	9.701368	3.62	9.936725	1.22	9.764643	4.83	10.235357	49
12	.701585	3.62	.936652	1.23	.764933	4.85	.235067	48
13	.701802	3.62	.936578	1.22	.765224	4.83	.234776	47
14	.702019	3.62	.936505	1.23	.765514	4.85	.234486	46
15	.702236	3.60	.936431	1.23	.765805	4.83	.234195	45
16	.702452	3.62	.936357	1.22	.766095	4.83	.233905	44
17	.702669	3.60	.936284	1.23	.766385	4.83	.233615	43
18	.702885	3.60	.936210	1.23	.766675	4.83	.233325	42
19	.703101	3.60	.936136	1.23	.766965	4.83	.233035	41
20	.703317	3.60	.936062	1.23	.767255	4.83	.232745	40
21	9.703533	3.60	9.935988	1.23	9.767545	4.82	10.232455	39
22	.703749	3.58	.935914	1.23	.767834	4.83	.232166	38
23	.703964	3.58	.935840	1.23	.768124	4.83	.231876	37
24	.704179	3.60	.935766	1.23	.768414	4.82	.231586	36
25	.704395	3.58	.935692	1.23	.768703	4.82	.231297	35
26	.704610	3.58	.935618	1.25	.768992	4.82	.231008	34
27	.704825	3.58	.935543	1.23	.769281	4.83	.230719	33
28	.705040	3.57	.935469	1.23	.769571	4.82	.230429	32
29	.705254	3.58	.935395	1.25	.769860	4.80	.230140	31
30	.705469	3.57	.935320	1.23	.770148	4.82	.229852	30
31	9.705683	3.58	9.935246	1.25	9.770437	4.82	10.229563	29
32	.705898	3.57	.935171	1.23	.770726	4.82	.229274	28
33	.706112	3.57	.935097	1.25	.771015	4.80	.228985	27
34	.706326	3.55	.935022	1.23	.771303	4.82	.228697	26
35	.706539	3.57	.934948	1.25	.771592	4.80	.228408	25
36	.706753	3.57	.934873	1.25	.771880	4.80	.228120	24
37	.706967	3.55	.934798	1.25	.772168	4.82	.227832	23
38	.707180	3.55	.934723	1.23	.772457	4.80	.227543	22
39	.707393	3.55	.934649	1.25	.772745	4.80	.227255	21
40	.707606	3.55	.934574	1.25	.773033	4.80	.226967	20
41	9.707819	3.55	9.934499	1.25	9.773321	4.78	10.226679	19
42	.708032	3.55	.934424	1.25	.773608	4.80	.226392	18
43	.708245	3.55	.934349	1.25	.773896	4.80	.226104	17
44	.708458	3.53	.934274	1.25	.774184	4.78	.225816	16
45	.708670	3.53	.934199	1.27	.774471	4.80	.225529	15
46	.708882	3.53	.934123	1.25	.774759	4.78	.225241	14
47	.709094	3.53	.934048	1.25	.775046	4.78	.224954	13
48	.709306	3.53	.933973	1.25	.775333	4.80	.224667	12
49	.709518	3.53	.933898	1.27	.775621	4.78	.224379	11
50	.709730	3.52	.933822	1.25	.775908	4.78	.224092	10
51	9.709941	3.53	9.933747	1.27	9.776195	4.78	10.223805	9
52	.710153	3.52	.933671	1.25	.776482	4.77	.223518	8
53	.710364	3.52	.933596	1.27	.776768	4.78	.223232	7
54	.710575	3.52	.933520	1.25	.777055	4.78	.222945	6
55	.710786	3.52	.933445	1.27	.777342	4.77	.222658	5
56	.710997	3.52	.933369	1.27	.777628	4.78	.222372	4
57	.711208	3.52	.933293	1.27	.777915	4.77	.222085	3
58	.711419	3.50	.933217	1.27	.778201	4.78	.221799	2
59	.711629	3.50	.933141	1.25	.778488	4.77	.221512	1
60	9.711839		9.933066		9.778774		10.221226	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.711839	3.52	9.933066	1.27	9.778774	4.77	10.221226	60
1	.712050	3.50	.932990	1.27	.779060	4.77	.220940	59
2	.712260	3.48	.932914	1.27	.779346	4.77	.220654	58
3	.712469	3.50	.932838	1.27	.779632	4.77	.220368	57
4	.712679	3.50	.932762	1.28	.779918	4.75	.220082	56
5	.712889	3.48	.932685	1.27	.780203	4.77	.219797	55
6	.713098	3.50	.932609	1.27	.780489	4.77	.219511	54
7	.713308	3.48	.932533	1.27	.780775	4.75	.219225	53
8	.713517	3.48	.932457	1.28	.781060	4.77	.218940	52
9	.713726	3.48	.932380	1.27	.781346	4.75	.218654	51
10	.713935	3.48	.932304	1.27	.781631	4.75	.218369	50
11	9.714144	3.47	9.932228	1.28	9.781916	4.75	10.218084	49
12	.714352	3.48	.932151	1.27	.782201	4.75	.217799	48
13	.714561	3.47	.932075	1.28	.782486	4.75	.217514	47
14	.714769	3.48	.931998	1.28	.782771	4.75	.217229	46
15	.714978	3.47	.931921	1.27	.783056	4.75	.216944	45
16	.715186	3.47	.931845	1.28	.783341	4.75	.216659	44
17	.715394	3.47	.931768	1.28	.783626	4.73	.216374	43
18	.715602	3.45	.931691	1.28	.783910	4.75	.216090	42
19	.715809	3.47	.931614	1.28	.784195	4.73	.215805	41
20	.716017	3.45	.931537	1.28	.784479	4.75	.215521	40
21	9.716224	3.47	9.931460	1.28	9.784764	4.73	10.215236	39
22	.716432	3.45	.931383	1.28	.785048	4.73	.214952	38
23	.716639	3.45	.931306	1.28	.785332	4.73	.214668	37
24	.716846	3.45	.931229	1.28	.785616	4.73	.214384	36
25	.717053	3.43	.931152	1.28	.785900	4.73	.214100	35
26	.717259	3.45	.931075	1.28	.786184	4.73	.213816	34
27	.717466	3.45	.930998	1.28	.786468	4.73	.213532	33
28	.717673	3.43	.930921	1.30	.786752	4.73	.213248	32
29	.717879	3.43	.930843	1.28	.787036	4.72	.212964	31
30	.718085	3.43	.930766	1.30	.787319	4.73	.212681	30
31	9.718291	3.43	9.930688	1.28	9.787603	4.72	10.212397	29
32	.718497	3.43	.930611	1.30	.787886	4.73	.212114	28
33	.718703	3.43	.930533	1.28	.788170	4.72	.211830	27
34	.718909	3.42	.930456	1.30	.788453	4.72	.211547	26
35	.719114	3.43	.930378	1.30	.788736	4.72	.211264	25
36	.719320	3.42	.930300	1.28	.789019	4.72	.210981	24
37	.719525	3.42	.930223	1.30	.789302	4.72	.210698	23
38	.719730	3.42	.930145	1.30	.789585	4.72	.210415	22
39	.719935	3.42	.930067	1.30	.789868	4.72	.210132	21
40	.720140	3.42	.929989	1.30	.790151	4.72	.209849	20
41	9.720345	3.40	9.929911	1.30	9.790434	4.70	10.209566	19
42	.720549	3.42	.929833	1.30	.790716	4.72	.209284	18
43	.720754	3.40	.929755	1.30	.790999	4.70	.209001	17
44	.720958	3.40	.929677	1.30	.791281	4.70	.208719	16
45	.721162	3.40	.929599	1.30	.791563	4.72	.208437	15
46	.721366	3.40	.929521	1.32	.791846	4.70	.208154	14
47	.721570	3.40	.929442	1.30	.792128	4.70	.207872	13
48	.721774	3.40	.929364	1.30	.792410	4.70	.207590	12
49	.721978	3.38	.929286	1.32	.792692	4.70	.207308	11
50	.722181	3.40	.929207	1.30	.792974	4.70	.207026	10
51	9.722385	3.38	9.929129	1.32	9.793256	4.70	10.206744	9
52	.722588	3.38	.929050	1.30	.793538	4.68	.206462	8
53	.722791	3.38	.928972	1.32	.793819	4.70	.206181	7
54	.722994	3.38	.928893	1.30	.794101	4.70	.205899	6
55	.723197	3.38	.928815	1.32	.794383	4.68	.205617	5
56	.723400	3.38	.928736	1.32	.794664	4.70	.205336	4
57	.723603	3.37	.928657	1.32	.794946	4.68	.205054	3
58	.723805	3.37	.928578	1.32	.795227	4.68	.204773	2
59	.724007	3.38	.928499	1.32	.795508	4.68	.204492	1
60	9.724210		9.928420		9.795789		10.204211	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.724210	3.37	9.928420	1.30	9.795789	4.68	10.204211	60
1	.724412	3.37	.928342	1.32	.796070	4.68	.203930	59
2	.724614	3.37	.928263	1.33	.796351	4.68	.203649	58
3	.724816	3.35	.928183	1.32	.796632	4.68	.203368	57
4	.725017	3.37	.928104	1.32	.796913	4.68	.203087	56
5	.725219	3.35	.928025	1.32	.797194	4.67	.202806	55
6	.725420	3.37	.927946	1.32	.797474	4.68	.202526	54
7	.725622	3.35	.927867	1.33	.797755	4.68	.202245	53
8	.725823	3.35	.927787	1.32	.798036	4.67	.201964	52
9	.726024	3.35	.927708	1.32	.798316	4.67	.201684	51
10	.726225	3.35	.927629	1.33	.798596	4.68	.201404	50
11	9.726426	3.33	9.927549	1.32	9.798877	4.67	10.201123	49
12	.726626	3.35	.927470	1.33	.799157	4.67	.200843	48
13	.726827	3.33	.927390	1.33	.799437	4.67	.200563	47
14	.727027	3.35	.927310	1.32	.799717	4.67	.200283	46
15	.727228	3.33	.927231	1.33	.799997	4.67	.200003	45
16	.727428	3.33	.927151	1.33	.800277	4.67	.199723	44
17	.727628	3.33	.927071	1.33	.800557	4.65	.199443	43
18	.727828	3.32	.926991	1.33	.800836	4.67	.199164	42
19	.728027	3.33	.926911	1.33	.801116	4.67	.198884	41
20	.728227	3.33	.926831	1.33	.801396	4.65	.198604	40
21	9.728427	3.32	9.926751	1.33	9.801675	4.67	10.198325	39
22	.728626	3.32	.926671	1.33	.801955	4.65	.198045	38
23	.728825	3.32	.926591	1.33	.802234	4.65	.197766	37
24	.729024	3.32	.926511	1.33	.802513	4.65	.197487	36
25	.729223	3.32	.926431	1.33	.802792	4.67	.197208	35
26	.729422	3.32	.926351	1.35	.803072	4.65	.196928	34
27	.729621	3.32	.926270	1.33	.803351	4.65	.196649	33
28	.729820	3.30	.926190	1.33	.803630	4.65	.196370	32
29	.730018	3.32	.926110	1.35	.803909	4.63	.196091	31
30	.730217	3.30	.926029	1.33	.804187	4.65	.195813	30
31	9.730415	3.30	9.925949	1.35	9.804466	4.65	10.195534	29
32	.730613	3.30	.925868	1.33	.804745	4.63	.195255	28
33	.730811	3.30	.925788	1.35	.805023	4.65	.194977	27
34	.731009	3.28	.925707	1.35	.805302	4.63	.194698	26
35	.731206	3.30	.925626	1.35	.805580	4.65	.194420	25
36	.731404	3.30	.925545	1.33	.805859	4.63	.194141	24
37	.731602	3.28	.925465	1.35	.806137	4.63	.193863	23
38	.731799	3.28	.925384	1.35	.806415	4.63	.193585	22
39	.731996	3.28	.925303	1.35	.806693	4.63	.193307	21
40	.732193	3.28	.925222	1.35	.806971	4.63	.193029	20
41	9.732390	3.28	9.925141	1.35	9.807249	4.63	10.192751	19
42	.732587	3.28	.925060	1.35	.807527	4.63	.192473	18
43	.732784	3.27	.924979	1.37	.807805	4.63	.192195	17
44	.732980	3.28	.924897	1.35	.808083	4.63	.191917	16
45	.733177	3.27	.924816	1.35	.808361	4.62	.191639	15
46	.733373	3.27	.924735	1.35	.808638	4.63	.191362	14
47	.733569	3.27	.924654	1.37	.808916	4.62	.191084	13
48	.733765	3.27	.924572	1.35	.809193	4.63	.190807	12
49	.733961	3.27	.924491	1.37	.809471	4.62	.190529	11
50	.734157	3.27	.924409	1.35	.809748	4.62	.190252	10
51	9.734353	3.27	9.924328	1.37	9.810025	4.62	10.189975	9
52	.734549	3.25	.924246	1.37	.810302	4.63	.189698	8
53	.734744	3.25	.924164	1.35	.810580	4.62	.189420	7
54	.734939	3.27	.924083	1.37	.810857	4.62	.189143	6
55	.735135	3.25	.924001	1.37	.811134	4.60	.188866	5
56	.735330	3.25	.923919	1.37	.811410	4.62	.188590	4
57	.735525	3.23	.923837	1.37	.811687	4.62	.188313	3
58	.735719	3.25	.923755	1.37	.811964	4.62	.188036	2
59	.735914	3.25	.923673	1.37	.812241	4.60	.187759	1
60	9.736109		9.923591		9.812517		10.187483	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.736109	3.23	9.923591	1.37	9.812517	4.62	10.187483	60
1	.736303	3.25	.923509	1.37	.812794	4.60	.187206	59
2	.736498	3.23	.923427	1.37	.813070	4.62	.186930	58
3	.736692	3.23	.923345	1.37	.813347	4.60	.186653	57
4	.736886	3.23	.923263	1.37	.813623	4.60	.186377	56
5	.737080	3.23	.923181	1.38	.813899	4.62	.186101	55
6	.737274	3.22	.923098	1.37	.814176	4.60	.185824	54
7	.737467	3.23	.923016	1.38	.814452	4.60	.185548	53
8	.737661	3.23	.922933	1.37	.814728	4.60	.185272	52
9	.737855	3.22	.922851	1.38	.815004	4.60	.184996	51
10	.738048	3.22	.922768	1.37	.815280	4.58	.184720	50
11	9.738241	3.22	9.922686	1.38	9.815555	4.60	10.184445	49
12	.738434	3.22	.922603	1.38	.815831	4.60	.184169	48
13	.738627	3.22	.922520	1.37	.816107	4.58	.183893	47
14	.738820	3.22	.922438	1.38	.816382	4.60	.183618	46
15	.739013	3.22	.922355	1.38	.816658	4.58	.183342	45
16	.739206	3.20	.922272	1.38	.816933	4.60	.183067	44
17	.739398	3.20	.922189	1.38	.817209	4.58	.182791	43
18	.739590	3.22	.922106	1.38	.817484	4.58	.182516	42
19	.739783	3.20	.922023	1.38	.817759	4.60	.182241	41
20	.739975	3.20	.921940	1.38	.818035	4.58	.181965	40
21	9.740167	3.20	9.921857	1.38	9.818310	4.58	10.181690	39
22	.740359	3.18	.921774	1.38	.818585	4.58	.181415	38
23	.740550	3.20	.921691	1.40	.818860	4.58	.181140	37
24	.740742	3.20	.921607	1.38	.819135	4.58	.180865	36
25	.740934	3.18	.921524	1.38	.819410	4.57	.180590	35
26	.741125	3.18	.921441	1.40	.819684	4.58	.180316	34
27	.741316	3.20	.921357	1.38	.819959	4.58	.180041	33
28	.741508	3.18	.921274	1.40	.820234	4.57	.179766	32
29	.741699	3.17	.921190	1.38	.820508	4.58	.179492	31
30	.741889	3.18	.921107	1.40	.820783	4.57	.179217	30
31	9.742080	3.18	9.921023	1.40	9.821057	4.58	10.178943	29
32	.742271	3.18	.920939	1.38	.821332	4.57	.178668	28
33	.742462	3.17	.920856	1.40	.821606	4.57	.178394	27
34	.742652	3.17	.920772	1.40	.821880	4.57	.178120	26
35	.742842	3.18	.920688	1.40	.822154	4.58	.177846	25
36	.743033	3.17	.920604	1.40	.822429	4.57	.177571	24
37	.743223	3.17	.920520	1.40	.822703	4.57	.177297	23
38	.743413	3.15	.920436	1.40	.822977	4.57	.177023	22
39	.743602	3.17	.920352	1.40	.823251	4.55	.176749	21
40	.743792	3.17	.920268	1.40	.823524	4.57	.176476	20
41	9.743982	3.15	9.920184	1.42	9.823798	4.57	10.176202	19
42	.744171	3.17	.920099	1.40	.824072	4.55	.175928	18
43	.744361	3.15	.920015	1.40	.824345	4.57	.175655	17
44	.744550	3.15	.919931	1.42	.824619	4.57	.175381	16
45	.744739	3.15	.919846	1.40	.824893	4.55	.175107	15
46	.744928	3.15	.919762	1.42	.825166	4.55	.174834	14
47	.745117	3.15	.919677	1.40	.825439	4.57	.174561	13
48	.745306	3.13	.919593	1.42	.825713	4.55	.174287	12
49	.745494	3.15	.919508	1.40	.825986	4.55	.174014	11
50	.745683	3.13	.919424	1.42	.826259	4.55	.173741	10
51	9.745871	3.15	9.919339	1.42	9.826532	4.55	10.173468	9
52	.746060	3.13	.919254	1.42	.826805	4.55	.173195	8
53	.746248	3.13	.919169	1.40	.827078	4.55	.172922	7
54	.746436	3.13	.919085	1.42	.827351	4.55	.172649	6
55	.746624	3.13	.919000	1.42	.827624	4.55	.172376	5
56	.746812	3.12	.918915	1.42	.827897	4.55	.172103	4
57	.746999	3.13	.918830	1.42	.828170	4.53	.171830	3
58	.747187	3.12	.918745	1.43	.828442	4.55	.171558	2
59	.747374	3.13	.918659	1.42	.828715	4.53	.171285	1
60	9.747562		9.918574		9.828987		10.171013	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.747562	3.12	9.918574	1.42	9.828967	4.55	10.171013	60
1	.747749	3.12	.918489	1.42	.829260	4.53	.170740	59
2	.747936	3.12	.918404	1.43	.829532	4.55	.170468	58
3	.748123	3.12	.918318	1.42	.829805	4.53	.170195	57
4	.748310	3.12	.918233	1.43	.830077	4.53	.169923	56
5	.748497	3.10	.918147	1.42	.830349	4.53	.169651	55
6	.748683	3.12	.918062	1.43	.830621	4.53	.169379	54
7	.748870	3.10	.917976	1.42	.830893	4.53	.169107	53
8	.749056	3.12	.917891	1.43	.831165	4.53	.168835	52
9	.749243	3.10	.917805	1.43	.831437	4.53	.168563	51
10	.749429	3.10	.917719	1.42	.831709	4.53	.168291	50
11	9.749615	3.10	9.917634	1.43	9.831981	4.53	10.168019	49
12	.749801	3.10	.917548	1.43	.832253	4.53	.167747	48
13	.749987	3.08	.917462	1.43	.832525	4.52	.167475	47
14	.750172	3.10	.917376	1.43	.832796	4.53	.167204	46
15	.750358	3.08	.917290	1.43	.833068	4.52	.166932	45
16	.750543	3.10	.917204	1.43	.833339	4.53	.166661	44
17	.750729	3.08	.917118	1.43	.833611	4.52	.166389	43
18	.750914	3.08	.917032	1.43	.833882	4.53	.166118	42
19	.751099	3.08	.916946	1.45	.834154	4.52	.165846	41
20	.751284	3.08	.916859	1.43	.834425	4.52	.165575	40
21	9.751469	3.08	9.916773	1.43	9.834696	4.52	10.165304	39
22	.751654	3.08	.916687	1.45	.834967	4.52	.165033	38
23	.751839	3.07	.916600	1.43	.835238	4.52	.164762	37
24	.752023	3.08	.916514	1.45	.835509	4.52	.164491	36
25	.752208	3.07	.916427	1.43	.835780	4.52	.164220	35
26	.752392	3.07	.916341	1.45	.836051	4.52	.163949	34
27	.752576	3.07	.916254	1.45	.836322	4.52	.163678	33
28	.752760	3.07	.916167	1.43	.836593	4.52	.163407	32
29	.752944	3.07	.916081	1.45	.836864	4.50	.163136	31
30	.753128	3.07	.915994	1.45	.837134	4.52	.162866	30
31	9.753312	3.05	9.915907	1.45	9.837405	4.50	10.162595	29
32	.753495	3.07	.915820	1.45	.837675	4.52	.162325	28
33	.753679	3.07	.915733	1.45	.837946	4.50	.162054	27
34	.753862	3.07	.915646	1.45	.838216	4.52	.161784	26
35	.754046	3.05	.915559	1.45	.838487	4.50	.161513	25
36	.754229	3.05	.915472	1.45	.838757	4.50	.161243	24
37	.754412	3.05	.915385	1.47	.839027	4.50	.160973	23
38	.754595	3.05	.915297	1.45	.839297	4.52	.160703	22
39	.754778	3.03	.915210	1.45	.839568	4.50	.160432	21
40	.754960	3.05	.915123	1.47	.839838	4.50	.160162	20
41	9.755143	3.05	9.915035	1.45	9.840108	4.50	10.159892	19
42	.755326	3.03	.914948	1.47	.840378	4.50	.159622	18
43	.755508	3.03	.914860	1.45	.840648	4.48	.159352	17
44	.755690	3.03	.914773	1.47	.840917	4.50	.159083	16
45	.755872	3.03	.914685	1.45	.841187	4.50	.158813	15
46	.756054	3.03	.914598	1.47	.841457	4.50	.158543	14
47	.756236	3.03	.914510	1.47	.841727	4.48	.158273	13
48	.756418	3.03	.914422	1.47	.841996	4.50	.158004	12
49	.756600	3.03	.914334	1.47	.842266	4.48	.157734	11
50	.756782	3.02	.914246	1.47	.842535	4.50	.157465	10
51	9.756963	3.02	9.914158	1.47	9.842805	4.48	10.157195	9
52	.757144	3.03	.914070	1.47	.843074	4.48	156926	8
53	.757326	3.02	.913982	1.47	.843343	4.48	.156657	7
54	.757507	3.02	.913894	1.47	.843612	4.50	.156388	6
55	.757688	3.02	.913806	1.47	.843882	4.48	.156118	5
56	.757869	3.02	.913718	1.47	.844151	4.48	.155849	4
57	.758050	3.00	.913630	1.48	.844420	4.48	.155580	3
58	.758230	3.02	913541	1.47	.844689	4.48	.155311	2
59	.758411	3.00	.913453	1.47	.844958	4.48	.155042	1
60	9.758591		9.913365		9.845227		10.154773	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.758591	3.02	9.913365	1.48	9.845227	4.48	10.154773	60
1	.758772	3.00	.913276	1.48	.845496	4.47	.154504	59
2	.758952	3.00	.913187	1.47	.845764	4.48	.154236	58
3	.759132	3.00	.913099	1.48	.846033	4.48	.153967	57
4	.759312	3.00	.913010	1.47	.846302	4.47	.153698	56
5	.759492	3.00	.912922	1.48	.846570	4.48	.153430	55
6	.759672	3.00	.912833	1.48	.846839	4.48	.153161	54
7	.759852	2.98	.912744	1.48	.847108	4.47	.152892	53
8	.760031	3.00	.912655	1.48	.847376	4.47	.152624	52
9	.760211	2.98	.912566	1.48	.847644	4.48	.152356	51
10	.760390	2.98	.912477	1.48	.847913	4.47	.152087	50
11	9.760569	2.98	9.912388	1.48	9.848181	4.47	10.151819	49
12	.760748	2.98	.912299	1.48	.848449	4.47	.151551	48
13	.760927	2.98	.912210	1.48	.848717	4.48	.151283	47
14	.761106	2.98	.912121	1.50	.848986	4.47	.151014	46
15	.761285	2.98	.912031	1.48	.849254	4.47	.150746	45
16	.761464	2.97	.911942	1.48	.849522	4.47	.150478	44
17	.761642	2.98	.911853	1.50	.849790	4.45	.150210	43
18	.761821	2.97	.911763	1.48	.850057	4.47	.149943	42
19	.761999	2.97	.911674	1.50	.850325	4.47	.149675	41
20	.762177	2.98	.911584	1.48	.850593	4.47	.149407	40
21	9.762356	2.97	9.911495	1.50	9.850861	4.47	10.149139	39
22	.762534	2.97	.911405	1.50	.851129	4.45	.148871	38
23	.762712	2.95	.911315	1.48	.851396	4.47	.148604	37
24	.762889	2.97	.911226	1.50	.851664	4.45	.148336	36
25	.763067	2.97	.911136	1.50	.851931	4.47	.148069	35
26	.763245	2.95	.911046	1.50	.852199	4.45	.147801	34
27	.763422	2.97	.910956	1.50	.852466	4.45	.147534	33
28	.763600	2.95	.910866	1.50	.852733	4.47	.147267	32
29	.763777	2.95	.910776	1.50	.853001	4.45	.146999	31
30	.763954	2.95	.910686	1.50	.853268	4.45	.146732	30
31	9.764131	2.95	9.910596	1.50	9.853535	4.45	10.146465	29
32	.764308	2.95	.910506	1.52	.853802	4.45	.146198	28
33	.764485	2.95	.910415	1.50	.854069	4.45	.145931	27
34	.764662	2.93	.910325	1.50	.854336	4.45	.145664	26
35	.764838	2.95	.910235	1.52	.854603	4.45	.145397	25
36	.765015	2.93	.910144	1.50	.854870	4.45	.145130	24
37	.765191	2.93	.910054	1.52	.855137	4.45	.144863	23
38	.765367	2.95	.909963	1.50	.855404	4.45	.144596	22
39	.765544	2.93	.909873	1.52	.855671	4.45	.144329	21
40	.765720	2.93	.909782	1.52	.855938	4.43	.144062	20
41	9.765896	2.93	9.909691	1.50	9.856204	4.45	10.143796	19
42	.766072	2.92	.909601	1.52	.856471	4.43	.143529	18
43	.766247	2.93	.909510	1.52	.856737	4.45	.143263	17
44	.766423	2.92	.909419	1.52	.857004	4.43	.142996	16
45	.766598	2.93	.909328	1.52	.857270	4.45	.142730	15
46	.766774	2.92	.909237	1.52	.857537	4.43	.142463	14
47	.766949	2.92	.909146	1.52	.857803	4.43	.142197	13
48	.767124	2.93	.909055	1.52	.858069	4.45	.141931	12
49	.767300	2.92	.908964	1.52	.858336	4.43	.141664	11
50	.767475	2.90	.908873	1.53	.858602	4.43	.141398	10
51	9.767649	2.92	9.908781	1.52	9.858868	4.43	10.141132	9
52	.767824	2.92	.908690	1.52	.859134	4.43	.140866	8
53	.767999	2.90	.908599	1.53	.859400	4.43	.140600	7
54	.768173	2.92	.908507	1.52	.859666	4.43	.140334	6
55	.768348	2.90	.908416	1.53	.859932	4.43	.140068	5
56	.768522	2.92	.908324	1.52	.860198	4.43	.139802	4
57	.768697	2.90	.908233	1.53	.860464	4.43	.139536	3
58	.768871	2.90	.908141	1.53	.860730	4.42	.139270	2
59	.769045	2.90	.908049	1.52	.860995	4.43	.139005	1
60	9.769219		9.907958		9.861261		10.138739	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.769219	2.90	9.907958	1.53	9.861261	4.43	10.138739	60
1	.769393	2.88	.907866	1.53	.861527	4.42	.138473	59
2	.769566	2.90	.907774	1.53	.861792	4.43	.138208	58
3	.769740	2.88	.907682	1.53	.862058	4.42	.137942	57
4	.769913	2.90	.907590	1.53	.862323	4.43	.137677	56
5	.770087	2.88	.907498	1.53	.862589	4.42	.137411	55
6	.770260	2.88	.907406	1.53	.862854	4.42	.137146	54
7	.770433	2.88	.907314	1.53	.863119	4.43	.136881	53
8	.770606	2.88	.907222	1.55	.863385	4.42	.136615	52
9	.770779	2.88	.907129	1.53	.863650	4.42	.136350	51
10	.770952	2.88	.907037	1.53	.863915	4.42	.136085	50
11	9.771125	2.88	9.906945	1.55	9.864180	4.42	10.135820	49
12	.771298	2.87	.906852	1.53	.864445	4.42	.135555	48
13	.771470	2.88	.906760	1.55	.864710	4.42	.135290	47
14	.771643	2.87	.906667	1.53	.864975	4.42	.135025	46
15	.771815	2.87	.906575	1.55	.865240	4.42	.134760	45
16	.771987	2.87	.906482	1.55	.865505	4.42	.134495	44
17	.772159	2.87	.906389	1.55	.865770	4.42	.134230	43
18	.772331	2.87	.906296	1.53	.866035	4.42	.133965	42
19	.772503	2.87	.906204	1.55	.866300	4.40	.133700	41
20	.772675	2.87	.906111	1.55	.866564	4.42	.133436	40
21	9.772847	2.85	9.906018	1.55	9.866829	4.42	10.133171	39
22	.773018	2.87	.905925	1.55	.867094	4.40	.132906	38
23	.773190	2.85	.905832	1.55	.867358	4.42	.132642	37
24	.773361	2.87	.905739	1.57	.867623	4.40	.132377	36
25	.773533	2.85	.905645	1.55	.867887	4.42	.132113	35
26	.773704	2.85	.905552	1.55	.868152	4.40	.131848	34
27	.773875	2.85	.905459	1.55	.868416	4.40	.131584	33
28	.774046	2.85	.905366	1.57	.868680	4.42	.131320	32
29	.774217	2.85	.905272	1.55	.868945	4.40	.131055	31
30	.774388	2.83	.905179	1.57	.869209	4.40	.130791	30
31	9.774558	2.85	9.905085	1.55	9.869473	4.40	10.130527	29
32	.774729	2.83	.904992	1.57	.869737	4.40	.130263	28
33	.774899	2.85	.904898	1.57	.870001	4.40	.129999	27
34	.775070	2.83	.904804	1.55	.870265	4.40	.129735	26
35	.775240	2.83	.904711	1.57	.870529	4.40	.129471	25
36	.775410	2.83	.904617	1.57	.870793	4.40	.129207	24
37	.775580	2.83	.904523	1.57	.871057	4.40	.128943	23
38	.775750	2.83	.904429	1.57	.871321	4.40	.128679	22
39	.775920	2.83	.904335	1.57	.871585	4.40	.128415	21
40	.776090	2.82	.904241	1.57	.871849	4.38	.128151	20
41	9.776259	2.83	9.904147	1.57	9.872112	4.40	10.127888	19
42	.776429	2.82	.904053	1.57	.872376	4.40	.127624	18
43	.776598	2.83	.903959	1.58	.872640	4.38	.127360	17
44	.776768	2.82	.903864	1.57	.872903	4.40	.127097	16
45	.776937	2.82	.903770	1.57	.873167	4.38	.126833	15
46	.777106	2.82	.903676	1.58	.873430	4.40	.126570	14
47	.777275	2.82	.903581	1.57	.873694	4.38	.126306	13
48	.777444	2.82	.903487	1.58	.873957	4.38	.126043	12
49	.777613	2.80	.903392	1.57	.874220	4.40	.125780	11
50	.777781	2.82	.903298	1.58	.874484	4.38	.125516	10
51	9.777950	2.82	9.903203	1.58	9.874747	4.38	10.125253	9
52	.778119	2.80	.903108	1.57	.875010	4.38	.124990	8
53	.778287	2.80	.903014	1.58	.875273	4.40	.124727	7
54	.778455	2.82	.902919	1.58	.875537	4.38	.124463	6
55	.778624	2.80	.902824	1.58	.875800	4.38	.124200	5
56	.778792	2.80	.902729	1.58	.876063	4.38	.123937	4
57	.778960	2.80	.902634	1.58	.876326	4.38	.123674	3
58	.779128	2.78	.902539	1.58	.876589	4.38	.123411	2
59	.779295	2.80	.902444	1.58	.876852	4.37	.123148	1
60	9.779463		9.902349		9.877114		10.122886	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

126° 53°

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.779463	2.80	9.902349	1.60	9.877114	4.38	10.122886	60
1	.779631	2.78	.902253	1.58	.877377	4.38	.122623	59
2	.779798	2.80	.902158	1.58	.877640	4.38	.122360	58
3	.779966	2.78	.902063	1.60	.877903	4.37	.122097	57
4	.780133	2.78	.901967	1.58	.878165	4.38	.121835	56
5	.780300	2.78	.901872	1.60	.878428	4.38	.121572	55
6	.780467	2.78	.901776	1.58	.878691	4.37	.121309	54
7	.780634	2.78	.901681	1.60	.878953	4.38	.121047	53
8	.780801	2.78	.901585	1.58	.879216	4.37	.120784	52
9	.780968	2.77	.901490	1.60	.879478	4.38	.120522	51
10	.781134	2.78	.901394	1.60	.879741	4.37	.120259	50
11	9.781301	2.78	9.901298	1.60	9.880003	4.37	10.119997	49
12	.781468	2.77	.901202	1.60	.880265	4.38	.119735	48
13	.781634	2.77	.901106	1.60	.880528	4.37	.119472	47
14	.781800	2.77	.901010	1.60	.880790	4.37	.119210	46
15	.781966	2.77	.900914	1.60	.881052	4.37	.118948	45
16	.782132	2.77	.900818	1.60	.881314	4.38	.118686	44
17	.782298	2.77	.900722	1.60	.881577	4.37	.118423	43
18	.782464	2.77	.900626	1.62	.881839	4.37	.118161	42
19	.782630	2.77	.900529	1.60	.882101	4.37	.117899	41
20	.782796	2.75	.900433	1.60	.882363	4.37	.117637	40
21	9.782961	2.77	9.900337	1.62	9.882625	4.37	10.117375	39
22	.783127	2.75	.900240	1.60	.882887	4.35	.117113	38
23	.783292	2.77	.900144	1.62	.883148	4.37	.116852	37
24	.783458	2.75	.900047	1.60	.883410	4.37	.116590	36
25	.783623	2.75	.899951	1.62	.883672	4.37	.116328	35
26	.783788	2.75	.899854	1.62	.883934	4.37	.116066	34
27	.783953	2.75	.899757	1.62	.884196	4.35	.115804	33
28	.784118	2.73	.899660	1.60	.884457	4.37	.115543	32
29	.784282	2.75	.899564	1.62	.884719	4.35	.115281	31
30	.784447	2.75	.899467	1.62	.884980	4.37	.115020	30
31	9.784612	2.73	9.899370	1.62	9.885242	4.37	10.114758	29
32	.784776	2.75	.899273	1.62	.885504	4.35	.114496	28
33	.784941	2.73	.899176	1.63	.885765	4.35	.114235	27
34	.785105	2.73	.899078	1.62	.886026	4.37	.113974	26
35	.785269	2.73	.898981	1.62	.886288	4.35	.113712	25
36	.785433	2.73	.898884	1.62	.886549	4.37	.113451	24
37	.785597	2.73	.898787	1.63	.886811	4.35	.113189	23
38	.785761	2.73	.898689	1.62	.887072	4.35	.112928	22
39	.785925	2.73	.898592	1.63	.887333	4.35	.112667	21
40	.786089	2.72	.898494	1.62	.887594	4.35	.112406	20
41	9.786252	2.73	9.898397	1.63	9.887855	4.35	10.112145	19
42	.786416	2.72	.898299	1.62	.888116	4.37	.111884	18
43	.786579	2.72	.898202	1.63	.888378	4.35	.111622	17
44	.786742	2.73	.898104	1.63	.888639	4.35	.111361	16
45	.786906	2.72	.898006	1.63	.888900	4.35	.111100	15
46	.787069	2.72	.897908	1.63	.889161	4.33	.110839	14
47	.787232	2.72	.897810	1.63	.889421	4.35	.110579	13
48	.787395	2.70	.897712	1.63	.889682	4.35	.110318	12
49	.787557	2.72	.897614	1.63	.889943	4.35	.110057	11
50	.787720	2.72	.897516	1.63	.890204	4.35	.109796	10
51	9.787883	2.70	9.897418	1.63	9.890465	4.33	10.109535	9
52	.788045	2.72	.897320	1.63	.890725	4.35	.109275	8
53	.788208	2.70	.897222	1.65	.890986	4.35	.109014	7
54	.788370	2.70	.897123	1.63	.891247	4.33	.108753	6
55	.788532	2.70	.897025	1.65	.891507	4.35	.108493	5
56	.788694	2.70	.896926	1.63	.891768	4.33	.108232	4
57	.788856	2.70	.896828	1.65	.892028	4.35	.107972	3
58	.789018	2.70	.896729	1.63	.892289	4.33	.107711	2
59	.789180	2.70	.896631	1.65	.892549	4.35	.107451	1
60	9.789342		9.896532		9.892810		10.107190	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.789342	2.70	9.896532	1.65	9.892810	4.33	10.107190	60
1	.789504	2.68	.896433	1.63	.893070	4.35	.106930	59
2	.789665	2.70	.896335	1.65	.893331	4.33	.106669	58
3	.789827	2.68	.896236	1.65	.893591	4.33	.106409	57
4	.789988	2.68	.896137	1.65	.893851	4.33	.106149	56
5	.790149	2.68	.896038	1.65	.894111	4.35	.105889	55
6	.790310	2.68	.895939	1.65	.894372	4.33	.105628	54
7	.790471	2.68	.895840	1.65	.894632	4.33	.105368	53
8	.790632	2.68	.895741	1.67	.894892	4.33	.105108	52
9	.790793	2.68	.895641	1.65	.895152	4.33	.104848	51
10	.790954	2.68	.895542	1.65	.895412	4.33	.104588	50
11	9.791115	2.67	9.895443	1.67	9.895672	4.33	10.104328	49
12	.791275	2.68	.895343	1.65	.895932	4.33	.104068	48
13	.791436	2.67	.895244	1.65	.896192	4.33	.103808	47
14	.791596	2.68	.895145	1.67	.896452	4.33	.103548	46
15	.791757	2.67	.895045	1.67	.896712	4.32	.103288	45
16	.791917	2.67	.894945	1.65	.896971	4.33	.103029	44
17	.792077	2.67	.894846	1.67	.897231	4.33	.102769	43
18	.792237	2.67	.894746	1.67	.897491	4.33	.102509	42
19	.792397	2.67	.894646	1.67	.897751	4.32	.102249	41
20	.792557	2.65	.894546	1.67	.898010	4.33	.101990	40
21	9.792716	2.67	9.894446	1.67	9.898270	4.33	10.101730	39
22	.792876	2.65	.894346	1.67	.898530	4.32	.101470	38
23	.793035	2.67	.894246	1.67	.898789	4.33	.101211	37
24	.793195	2.65	.894146	1.67	.899049	4.32	.100951	36
25	.793354	2.67	.894046	1.67	.899308	4.33	.100692	35
26	.793514	2.65	.893946	1.67	.899568	4.32	.100432	34
27	.793673	2.65	.893846	1.68	.899827	4.33	.100173	33
28	.793832	2.65	.893745	1.67	.900087	4.32	.099913	32
29	.793991	2.65	.893645	1.68	.900346	4.32	.099654	31
30	.794150	2.63	.893544	1.67	.900605	4.32	.099395	30
31	9.794308	2.65	9.893444	1.68	9.900864	4.33	10.099136	29
32	.794467	2.65	.893343	1.67	.901124	4.32	.098876	28
33	.794626	2.63	.893243	1.68	.901383	4.32	.098617	27
34	.794784	2.63	.893142	1.68	.901642	4.32	.098358	26
35	.794942	2.65	.893041	1.68	.901901	4.32	.098099	25
36	.795101	2.63	.892940	1.68	.902160	4.33	.097840	24
37	.795259	2.63	.892839	1.67	.902420	4.32	.097580	23
38	.795417	2.63	.892739	1.68	.902679	4.32	.097321	22
39	.795575	2.63	.892638	1.70	.902938	4.32	.097062	21
40	.795733	2.63	.892536	1.68	.903197	4.32	.096803	20
41	9.795891	2.63	9.892435	1.68	9.903456	4.30	10.096544	19
42	.796049	2.62	.892334	1.68	.903714	4.32	.096286	18
43	.796206	2.63	.892233	1.68	.903973	4.32	.096027	17
44	.796364	2.62	.892132	1.70	.904232	4.32	.095768	16
45	.796521	2.63	.892030	1.68	.904491	4.32	.095509	15
46	.796679	2.62	.891929	1.70	.904750	4.30	.095250	14
47	.796836	2.62	.891827	1.68	.905008	4.32	.094992	13
48	.796993	2.62	.891726	1.70	.905267	4.32	.094733	12
49	.797150	2.62	.891624	1.68	.905526	4.32	.094474	11
50	.797307	2.62	.891523	1.70	.905785	4.30	.094215	10
51	9.797464	2.62	9.891421	1.70	9.906043	4.32	10.093957	9
52	.797621	2.60	.891319	1.70	.906302	4.30	.093698	8
53	.797777	2.62	.891217	1.70	.906560	4.32	.093440	7
54	.797934	2.62	.891115	1.70	.906819	4.30	.093181	6
55	.798091	2.60	.891013	1.70	.907077	4.32	.092923	5
56	.798247	2.60	.890911	1.70	.907336	4.30	.092664	4
57	.798403	2.62	.890809	1.70	.907594	4.32	.092406	3
58	.798560	2.60	.890707	1.70	.907853	4.30	.092147	2
59	.798716	2.60	.890605	1.70	.908111	4.30	.091889	1
60	9.798872		9.890503		9.908369		10.091631	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.
0	9.798872	2.60	9.890503	1.72	9.908369	4.32	10.091631
1	.799028	2.60	.890400	1.70	.908628	4.30	.091372
2	.799184	2.58	.890298	1.72	.908886	4.30	.091114
3	.799339	2.60	.890195	1.70	.909144	4.30	.090856
4	.799495	2.60	.890093	1.72	.909402	4.30	.090598
5	.799651	2.58	.889990	1.70	.909660	4.30	.090340
6	.799806	2.60	.889888	1.72	.909918	4.32	.090082
7	.799962	2.58	.889785	1.72	.910177	4.30	.089823
8	.800117	2.58	.889682	1.72	.910435	4.30	.089565
9	.800272	2.58	.889579	1.70	.910693	4.30	.089307
10	.800427	2.58	.889477	1.72	.910951	4.30	.089049
11	9.800582	2.58	9.889374	1.72	9.911209	4.30	10.088791
12	.800737	2.58	.889271	1.72	.911467	4.30	.088533
13	.800892	2.58	.889168	1.73	.911725	4.28	.088275
14	.801047	2.57	.889064	1.72	.911982	4.30	.088018
15	.801201	2.58	.888961	1.72	.912240	4.30	.087760
16	.801356	2.58	.888858	1.72	.912498	4.30	.087502
17	.801511	2.57	.888755	1.73	.912756	4.30	.087244
18	.801665	2.57	.888651	1.72	.913014	4.28	.086986
19	.801819	2.57	.888548	1.73	.913271	4.30	.086729
20	.801973	2.58	.888444	1.72	.913529	4.30	.086471
21	9.802128	2.57	9.888341	1.73	9.913787	4.28	10.086213
22	.802282	2.57	.888237	1.72	.914044	4.30	.085956
23	.802436	2.55	.888134	1.73	.914302	4.30	.085698
24	.802589	2.57	.888030	1.73	.914560	4.28	.085440
25	.802743	2.57	.887926	1.73	.914817	4.30	.085183
26	.802897	2.55	.887822	1.73	.915075	4.28	.084925
27	.803050	2.57	.887718	1.73	.915332	4.30	.084668
28	.803204	2.55	.887614	1.73	.915590	4.28	.084410
29	.803357	2.57	.887510	1.73	.915847	4.28	.084153
30	.803511	2.55	.887406	1.73	.916104	4.30	.083896
31	9.803664	2.55	9.887302	1.73	9.916362	4.28	10.083638
32	.803817	2.55	.887198	1.75	.916619	4.30	.083381
33	.803970	2.55	.887093	1.73	.916877	4.28	.083123
34	.804123	2.55	.886989	1.73	.917134	4.28	.082866
35	.804276	2.55	.886885	1.75	.917391	4.28	.082609
36	.804428	2.55	.886780	1.73	.917648	4.30	.082352
37	.804581	2.55	.886676	1.75	.917906	4.28	.082094
38	.804734	2.53	.886571	1.75	.918163	4.28	.081837
39	.804886	2.55	.886466	1.73	.918420	4.28	.081580
40	.805039	2.53	.886362	1.75	.918677	4.28	.081323
41	9.805191	2.53	9.886257	1.75	9.918934	4.28	10.081066
42	.805343	2.53	.886152	1.75	.919191	4.28	.080809
43	.805495	2.53	.886047	1.75	.919448	4.28	.080552
44	.805647	2.53	.885942	1.75	.919705	4.28	.080295
45	.805799	2.53	.885837	1.75	.919962	4.28	.080038
46	.805951	2.53	.885732	1.75	.920219	4.28	.079781
47	.806103	2.52	.885627	1.75	.920476	4.28	.079524
48	.806254	2.53	.885522	1.77	.920733	4.28	.079267
49	.806406	2.52	.885416	1.75	.920990	4.28	.079010
50	.806557	2.53	.885311	1.77	.921247	4.27	.078753
51	9.806709	2.52	9.885205	1.75	9.921503	4.28	10.078497
52	.806860	2.52	.885100	1.77	.921760	4.28	.078240
53	.807011	2.53	.884994	1.75	.922017	4.28	.077983
54	.807163	2.52	.884889	1.77	.922274	4.27	.077726
55	.807314	2.52	.884783	1.77	.922530	4.28	.077470
56	.807465	2.50	.884677	1.75	.922787	4.28	.077213
57	.807615	2.52	.884572	1.77	.923044	4.27	.076956
58	.807766	2.52	.884466	1.77	.923300	4.28	.076700
59	.807917	2.50	.884360	1.77	.923557	4.28	.076443
60	9.808067		9.884254		9.923814		10.076186
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.808067	2.52	9.884254	1.77	9.923814	4.27	10.076186	60
1	.808218	2.50	.884148	1.77	.924070	4.28	.075930	59
2	.808368	2.52	.884042	1.77	.924327	4.27	.075673	58
3	.808519	2.50	.883936	1.78	.924583	4.28	.075417	57
4	.808669	2.50	.883829	1.77	.924840	4.27	.075160	56
5	.808819	2.50	.883723	1.77	.925096	4.27	.074904	55
6	.808969	2.50	.883617	1.78	.925352	4.28	.074648	54
7	.809119	2.50	.883510	1.77	.925609	4.27	.074391	53
8	.809269	2.50	.883404	1.78	.925865	4.28	.074135	52
9	.809419	2.50	.883297	1.77	.926122	4.27	.073878	51
10	.809569	2.48	.883191	1.78	.926378	4.27	.073622	50
11	9.809718	2.50	9.883084	1.78	9.926634	4.27	10.073366	49
12	.809868	2.48	.882977	1.77	.926890	4.28	.073110	48
13	.810017	2.50	.882871	1.78	.927147	4.27	.072853	47
14	.810167	2.48	.882764	1.78	.927403	4.27	.072597	46
15	.810316	2.48	.882657	1.78	.927659	4.27	.072341	45
16	.810465	2.48	.882550	1.78	.927915	4.27	.072085	44
17	.810614	2.48	.882443	1.78	.928171	4.27	.071829	43
18	.810763	2.48	.882336	1.78	.928427	4.28	.071573	42
19	.810912	2.48	.882229	1.80	.928684	4.27	.071316	41
20	.811061	2.48	.882121	1.78	.928940	4.27	.071060	40
21	9.811210	2.47	9.882014	1.78	9.929196	4.27	10.070804	39
22	.811358	2.48	.881907	1.80	.929452	4.27	.070548	38
23	.811507	2.47	.881799	1.78	.929708	4.27	.070292	37
24	.811655	2.48	.881692	1.80	.929964	4.27	.070036	36
25	.811804	2.47	.881584	1.78	.930220	4.25	.069780	35
26	.811952	2.47	.881477	1.80	.930475	4.27	.069525	34
27	.812100	2.47	.881369	1.80	.930731	4.27	.069269	33
28	.812248	2.47	.881261	1.80	.930987	4.27	.069013	32
29	.812396	2.47	.881153	1.78	.931243	4.27	.068757	31
30	.812544	2.47	.881046	1.80	.931499	4.27	.068501	30
31	9.812692	2.47	9.880938	1.80	9.931755	4.25	10.068245	29
32	.812840	2.47	.880830	1.80	.932010	4.27	.067990	28
33	.812988	2.45	.880722	1.82	.932266	4.27	.067734	27
34	.813135	2.47	.880613	1.80	.932522	4.27	.067478	26
35	.813283	2.45	.880505	1.80	.932778	4.25	.067222	25
36	.813430	2.47	.880397	1.80	.933033	4.27	.066967	24
37	.813578	2.45	.880289	1.82	.933289	4.27	.066711	23
38	.813725	2.45	.880180	1.80	.933545	4.25	.066455	22
39	.813872	2.45	.880072	1.82	.933800	4.27	.066200	21
40	.814019	2.45	.879963	1.80	.934056	4.25	.065944	20
41	9.814166	2.45	9.879855	1.82	9.934311	4.27	10.065689	19
42	.814313	2.45	.879746	1.82	.934567	4.25	.065433	18
43	.814460	2.45	.879637	1.80	.934822	4.27	.065178	17
44	.814607	2.43	.879529	1.82	.935078	4.25	.064922	16
45	.814753	2.45	.879420	1.82	.935333	4.27	.064667	15
46	.814900	2.43	.879311	1.82	.935589	4.25	.064411	14
47	.815046	2.45	.879202	1.82	.935844	4.27	.064156	13
48	.815193	2.43	.879093	1.82	.936100	4.25	.063900	12
49	.815339	2.43	.878984	1.82	.936355	4.27	.063645	11
50	.815485	2.45	.878875	1.82	.936611	4.25	.063389	10
51	9.815632	2.43	9.878766	1.83	9.936866	4.25	10.063134	9
52	.815778	2.43	.878656	1.82	.937121	4.27	.062879	8
53	.815924	2.42	.878547	1.82	.937377	4.25	.062623	7
54	.816069	2.43	.878438	1.83	.937632	4.25	.062368	6
55	.816215	2.43	.878328	1.82	.937887	4.25	.062113	5
56	.816361	2.43	.878219	1.83	.938142	4.27	.061858	4
57	.816507	2.42	.878109	1.83	.938398	4.25	.061602	3
58	.816652	2.43	.877999	1.82	.938653	4.25	.061347	2
59	.816798	2.42	.877890	1.83	.938908	4.25	.061092	1
60	9.816943		9.877780		9.939163		10.060837	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.
0	9.816943	2.42	9.877780	1.83	9.939163	4.25	10.060837
1	.817088	2.42	.877670	1.83	.939418	4.25	.060582
2	.817233	2.43	.877560	1.83	.939673	4.25	.060327
3	.817379	2.42	.877450	1.83	.939928	4.25	.060072
4	.817524	2.40	.877340	1.83	.940183	4.27	.059817
5	.817668	2.42	.877230	1.83	.940439	4.25	.059561
6	.817813	2.42	.877120	1.83	.940694	4.25	.059306
7	.817958	2.42	.877010	1.85	.940949	4.25	.059051
8	.818103	2.40	.876899	1.83	.941204	4.25	.058796
9	.818247	2.42	.876789	1.85	.941459	4.23	.058541
10	.818392	2.40	.876678	1.83	.941713	4.25	.058287
11	9.818536	2.42	9.876568	1.85	9.941968	4.25	10.058032
12	.818681	2.40	.876457	1.83	.942223	4.25	.057777
13	.818825	2.40	.876347	1.85	.942478	4.25	.057522
14	.818969	2.40	.876236	1.85	.942733	4.25	.057267
15	.819113	2.40	.876125	1.85	.942988	4.25	.057012
16	.819257	2.40	.876014	1.83	.943243	4.25	.056757
17	.819401	2.40	.875904	1.85	.943498	4.23	.056502
18	.819545	2.40	.875793	1.85	.943752	4.25	.056248
19	.819689	2.38	.875682	1.85	.944007	4.25	.055993
20	.819832	2.40	.875571	1.87	.944262	4.25	.055738
21	9.819976	2.40	9.875459	1.85	9.944517	4.23	10.055483
22	.820120	2.38	.875348	1.85	.944771	4.25	.055229
23	.820263	2.38	.875237	1.85	.945026	4.25	.054974
24	.820406	2.40	.875126	1.87	.945281	4.23	.054719
25	.820550	2.38	.875014	1.85	.945535	4.25	.054465
26	.820693	2.38	.874903	1.87	.945790	4.25	.054210
27	.820836	2.38	.874791	1.85	.946045	4.23	.053955
28	.820979	2.38	.874680	1.87	.946299	4.25	.053701
29	.821122	2.38	.874568	1.87	.946554	4.23	.053446
30	.821265	2.37	.874456	1.87	.946808	4.25	.053192
31	9.821407	2.38	9.874344	1.87	9.947063	4.25	10.052937
32	.821550	2.38	.874232	1.85	.947318	4.23	.052682
33	.821693	2.37	.874121	1.87	.947572	4.25	.052428
34	.821835	2.37	.874009	1.88	.947827	4.23	.052173
35	.821977	2.38	.873896	1.87	.948081	4.23	.051919
36	.822120	2.37	.873784	1.87	.948335	4.25	.051665
37	.822262	2.37	.873672	1.87	.948590	4.23	.051410
38	822404	2.37	.873560	1.87	.948844	4.25	.051156
39	.822546	2.37	.873448	1.88	.949099	4.23	.050901
40	.822688	2.37	.873335	1.87	.949353	4.25	.050647
41	9.822830	2.37	9.873223	1.88	9.949608	4.23	10.050392
42	.822972	2.37	.873110	1.87	.949862	4.23	.050138
43	.823114	2.35	.872998	1.88	.950116	4.25	.049884
44	.823255	2.37	.872885	1.88	.950371	4.23	.049629
45	.823397	2.37	.872772	1.88	.950625	4.23	.049375
46	.823539	2.35	.872659	1.87	.950879	4.23	.049121
47	.823680	2.35	.872547	1.88	.951133	4.25	.048867
48	.823821	2.37	.872434	1.88	.951388	4.23	.048612
49	.823963	2.35	.872321	1.88	.951642	4.23	.048358
50	.824104	2.35	.872208	1.88	.951896	4.23	.048104
51	9.824245	2.35	9.872095	1.90	9.952150	4.25	10.047850
52	.824386	2.35	.871981	1.88	.952405	4.23	.047595
53	.824527	2.35	.871868	1.88	.952659	4.23	.047341
54	.824668	2.33	.871755	1.90	.952913	4.23	.047087
55	.824808	2.35	.871641	1.88	.953167	4.23	.046833
56	.824949	2.35	.871528	1.90	.953421	4.23	.046579
57	.825090	2.33	.871414	1.88	.953675	4.23	.046325
58	.825230	2.35	.871301	1.90	.953929	4.23	.046071
59	.825371	2.33	.871187	1.90	.954183	4.23	.045817
60	9.825511		9.871073		9.954437		10.045563
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.825511	2.33	9.871073	1.88	9.954437	4.23	10.045563	60
1	.825651	2.33	.870960	1.90	.954691	4.25	.045309	59
2	.825791	2.33	.870846	1.90	.954946	4.23	.045054	58
3	.825931	2.33	.870732	1.90	.955200	4.23	.044800	57
4	.826071	2.33	.870618	1.90	.955454	4.23	.044546	56
5	.826211	2.33	.870504	1.90	.955708	4.22	.044292	55
6	.826351	2.33	.870390	1.90	.955961	4.23	.044039	54
7	.826491	2.33	.870276	1.92	.956215	4.23	.043785	53
8	.826631	2.32	.870161	1.90	.956469	4.23	.043531	52
9	.826770	2.33	.870047	1.90	.956723	4.23	.043277	51
10	.826910	2.32	.869933	1.92	.956977	4.23	.043023	50
11	9.827049	2.33	9.869818	1.90	9.957231	4.23	10.042769	49
12	.827189	2.32	.869704	1.92	.957485	4.23	.042515	48
13	.827328	2.32	.869589	1.92	.957739	4.23	.042261	47
14	.827467	2.32	.869474	1.90	.957993	4.23	.042007	46
15	.827606	2.32	.869360	1.92	.958247	4.22	.041753	45
16	.827745	2.32	.869245	1.92	.958500	4.23	.041500	44
17	.827884	2.32	.869130	1.92	.958754	4.23	.041246	43
18	.828023	2.32	.869015	1.92	.959008	4.23	.040992	42
19	.828162	2.32	.868900	1.92	.959262	4.23	.040738	41
20	.828301	2.30	.868785	1.92	.959516	4.22	.040484	40
21	9.828439	2.32	9.868670	1.92	9.959769	4.23	10.040231	39
22	.828578	2.30	.868555	1.92	.960023	4.23	.039977	38
23	.828716	2.32	.868440	1.93	.960277	4.22	.039723	37
24	.828855	2.30	.868324	1.92	.960530	4.23	.039470	36
25	.828993	2.30	.868209	1.93	.960784	4.23	.039216	35
26	.829131	2.30	.868093	1.92	.961038	4.23	.038962	34
27	.829269	2.30	.867978	1.93	.961292	4.22	.038708	33
28	.829407	2.30	.867862	1.92	.961545	4.23	.038455	32
29	.829545	2.30	.867747	1.93	.961799	4.22	.038201	31
30	.829683	2.30	.867631	1.93	.962052	4.23	.037948	30
31	9.829821	2.30	9.867515	1.93	9.962306	4.23	10.037694	29
32	.829959	2.30	.867399	1.93	.962560	4.22	.037440	28
33	.830097	2.28	.867283	1.93	.962813	4.23	.037187	27
34	.830234	2.30	.867167	1.93	.963067	4.22	.036933	26
35	.830372	2.28	.867051	1.93	.963320	4.23	.036680	25
36	.830509	2.28	.866935	1.93	.963574	4.23	.036426	24
37	.830646	2.30	.866819	1.93	.963828	4.22	.036172	23
38	.830784	2.28	.866703	1.95	.964081	4.23	.035919	22
39	.830921	2.28	.866586	1.93	.964335	4.22	.035665	21
40	.831058	2.28	.866470	1.95	.964588	4.23	.035412	20
41	9.831195	2.28	9.866353	1.93	9.964842	4.22	10.035158	19
42	.831332	2.28	.866237	1.95	.965095	4.23	.034905	18
43	.831469	2.28	.866120	1.93	.965349	4.22	.034651	17
44	.831606	2.27	.866004	1.95	.965602	4.22	.034398	16
45	.831742	2.28	.865887	1.95	.965855	4.23	.034145	15
46	.831879	2.27	.865770	1.95	.966109	4.22	.033891	14
47	.832015	2.28	.865653	1.95	.966362	4.23	.033638	13
48	.832152	2.27	.865536	1.95	.966616	4.22	.033384	12
49	.832288	2.28	.865419	1.95	.966869	4.23	.033131	11
50	.832425	2.27	.865302	1.95	.967123	4.22	.032877	10
51	9.832561	2.27	9.865185	1.95	9.967376	4.22	10.032624	9
52	.832697	2.27	.865068	1.97	.967629	4.23	.032371	8
53	.832833	2.27	.864950	1.95	.967883	4.22	.032117	7
54	.832969	2.27	.864833	1.95	.968136	4.22	.031864	6
55	.833105	2.27	.864716	1.97	.968389	4.23	.031611	5
56	.833241	2.27	.864598	1.95	.968643	4.22	.031357	4
57	.833377	2.25	.864481	1.97	.968896	4.22	.031104	3
58	.833512	2.27	.864363	1.97	.969149	4.23	.030851	2
59	.833648	2.25	.864245	1.97	.969403	4.22	.030597	1
60	9.833783		9.864127		9.969656		10.030344	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.833783	2.27	9.864127	1.95	9.969656	4.22	10.030344	60
1	.833919	2.25	.864010	1.97	.969909	4.22	.030091	59
2	.834054	2.25	.863892	1.97	.970162	4.23	.029838	58
3	.834189	2.27	.863774	1.97	.970416	4.22	.029584	57
4	.834325	2.25	.863656	1.97	.970669	4.22	.029331	56
5	.834460	2.25	.863538	1.98	.970922	4.22	.029078	55
6	.834595	2.25	.863419	1.97	.971175	4.23	.028825	54
7	.834730	2.25	.863301	1.97	.971429	4.22	.028571	53
8	.834865	2.23	.863183	1.98	.971682	4.22	.028318	52
9	.834999	2.25	.863064	1.97	.971935	4.22	.028065	51
10	.835134	2.25	.862946	1.98	.972188	4.22	.027812	50
11	9.835269	2.23	9.862827	1.97	9.972441	4.23	10.027559	49
12	.835403	2.25	.862709	1.98	.972695	4.22	.027305	48
13	.835538	2.23	.862590	1.98	.972948	4.22	.027052	47
14	.835672	2.25	.862471	1.97	.973201	4.22	.026799	46
15	.835807	2.23	.862353	1.98	.973454	4.22	.026546	45
16	.835941	2.23	.862234	1.98	.973707	4.22	.026293	44
17	.836075	2.23	.862115	1.98	.973960	4.22	.026040	43
18	.836209	2.23	.861996	1.98	.974213	4.22	.025787	42
19	.836343	2.23	.861877	1.98	.974466	4.23	.025534	41
20	.836477	2.23	.861758	2.00	.974720	4.22	.025280	40
21	9.836611	2.23	9.861638	1.98	9.974973	4.22	10.025027	39
22	.836745	2.22	.861519	1.98	.975226	4.22	.024774	38
23	.836878	2.23	.861400	2.00	.975479	4.22	.024521	37
24	.837012	2.23	.861280	1.98	.975732	4.22	.024268	36
25	.837146	2.22	.861161	2.00	.975985	4.22	.024015	35
26	.837279	2.22	.861041	1.98	.976238	4.22	.023762	34
27	.837412	2.23	.860922	2.00	.976491	4.22	.023509	33
28	.837546	2.22	.860802	2.00	.976744	4.22	.023256	32
29	.837679	2.22	.860682	2.00	.976997	4.22	.023003	31
30	.837812	2.22	.860562	2.00	.977250	4.22	.022750	30
31	9.837945	2.22	9.860442	2.00	9.977503	4.22	10.022497	29
32	.838078	2.22	.860322	2.00	.977756	4.22	.022244	28
33	.838211	2.22	.860202	2.00	.978009	4.22	.021991	27
34	.838344	2.22	.860082	2.00	.978262	4.22	.021738	26
35	.838477	2.22	.859962	2.00	.978515	4.22	.021485	25
36	.838610	2.20	.859842	2.02	.978768	4.22	.021232	24
37	.838742	2.22	.859721	2.00	.979021	4.22	.020979	23
38	.838875	2.20	.859601	2.02	.979274	4.22	.020726	22
39	.839007	2.22	.859480	2.00	.979527	4.22	.020473	21
40	.839140	2.20	.859360	2.02	.979780	4.22	.020220	20
41	9.839272	2.20	9.859239	2.00	9.980033	4.22	10.019967	19
42	.839404	2.20	.859119	2.02	.980286	4.20	.019714	18
43	.839536	2.20	.858998	2.02	.980538	4.22	.019462	17
44	.839668	2.20	.858877	2.02	.980791	4.22	.019209	16
45	.839800	2.20	.858756	2.02	.981044	4.22	.018956	15
46	.839932	2.20	.858635	2.02	.981297	4.22	.018703	14
47	.840064	2.20	.858514	2.02	.981550	4.22	.018450	13
48	.840196	2.20	.858393	2.02	.981803	4.22	.018197	12
49	.840328	2.18	.858272	2.02	.982056	4.22	.017944	11
50	.840459	2.20	.858151	2.03	.982309	4.22	.017691	10
51	9.840591	2.18	9.858029	2.02	9.982562	4.20	10.017438	9
52	.840722	2.20	.857908	2.03	.982814	4.22	.017186	8
53	.840854	2.18	.857786	2.02	.983067	4.22	.016933	7
54	.840985	2.18	.857665	2.03	.983320	4.22	.016680	6
55	.841116	2.18	.857543	2.02	.983573	4.22	.016427	5
56	.841247	2.18	.857422	2.03	.983826	4.22	.016174	4
57	.841378	2.18	.857300	2.03	.984079	4.22	.015921	3
58	.841509	2.18	.857178	2.03	.984332	4.20	.015668	2
59	.841640	2.18	.857056	2.03	.984584	4.22	.015416	1
60	9.841771		9.856934		9.984837		10.015163	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

′	Sine.	D. 1″.	Cosine.	D. 1″.	Tang.	D. 1″.	Cotang.	′
0	9.841771	2.18	9.856934	2.03	9.984837	4.22	10.015163	60
1	.841902	2.18	.856812	2.03	.985090	4.22	.014910	59
2	.842033	2.17	.856690	2.03	.985343	4.22	.014657	58
3	.842163	2.18	.856568	2.03	.985596	4.20	.014404	57
4	.842294	2.17	.856446	2.05	.985848	4.22	.014152	56
5	.842424	2.18	.856323	2.03	.986101	4.22	.013899	55
6	.842555	2.17	.856201	2.05	.986354	4.22	.013646	54
7	.842685	2.17	.856078	2.03	.986607	4.22	.013393	53
8	.842815	2.18	.855956	2.05	.986860	4.20	.013140	52
9	.842946	2.17	.855833	2.03	.987112	4.22	.012888	51
10	.843076	2.17	.855711	2.05	.987365	4.22	.012635	50
11	9.843206	2.17	9.855588	2.05	9.987618	4.22	10.012382	49
12	.843336	2.17	.855465	2.05	.987871	4.20	.012129	48
13	.843466	2.15	.855342	2.05	.988123	4.22	.011877	47
14	.843595	2.17	.855219	2.05	.988376	4.22	.011624	46
15	.843725	2.17	.855096	2.05	.988629	4.22	.011371	45
16	.843855	2.15	.854973	2.05	.988882	4.20	.011118	44
17	.843984	2.17	.854850	2.05	.989134	4.22	.010866	43
18	.844114	2.15	.854727	2.07	.989387	4.22	.010613	42
19	.844243	2.15	.854603	2.05	.989640	4.22	.010360	41
20	.844372	2.17	.854480	2.07	989893	4.20	.010107	40
21	9.844502	2.15	9.854356	2.05	9.990145	4.22	10.009855	39
22	.844631	2.15	.854233	2.07	.990398	4.22	.009602	38
23	.844760	2.15	.854109	2.05	.990651	4.20	.009349	37
24	.844889	2.15	.853986	2.07	.990903	4.22	.009097	36
25	.845018	2.15	.853862	2.07	.991156	4.22	.008844	35
26	.845127	2.15	.853738	2.07	.991409	4.22	.008591	34
27	.845276	2.15	.853614	2.07	.991662	4.20	.008338	33
28	.845405	2.13	.853490	2.07	.991914	4.22	.008086	32
29	.845533	2.15	.853366	2.07	.992167	4.22	.007833	31
30	.845662	2.13	.853242	2.07	.992420	4.20	.007580	30
31	9.845790	2.15	9.853118	2.07	9.992672	4.22	10.007328	29
32	.845919	2.13	.852994	2.08	.992925	4.22	.007075	28
33	.846047	2.13	.852869	2.07	.993178	4.22	.006822	27
34	.846175	2.15	.852745	2.08	.993431	4.20	.006569	26
35	.846304	2.13	.852620	2.07	.993683	4.22	.006317	25
36	.846432	2.13	.852496	2.08	.993936	4.22	.006064	24
37	.846560	2.13	.852371	2.07	.994189	4.20	.005811	23
38	.846688	2.13	.852247	2.08	.994441	4.22	.005559	22
39	.846816	2.13	.852122	2.08	.994694	4.22	.005306	21
40	.846944	2.12	.851997	2.08	.994947	4.20	.005053	20
41	9.847071	2.13	9.851872	2.08	9.995199	4.22	10.004801	19
42	.847199	2.13	.851747	2.08	.995452	4.22	.004548	18
43	.847327	2.12	.851622	2.08	.995705	4.20	.004295	17
44	.847454	2.13	.851497	2.08	.995957	4.22	.004043	16
45	.847582	2.12	.851372	2.10	.996210	4.22	.003790	15
46	.847709	2.12	.851246	2.08	.996463	4.20	.003537	14
47	.847836	2.13	.851121	2.08	.996715	4.22	.003285	13
48	.847964	2.12	.850996	2.10	.996968	4.22	.003032	12
49	.848091	2.12	.850870	2.08	.997221	4.20	.002779	11
50	.848218	2.12	.850745	2.10	.997473	4.22	.002527	10
51	9.848345	2.12	9.850619	2.10	9.997726	4.22	10.002274	9
52	.848472	2.12	.850493	2.08	.997979	4.20	.002021	8
53	.848599	2.12	.850368	2.10	.998231	4.22	.001769	7
54	.848726	2.10	.850242	2.10	.998484	4.22	.001516	6
55	.848852	2.12	.850116	2.10	.998737	4.20	.001263	5
56	.848979	2.12	.849990	2.10	.998989	4.22	.001011	4
57	.849106	2.10	.849864	2.10	.999242	4.22	.000758	3
58	.849232	2.12	.849738	2.12	.999495	4.20	.000505	2
59	.849359	2.10	.849611	2.10	.999747	4.22	.000253	1
60	9.849485		9.849485		10.000000		10.000000	0
′	Cosine.	D. 1″.	Sine.	D. 1″.	Cotang.	D. 1″.	Tang.	′

Art. 42. Azimuth by Altitude of Sun.

The azimuth of a given line may be determined by taking the altitude of the sun with an engineer's transit having a good vertical circle, and reading the horizontal angle between the sun and the line. The latitude of the place must be known and a nautical almanac must be at hand for finding the declination of the sun at the moment of observation.

In Fig 59 let A represent the center of the celestial sphere, Z the zenith, P the pole, N the north point of the horizon, S the position of the sun at the moment of observation. Then, in the spherical triangle PZS, the angle Z is the azimuth of the sun, and this is the same as the horizontal angle NAC. If AB be the line whose azimuth is to be found, NAB is its azimuth. Now if the horizontal angle BAC be measured, and Z be computed, the azimuth of AB is known.

To find the azimuth of the sun Z, let z be the complement of the observed altitude CS, corrected for refraction and parallax; let ϕ be the latitude of the place, or the arc NP; let δ be the declination of the sun, or the arc QS. Then in the spherical triangle PZS three sides are known, and hence

$$\tan \tfrac{1}{2}Z = \sqrt{\frac{\cos \frac{1}{2}(z+\phi+\delta)\sin \frac{1}{2}(z+\phi-\delta)}{\cos \frac{1}{2}(z-\phi-\delta)\sin \frac{1}{2}(z-\phi+\delta)}},$$

from which the azimuth Z can be computed.

In the figure S denotes the place of the sun in the summer half-year when δ is positive, and S' its place in the winter half-year when δ is negative. If the observation be made in the forenoon, the value of Z is less than 180 degrees; if it be made in the afternoon, its value is greater than 180 degrees.

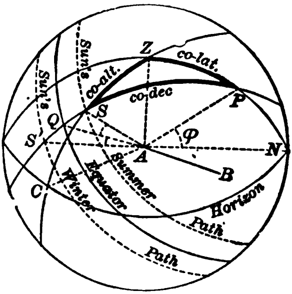


Fig. 59.

The transit having been put into thorough adjustment, it is set up at A, the end of the line AB, whose azimuth is to be found. The vernier of the horizontal limb having been set at 0° 00′, the telescope is pointed at B and the alidade unclamped. The telescope is

then pointed upon the sun, the objective and eyepiece being so focused that the shadow of the cross-wires and the image of the sun may be plainly seen on a white piece of paper held behind the eyepiece. The cross-wires should be made tangent to the bright circle on its lower and right-hand sides, and the horizontal and vertical angles be read. Next, the cross-wires should be made tangent on the upper and left-hand sides of the bright circle, and the angles be read again. If the transit has a full vertical circle, which is necessary for the best work, observations should be taken both in the direct and reverse position of the telescope.

The following record of an observation will illustrate the method of making the measurements and obtaining the data for computation. The declination δ for 8:43 A.M., eastern standard time, of the day of observation, is here taken from a nautical almanac, but for general purposes it may be taken

Time May 19, 1897.	Tel.	Vertical Angle. CAS	Horizontal Angle. BAC	Data and Results.
A.M.		Wires tang and right	ent to lower sides.	$\phi = 40° 36' 27''$ δ at 7 A.M. $= 19° 53' 10''$ 55
$8^h 40^m$	D	43° 09′ 00″	64° 48′ 00″	$\delta = 19° 54' 05''$
42	R	43 35 30	65 10 30	Appar. Alt. = 43° 58′ 22″ Parallax . . . +06 Refraction . . −60
		Wires tang and left	ent to upper sides.	Altitude = 43° 57′ 28″ 90 00 00
8 44	R	44° 21′ 00″	64° 52′ 30″	$z = 46° 02' 32''$
46	D	44 48 00	65 15 00	$Z = 101° 45' 36''$ 65 01 30
Means =		43° 58′ 22″	65° 01′ 30″	$NAB = 36° 44' 06''$

from the solar table mentioned on page 126. The mean apparent altitude is 43° 58′ 22″, and this being corrected for parallax and refraction, the zenith distance z is found. By computation from the formula, the mean azimuth of the sun is 101° 45′ 36″, and subtracting from this the mean horizontal angle BAC the final azimuth of the line AB is 36° 44′ 06″.

The uncertainty of an azimuth found by this method is two

or three minutes. The best time for observation is when the bearing of the sun is nearly east or nearly west, and for any precise work a mean result should be determined by several morning and afternoon observations.

The correction for parallax of the sun is less than 8″.6, and is always added to the apparent altitude; for an altitude of 20° the parallax correction is 8″, for 40° it is 7″, and for 60° it is 6″. In precise computations the value of the parallax correction may be found by multiplying 8″.6 by the cosine of the apparent altitude of the sun.

The correction for refraction is always subtracted from the apparent altitude, and its value is to be taken from the following table, interpolating when necessary.

TABLE XIII. MEAN REFRACTIONS.

Apparent Altitude.	Refraction.	Apparent Altitude.	Refraction.	Apparent Altitude.	Refraction.	Apparent Altitude.	Refraction.
0°	34′ 54″	20°	2′ 37″	40°	69″	60°	33″
1	24 25	21	2 29	41	66	61	33
2	18 09	22	2 22	42	64	62	31
3	14 15	23	2 15	43	62	63	29
4	11 39	24	2 09	44	60	64	28
5	9 46	25	2 03	45	58	65	27
6	8 23	26	1 58	46	56	66	26
7	7 20	27	1 53	47	54	67	24
8	6 30	28	1 48	48	52	68	23
9	5 49	29	1 44	49	50	69	22
10	5 16	30	1 40	50	48	70	21
11	4 49	31	1 36	51	47	72	19
12	4 25	32	1 32	52	45	74	17
13	4 05	33	1 29	53	43	76	15
14	3 47	34	1 25	54	42	78	12
15	3 32	35	1 22	55	40	80	10
16	3 19	36	1 19	56	39	82	8
17	3 07	37	1 16	57	38	84	6
18	2 56	38	1 14	58	36	86	4
19	2 46	39	1 11	59	35	88	2
20	2 37	40	1 09	60	33	90	0

Areas and Volumes.

In Fig. 60, $n+1$ offsets, $O_1, O_2, \ldots O_{n+1}$, distant d apart, are measured from a line fg to the curved boundary of a field as $ab \ldots bq$. Then the area of $abpqgf$ is given very nearly by the following formulas:

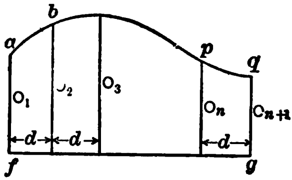


Fig. 60.

If $n = 2$, $A = \frac{1}{3}d(O_1 + 4O_2 + O_3)$ (Simpson's Rule).

If $n = 3$, $A = \frac{3}{8}d(O_1 + 3O_2 + 3O_3 + O_4)$ (Cotes' Rule).

If $n = 4$, $A = \frac{2}{45}d[7(O_1 + O_5) + 32(O_2 + O_4) + 12O_3]$.

If $n = 6$, $A = \frac{3}{10}d[O_1 + O_3 + O_5 + O_7 + 5(O_2 + O_4 + O_6) + O_4]$ (Weddles' Rule).

If n be even,

$$A = \tfrac{1}{3}d[O_1 + O_{n+1} + 4(O_2 + \ldots + O_n) + 2(O_3 + \ldots + O_{n-1})].$$

All the above formulas are exact if the curve be a parabola or a straight line.

The area of a segment of a circle is, very nearly:

$$A = \tfrac{4}{3}h\sqrt{2rh - (0.6 + 0.01h/r)h^2}.$$

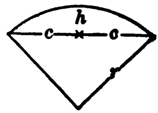


Fig. 61.

This formula gives areas exact to five places for values of h less than $0.6r$ and a maximum error, when $h = r$, of $0.00117r^2$. For more exact results when $h = 0.6r$, $0.7r$, $0.8r$, $0.9r$, and r, use, respectively, 0.6062, 0.6076, 0.6089, 0.6106, and 0.6121 for $(0.6 + 0.01h/r)$ in the formula.

The surface of a segment of a sphere is $A = 2\pi rh$ (Fig. 61).

The volume of a spherical segment is (Fig. 61):

$$V = \tfrac{1}{6}\pi h(3c^2 + h^2).$$

If a solid has parallel plane ends and is otherwise bounded by surfaces that can be generated by a straight line always touching the peripheries of the end planes, it is a prismoid and the volume is

$$V = \tfrac{1}{6}l(A_1 + 4M + A_2),$$

in which M is the area midway between the end areas A_1 and A_2 and l is the distance between the ends. This prismoidal formula applies also to spheres and ellipsoids. It is widely used for the computation of earthwork volumes.